



## 저작자표시 2.0 대한민국

이용자는 아래의 조건을 따르는 경우에 한하여 자유롭게

- 이 저작물을 복제, 배포, 전송, 전시, 공연 및 방송할 수 있습니다.
- 이차적 저작물을 작성할 수 있습니다.
- 이 저작물을 영리 목적으로 이용할 수 있습니다.

다음과 같은 조건을 따라야 합니다:



**저작자표시.** 귀하는 원저작자를 표시하여야 합니다.

- 귀하는, 이 저작물의 재이용이나 배포의 경우, 이 저작물에 적용된 이용허락조건을 명확하게 나타내어야 합니다.
- 저작권자로부터 별도의 허가를 받으면 이러한 조건들은 적용되지 않습니다.

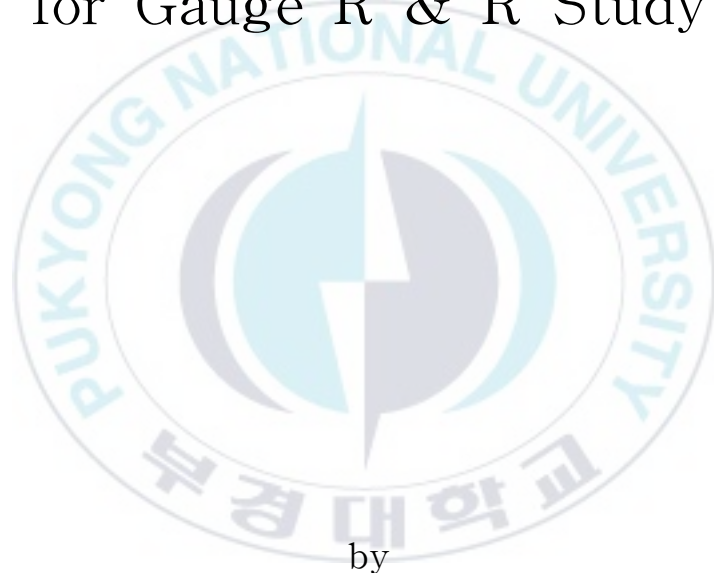
**저작권법에 따른 이용자의 권리는 위의 내용에 의하여 영향을 받지 않습니다.**

이것은 [이용허락규약\(Legal Code\)](#)을 이해하기 쉽게 요약한 것입니다.

[Disclaimer](#) 

Thesis for the Degree of Master of Science

Confidence Intervals in Two-factor  
Mixed Model with One Covariate  
for Gauge R & R Study



by

Jeong Hui Hong

Department of Statistics

The Graduate School

Pukyong National University

February 2007

Confidence Intervals in Two-factor  
Mixed Model with One Covariate  
for Gauge R & R Study  
계측기(R & R) 연구를 위한 공변량을 갖는  
2요인 혼합 모형의 신뢰구간

Advisor: Prof. Dong Joon Park

by  
Jeong Hui Hong

A thesis submitted in partial fulfillment of the requirements  
for the degree of

Master of Science

in the Department of Statistics, The Graduate School,  
Pukyong National University

February 2007

홍정희의 이학석사 학위논문을 인준함.

2007년 2월 일



주 심 이학박사 장 대 홍 (인)

위 원 이학박사 차 지 환 (인)

위 원 이학박사 박 동 준 (인)

This certifies that the dissertaion of  
Jeong Hui Hong is approved

A dissertation  
by  
Jeong Hui Hong

Approved by:

---

Dae-Heung Jang

---

Ji-Hwan Cha

---

Dong-Joon Park

February 28, 2007

계측기(R&R) 연구를 위한 공변량을 갖는  
2요인 혼합 모형의 신뢰구간

홍 정 희

부경대학교 대학원 통계학과

요 약

이 논문은 계측기 (R & R) 연구를 위한 공변량을 갖는 2요인 교차 혼합모형에 나타난 변동에 관한 신뢰구간을 제안하였다. 모형의 변동은 부품, 작업자, 측정의 분산을 의미하는데 제안되는 신뢰구간들은 수정대표본 방법, 일반화 P값에 의한 방법, SAS의 PROC MIXED에서 계산되는 잔차 최대우도방법에 기초하였다. 제안되는 세 가지 방법들을 비교하기 위하여 부품과 작업자와 측정값들의 여러 가지 값들에 대하여 SAS/IML로 시뮬레이션을 실행하였다. 시뮬레이션 결과 특히 총 분산에 대한 부품이나 작업자의 분산 비율이 작을 때는 수정대표본방법이나 일반화 P값에 의한 신뢰구간이 잔차 최대우도 방법보다 더 신뢰계수를 잘 지킨다는 것을 볼 수 있었고 수치 값이 들어있는 예제를 제시하였다.

# CONTENTS

|                                                                                         | Page |
|-----------------------------------------------------------------------------------------|------|
| LIST OF TABLES .....                                                                    | ii   |
| LIST OF FIGURES .....                                                                   | vii  |
| ABSTRACT (KOREAN) .....                                                                 | 1    |
| CHAPTER                                                                                 |      |
| 1 INTRODUCTION .....                                                                    | 2    |
| 2 CONFIDENCE INTERVALS IN TWO-FACTOR CROSSED<br>MIXED MODEL WITH ONE COVARIATE .....    | 4    |
| 2.1 Two-factor Crossed Mixed Model with One Covariate .....                             | 4    |
| 2.2 Distributional Results .....                                                        | 4    |
| 2.3 Confidence Intervals on Variance Components Using et al.<br>Method .....            | 22   |
| 2.4 Generalized Confidence Intervals on Variance Components .                           | 25   |
| 2.5 Confidence Intervals on Variance Components Using SAS<br>PROC MIXED Procedure ..... | 27   |
| 3 SIMULATION AND CONCLUSION .....                                                       | 29   |
| 3.1 Simulation Study .....                                                              | 29   |
| 3.2 Simulation Results .....                                                            | 31   |
| 3.3 A Numerical Example .....                                                           | 93   |
| 3.4 Concluding Remarks .....                                                            | 97   |
| REFERENCES .....                                                                        | 98   |
| Appendix .....                                                                          | 100  |

## LIST OF TABLES

| Table |                                                               | Page |
|-------|---------------------------------------------------------------|------|
| 2.2.1 | ANOVA for Model (2.2.1) .....                                 | 9    |
| 2.2.2 | Adjusted ANOVA for Model (2.2.1) .....                        | 10   |
| 2.5.1 | An Example Statement of PROC MIXED .....                      | 27   |
| 3.1.1 | Eight Designs Used in Simulation Study .....                  | 29   |
| 3.1.2 | Parameter Values Used in Simulation Study .....               | 30   |
| 3.2.1 | Range of Simulated Confidence Coefficients for 90%            |      |
|       | Two-sided Intervals on $\sigma_P^2$ when I=6, J=3, K=2 .....  | 33   |
| 3.2.2 | Range of Simulated Confidence Coefficients for 90%            |      |
|       | Two-sided Intervals on $\sigma_P^2$ when I=6, J=3, K=4 .....  | 34   |
| 3.2.3 | Range of Simulated Confidence Coefficients for 90%            |      |
|       | Two-sided Intervals on $\sigma_P^2$ when I=6, J=6, K=2 .....  | 35   |
| 3.2.4 | Range of Simulated Confidence Coefficients for 90%            |      |
|       | Two-sided Intervals on $\sigma_P^2$ when I=6, J=6, K=4 .....  | 36   |
| 3.2.5 | Range of Simulated Confidence Coefficients for 90%            |      |
|       | Two-sided Intervals on $\sigma_P^2$ when I=12, J=3, K=2 ..... | 37   |
| 3.2.6 | Range of Simulated Confidence Coefficients for 90%            |      |
|       | Two-sided Intervals on $\sigma_P^2$ when I=12, J=3, K=4 ..... | 38   |
| 3.2.7 | Range of Simulated Confidence Coefficients for 90%            |      |
|       | Two-sided Intervals on $\sigma_P^2$ when I=12, J=6, K=2 ..... | 39   |
| 3.2.8 | Range of Simulated Confidence Coefficients for 90%            |      |
|       | Two-sided Intervals on $\sigma_P^2$ when I=12, J=6, K=4 ..... | 40   |



| Table  |                                                               | Page |
|--------|---------------------------------------------------------------|------|
| 3.2.9  | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_P^2$ when I=24, J=3, K=2 ..... | 41   |
| 3.2.10 | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_P^2$ when I=24, J=3, K=4 ..... | 42   |
| 3.2.11 | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_P^2$ when I=24, J=6, K=2 ..... | 43   |
| 3.2.12 | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_P^2$ when I=24, J=6, K=4 ..... | 44   |
| 3.2.13 | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_O^2$ when I=6, J=3, K=2 .....  | 45   |
| 3.2.14 | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_O^2$ when I=6, J=3, K=4 .....  | 46   |
| 3.2.15 | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_O^2$ when I=6, J=6, K=2 .....  | 47   |
| 3.2.16 | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_O^2$ when I=6, J=6, K=4 .....  | 48   |
| 3.2.17 | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_O^2$ when I=12, J=3, K=2 ..... | 49   |
| 3.2.18 | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_O^2$ when I=12, J=3, K=4 ..... | 50   |
| 3.2.19 | Range of Simulated Confidence Coefficients for 90%            |      |
|        | Two-sided Intervals on $\sigma_O^2$ when I=12, J=6, K=2 ..... | 51   |

| Table  | Page                                                                                                                   |
|--------|------------------------------------------------------------------------------------------------------------------------|
| 3.2.20 | Range of Simulated Confidence Coefficients for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=12, J=6, K=4 ..... 52 |
| 3.2.21 | Range of Simulated Confidence Coefficients for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=24, J=3, K=2 ..... 53 |
| 3.2.22 | Range of Simulated Confidence Coefficients for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=24, J=3, K=4 ..... 54 |
| 3.2.23 | Range of Simulated Confidence Coefficients for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=24, J=6, K=2 ..... 55 |
| 3.2.24 | Range of Simulated Confidence Coefficients for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=24, J=6, K=4 ..... 56 |
| 3.2.25 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=6, J=3, K=2 ..... 57           |
| 3.2.26 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=6, J=3, K=4 ..... 58           |
| 3.2.27 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=6, J=6, K=2 ..... 59           |
| 3.2.28 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=6, J=6, K=4 ..... 60           |
| 3.2.29 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=12, J=3, K=2 ..... 61          |
| 3.2.30 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=12, J=3, K=4 ..... 62          |

| Table  | Page                                                                                                          |
|--------|---------------------------------------------------------------------------------------------------------------|
| 3.2.31 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=12, J=6, K=2 ..... 63 |
| 3.2.32 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=12, J=6, K=4 ..... 64 |
| 3.2.33 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=24, J=3, K=2 ..... 65 |
| 3.2.34 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=24, J=3, K=4 ..... 66 |
| 3.2.35 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=24, J=6, K=2 ..... 67 |
| 3.2.36 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_P^2$ when I=24, J=6, K=4 ..... 68 |
| 3.2.37 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=6, J=3, K=2 ..... 69  |
| 3.2.38 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=6, J=3, K=4 ..... 70  |
| 3.2.39 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=6, J=6, K=2 ..... 71  |
| 3.2.40 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=6, J=6, K=4 ..... 72  |
| 3.2.41 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=12, J=3, K=2 ..... 73 |

| Table  |                                                                                                            | Page |
|--------|------------------------------------------------------------------------------------------------------------|------|
| 3.2.42 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=12, J=3, K=4 ..... | 74   |
| 3.2.43 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=12, J=6, K=2 ..... | 75   |
| 3.2.44 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=12, J=6, K=4 ..... | 76   |
| 3.2.45 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=24, J=3, K=2 ..... | 77   |
| 3.2.46 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=24, J=3, K=4 ..... | 78   |
| 3.2.47 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=24, J=6, K=2 ..... | 79   |
| 3.2.48 | Range of Average Interval Lengths for 90%<br>Two-sided Intervals on $\sigma_O^2$ when I=24, J=6, K=4 ..... | 80   |
| 3.3.1  | Data Set Used .....                                                                                        | 94   |
| 3.3.2  | An Example Statement of PROC GLM for<br>Calculating Mean Squares .....                                     | 94   |
| 3.3.3  | Results of PROC GLM .....                                                                                  | 95   |
| 3.3.4  | 90% Confidence Intervals on Variance<br>Components .....                                                   | 96   |

## LIST OF FIGURES

| Figure  |                                                        | Page |
|---------|--------------------------------------------------------|------|
| 3.2.1.a | Boxplots for Simulated Confidence Coefficients for 90% |      |
|         | Two-sided Intervals on $\sigma_P^2$ .....              | 81   |
| 3.2.1.b | Boxplots for Simulated Confidence Coefficients for 90% |      |
|         | Two-sided Intervals on $\sigma_P^2$ .....              | 82   |
| 3.2.1.c | Boxplots for Simulated Confidence Coefficients for 90% |      |
|         | Two-sided Intervals on $\sigma_P^2$ .....              | 83   |
| 3.2.2.a | Boxplots for Simulated Confidence Coefficients for 90% |      |
|         | Two-sided Intervals on $\sigma_O^2$ .....              | 84   |
| 3.2.2.b | Boxplots for Simulated Confidence Coefficients for 90% |      |
|         | Two-sided Intervals on $\sigma_O^2$ .....              | 85   |
| 3.2.2.c | Boxplots for Simulated Confidence Coefficients for 90% |      |
|         | Two-sided Intervals on $\sigma_O^2$ .....              | 86   |
| 3.2.3.a | Boxplots for Average Interval Length for 90%           |      |
|         | Two-sided Intervals on $\sigma_P^2$ .....              | 87   |
| 3.2.3.b | Boxplots for Average Interval Length for 90%           |      |
|         | Two-sided Intervals on $\sigma_P^2$ .....              | 88   |
| 3.2.3.c | Boxplots for Average Interval Length for 90%           |      |
|         | Two-sided Intervals on $\sigma_P^2$ .....              | 89   |
| 3.2.4.a | Boxplots for Average Interval Length for 90%           |      |
|         | Two-sided Intervals on $\sigma_O^2$ .....              | 90   |

| Figure  |                                              | Page |
|---------|----------------------------------------------|------|
| 3.2.4.b | Boxplots for Average Interval Length for 90% |      |
|         | Two-sided Intervals on $\sigma_P^2$ .....    | 91   |
| 3.2.4.c | Boxplots for Average Interval Length for 90% |      |
|         | Two-sided Intervals on $\sigma_P^2$ .....    | 92   |



계측기(R&R) 연구를 위한 공변량을 갖는  
2요인 혼합 모형의 신뢰구간

홍 정 희

부경대학교 대학원 통계학과

요 약

이 논문은 계측기 (R & R) 연구를 위한 공변량을 갖는 2요인 교차 혼합모형에 나타난 변동에 관한 신뢰구간을 제안하였다. 모형의 변동은 부품, 작업자, 측정의 분산을 의미하는데 제안되는 신뢰구간들은 수정대표본 방법, 일반화 P값에 의한 방법, SAS의 PROC MIXED에서 계산되는 잔차 최대우도방법에 기초하였다. 제안되는 세 가지 방법들을 비교하기 위하여 부품과 작업자와 측정값들의 여러 가지 값들에 대하여 SAS/IML로 시뮬레이션을 실행하였다. 시뮬레이션 결과 특히 총 분산에 대한 부품이나 작업자의 분산 비율이 작을 때는 수정대표본방법이나 일반화 P값에 의한 신뢰구간이 잔차 최대우도 방법보다 더 신뢰계수를 잘 지킨다는 것을 볼 수 있었고 수치 값이 들어있는 예제를 제시하였다.

## 1. INTRODUCTION

Measurements obtained in manufacturing process are used to control the quality of final product. The sources of variability in the measurement process are due to the measurement system. In order to determine whether a measurement procedure is adequate for monitoring a manufacturing process, gauge capability analysis is needed. A gauge is used to obtain replicate measurements on units by several different operators, setups, or time periods. One of the common experiments employed in industry is to properly monitor manufacturing process, e.g., repeatability and reproducibility. The variability is inherent in the measurement system, which we generally think of as the precision of the gauge. Gauge repeatability and reproducibility(R & R) study include comparison of measurement system with manufacturing process. The sources of variability in gauge R & R study are expressed as variance components and confidence intervals on variance components are utilized for quality control. Burdick et al.(2005) define that repeatability represents the gauge variability when it is used to measure the same unit(with the same operator or setup or in the same time period). Reproducibility is referred to as the variability arising from different operators, setups, or time periods.

Montgomery and Runger(1993 a, 1993 b) provided complete background on gauge capability and designed experiments. They compared classical R & R analysis using  $\bar{X}$  and  $R$  charts and ANOVA analysis by illustrating numerical examples. Burdick and Larsen(1997) proposed alternative confidence intervals on measures of variability in a balanced two-factor crossed random models. They compared a modified large sample(MLS) method and Restricted Maximum Likelihood(REML) method. Borrer et al.(1997) compared MLS



method with REML method for confidence intervals on gauge variability in balanced two-factor crossed random models with interaction. They concluded that REML method resulted in shorter intervals than MLS method but REML method did not maintain the stated level of confidence. Dolezal et al.(1998) considered a balanced two-factor crossed random model with fixed operators and compared two confidence intervals; operator as a random factor as usual and operator as a fixed factor. Burdick et al.(2003) provided more recent review of the methods for conducting and analyzing measurement systems capabilities, focusing on the analysis of variance approach. Adamec and Burdick(2003) proposed two confidence intervals on a discrimination ratio used to determine the adequacy of the measurement system considering a traditional two-factor model. Gong et al.(2005) considered methods for constructing confidence intervals in a two-factor gauge repeatability and reproducibility when there are unequal replicates. They provided easy and simple EXCEL and SAS codes for calculating confidence intervals. The classical R & R study gives a downward biased estimator of the variance component representing gauge reproducibility. Confidence intervals on variance components are therefore analyzed using ANOVA approach that leads to a direct and convenient method in an experimental design(Montgomery and Runger, 1993 b).

This thesis proposes confidence intervals on variance components in two factor crossed mixed model with one covariate for gauge R & R study. Computer simulation is used to compare the performance of the confidence intervals. A numerical example is provided and recommendations are presented.

## 2. CONFIDENCE INTERVALS IN TWO-FACTOR CROSSED MIXED MODEL WITH ONE COVARIATE

### 2.1 Two-factor Crossed Mixed Model with One Covariate

Two-factor crossed mixed model with one covariate for gauge R & R study employs  $J$  operators randomly chosen to conduct measurements on  $I$  randomly selected parts from a manufacturing process. In this R&R study each operator measures each part  $k$  times. The model that explains this study is written as

$$Y_{ijk} = \mu + \beta X_{ijk} + P_i + O_j + E_{ijk} \quad (2.1.1)$$

$$i = 1, \dots, I; \quad j = 1, \dots, J; \quad k = 1, \dots, K$$

where  $Y_{ijk}$  is the  $k$ th measurement of the  $i$ th part measured by the  $j$ th operator,  $\mu$  and  $\beta$  are unknown constants,  $X_{ijk}$  is a covariate,  $P_i$  is the  $i$ th randomly selected part,  $O_j$  is the  $j$ th randomly chosen operator, and  $E_{ijk}$  is the  $k$ th measurement error of the  $i$ th part measured by the  $j$ th operator.  $P_i$ ,  $O_j$ , and  $E_{ijk}$  are jointly independent normal random variables with zero means and variances  $\sigma_P^2$ ,  $\sigma_O^2$ , and  $\sigma_E^2$ , respectively. Since the  $X_{ijk}$  and  $\beta$  are fixed and  $P_i$  and  $O_j$  are random, model (2.1.1) is a two-factor crossed mixed model with one covariate.

### 2.2 Distributional Results

Model (2.1.1) is written in matrix notation,

$$\mathbf{y} = \mathbf{X} \underline{\alpha} + \mathbf{Z}_1 \mathbf{p} + \mathbf{Z}_2 \mathbf{o} + \mathbf{Z}_3 \mathbf{e} \quad (2.2.1)$$

where  $\mathbf{y}$  is an  $IJK \times 1$  vector of observations,  $\mathbf{X}$  is an  $IJK$  matrix of known values with a column of 1's in the first column and a column of  $X_{ijk}$ 's in the

second column,  $\underline{\alpha}$  is a  $2 \times 1$  vector of parameters with  $\mu$  and  $\beta$  as elements,  $\mathbf{Z}_1$  is an  $IJK \times I$  design matrix with 0's and 1's,  $\mathbf{p}$  is an  $I \times 1$  vector of random part effects,  $\mathbf{Z}_2$  is an  $IJK \times J$  design matrix with 0's and 1's,  $\mathbf{o}$  is a  $J \times 1$  vector of random operator effects,  $\mathbf{Z}_3$  is an  $IJK \times IJK$  design matrix which is an identity matrix, and  $\mathbf{e}$  is an  $IJK \times 1$  vector of random measurement errors. In particular,

$$\mathbf{y} = \begin{bmatrix} Y_{111} \\ \vdots \\ Y_{IJK} \end{bmatrix}, \quad \mathbf{X} = \begin{bmatrix} 1 & X_{111} \\ \vdots & \vdots \\ \vdots & \vdots \\ 1 & X_{IJK} \end{bmatrix}, \quad \underline{\alpha} = \begin{bmatrix} \mu \\ \beta \end{bmatrix},$$

$$\mathbf{p} = \begin{bmatrix} P_1 \\ \vdots \\ \vdots \\ P_I \end{bmatrix}, \quad \mathbf{o} = \begin{bmatrix} O_1 \\ \vdots \\ \vdots \\ O_J \end{bmatrix}, \quad \mathbf{e} = \begin{bmatrix} E_{111} \\ \vdots \\ \vdots \\ E_{IJK} \end{bmatrix},$$

$$\begin{aligned}
\mathbf{Z}_1 &= \begin{bmatrix} 1 & 0 & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ 1 & 0 & \dots & 0 \\ 0 & 1 & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ 0 & 1 & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ 0 & 0 & \dots & 1 \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ 0 & 0 & \dots & 1 \end{bmatrix} = \bigoplus_{i=1}^I \underline{1}_{JK}, \quad \mathbf{Z}_2 = \begin{bmatrix} 1 & 0 & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ 1 & 0 & \dots & 0 \\ 0 & 1 & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ 0 & 1 & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ 0 & 0 & \dots & 1 \\ \vdots & \vdots & \dots & \vdots \\ 0 & 0 & \dots & 1 \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ \vdots & \vdots & \dots & \vdots \\ 1 & 0 & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ 1 & 0 & \dots & 0 \\ 0 & 1 & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ 0 & 1 & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ 0 & 0 & \dots & 1 \\ \vdots & \vdots & \dots & \vdots \\ 0 & 0 & \dots & 1 \end{bmatrix} = \underline{1}_I \otimes \left( \bigoplus_{j=1}^J \underline{1}_K \right),
\end{aligned}$$

$$\mathbf{Z}_3 = \begin{bmatrix} 1 & 0 & 0 & \dots & 0 \\ 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & 1 \end{bmatrix} = \mathbf{D}_{IJK},$$

$\mathbf{1}_{JK}$ ,  $\mathbf{1}_I$ , and  $\mathbf{1}_K$  are, respectively, a  $JK \times 1$  column vector of 1's, an  $I \times 1$  column vector of 1's, and a  $K \times 1$  column vector of 1's,  $\oplus$  is the direct sum operator,  $\otimes$  is the direct product operator, and  $\mathbf{D}_{IJK}$  is an  $IJK \times IJK$  identity matrix. The direct sum of two matrices  $A$  and  $B$  is defined as

$$\mathbf{A} \oplus \mathbf{B} = \begin{bmatrix} \mathbf{A} & 0 \\ 0 & \mathbf{B} \end{bmatrix}$$

and the direct product of two matrices  $A$  and  $B$  is defined as

$$\mathbf{A}_{p \times q} \otimes \mathbf{B}_{m \times n} = \begin{bmatrix} a_{11}\mathbf{B}_{m \times n} & \dots & a_{1q}\mathbf{B}_{m \times n} \\ \vdots & \ddots & \vdots \\ a_{p1}\mathbf{B}_{m \times n} & \dots & a_{pq}\mathbf{B}_{m \times n} \end{bmatrix}.$$

The variance-covariance matrix of  $\mathbf{y}$  is

$$\begin{aligned} \mathbf{V} = V(\mathbf{y}) &= V(\mathbf{X}\underline{\alpha} + \mathbf{Z}_1\mathbf{p} + \mathbf{Z}_2\mathbf{o} + \mathbf{Z}_3\mathbf{e}) \\ &= \sigma_P^2 \mathbf{Z}_1 \mathbf{Z}_1' + \sigma_O^2 \mathbf{Z}_2 \mathbf{Z}_2' + \sigma_E^2 \mathbf{Z}_3 \mathbf{Z}_3'. \end{aligned}$$

In particular, the covariance of  $Y_{ijk}$ , and  $Y_{i'j'k'}$  is obtained as

$$Cov(Y_{ijk}, Y_{i'j'k'}) = \begin{cases} 0 & \text{if } i \neq i' \\ \sigma_P^2 & \text{if } i = i', j \neq j' \\ \sigma_P^2 + \sigma_O^2 & \text{if } i = i', j = j', k \neq k' \\ \sigma_P^2 + \sigma_O^2 + \sigma_E^2 & \text{if } i = i', j = j', k = k' \end{cases}.$$

The variance-covariance matrix structure of  $\mathbf{V}$  is

$$\mathbf{V} = \begin{bmatrix} \mathbf{V}_1 & 0 & \cdots & 0 \\ 0 & \mathbf{V}_2 & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \cdots & \mathbf{V}_I \end{bmatrix}$$

where matrix  $\mathbf{V}_i$  is

$$\mathbf{V}_i = \begin{matrix} & \begin{matrix} Y_{i11} & \cdots & Y_{i1K} & \cdots & Y_{iJ1} & \cdots & Y_{iJK} \end{matrix} \\ \begin{matrix} Y_{i11} \\ \vdots \\ Y_{i1K} \\ \vdots \\ Y_{iJ1} \\ \vdots \\ Y_{iJK} \end{matrix} & \begin{pmatrix} V_{POE} & \cdots & V_{PO} & \cdots & V_P & \cdots & V_P \\ \vdots & \ddots & \vdots & & \vdots & & \vdots \\ V_{PO} & \cdots & V_{POE} & \cdots & V_P & \cdots & V_P \\ \vdots & & \vdots & \ddots & \vdots & & \vdots \\ V_P & \cdots & V_P & \cdots & V_{POE} & \cdots & V_{PO} \\ \vdots & & \vdots & & \vdots & \ddots & \vdots \\ V_P & \cdots & V_P & \cdots & V_{PO} & \cdots & V_{POE} \end{pmatrix} \end{matrix},$$

$$V_{POE} = \sigma_P^2 + \sigma_O^2 + \sigma_E^2, \quad V_{PO} = \sigma_P^2 + \sigma_O^2, \quad \text{and} \quad V_P = \sigma_P^2.$$

In order to form confidence intervals on the variance components, an appropriate set of sums of squares is needed. The analysis of variance for  $Y_{ijk}$ ,  $X_{ijk}$ , and  $X_{ijk}Y_{ijk}$  is shown in Table 2.2.1.

**TABLE 2.2.1 ANOVA for Model (2.1.1)**

| Sums of Squares and Products |           |           |            |                   |
|------------------------------|-----------|-----------|------------|-------------------|
| SV                           | Y         | X         | XY         | DF                |
| Parts                        | $SS_{PY}$ | $SS_{PX}$ | $SP_{PXY}$ | $I - 1$           |
| Operators                    | $SS_{OY}$ | $SS_{OX}$ | $SP_{OXY}$ | $J - 1$           |
| Error                        | $SS_{EY}$ | $SS_{EX}$ | $SP_{EXY}$ | $IJK - I - J + 1$ |
| Total                        | $SST_Y$   | $SST_X$   | $SPT_{XY}$ | $IJK - 1$         |

The notation in Table 2.2.1. is defined as

$$SS_{PY} = JK \sum_i (\bar{Y}_{i..} - \bar{Y}...)^2,$$

$$SS_{PX} = JK \sum_i (\bar{X}_{i..} - \bar{X}...)^2,$$

$$SP_{PXY} = JK \sum_i (\bar{X}_{i..} - \bar{X}...)(\bar{Y}_{i..} - \bar{Y}...),$$

$$SS_{OY} = IK \sum_j (\bar{Y}_{.j.} - \bar{Y}...)^2,$$

$$SS_{OX} = IK \sum_j (\bar{X}_{.j.} - \bar{X}...)^2,$$

$$SP_{OXY} = IK \sum_j (\bar{X}_{.j.} - \bar{X}...)(\bar{Y}_{.j.} - \bar{Y}...),$$

$$\begin{aligned}
SS_{EY} &= \sum_i \sum_j \sum_k (Y_{ijk} - \bar{Y}_{i..} - \bar{Y}_{.j.} + \bar{Y}_{...})^2, \\
SS_{EX} &= \sum_i \sum_j \sum_k (X_{ijk} - \bar{X}_{i..} - \bar{X}_{.j.} + \bar{X}_{...})^2, \\
SP_{EXY} &= \sum_i \sum_j \sum_k (X_{ijk} - \bar{X}_{i..} - \bar{X}_{.j.} + \bar{X}_{...})(Y_{ijk} - \bar{Y}_{i..} - \bar{Y}_{.j.} + \bar{Y}_{...}), \\
SST_Y &= \sum_i \sum_j \sum_k (Y_{ijk} - \bar{Y}_{...})^2, \\
SST_X &= \sum_i \sum_j \sum_k (X_{ijk} - \bar{X}_{...})^2, \quad \text{and} \\
SPT_{XY} &= \sum_i \sum_j \sum_k (X_{ijk} - \bar{X}_{...})(Y_{ijk} - \bar{Y}_{...}).
\end{aligned}$$

In order to focus on constructing confidence intervals on the variance components, Table 2.2.1 is modified in Table 2.2.2 that presents expected mean squares.

**TABLE 2.2.2 Adjusted ANOVA for Model(2.1.1)**

| SV         | SS    | DF            | MS      | EMS                         |
|------------|-------|---------------|---------|-----------------------------|
| Parts      | $R_1$ | $I - 2$       | $S_P^2$ | $\sigma_E^2 + JK\sigma_P^2$ |
| Operators  | $R_2$ | $J - 2$       | $S_O^2$ | $\sigma_E^2 + IK\sigma_O^2$ |
| Replicates | $R_3$ | $IJK - I - J$ | $S_E^2$ | $\sigma_E^2$                |

where sums of squares  $R_1$ ,  $R_2$ , and  $R_3$  and mean squares  $S_P^2$ ,  $S_O^2$ , and  $S_E^2$  are defined as



$$S_P^2 = \frac{R_1}{I - 2},$$

$$S_O^2 = \frac{R_2}{J - 2},$$

$$S_E^2 = \frac{R_3}{IJK - I - J},$$

$$R_1 = JK \mathbf{y}' \mathbf{W}_1' (\mathbf{D}_I - \mathbf{H}_1) \mathbf{W}_1 \mathbf{y},$$

$$R_2 = IK \mathbf{y}' \mathbf{W}_2' (\mathbf{D}_J - \mathbf{H}_2) \mathbf{W}_2 \mathbf{y},$$

$$R_3 = \mathbf{y}' \mathbf{W}_3' (\mathbf{D}_{IJK} - \mathbf{H}_3) \mathbf{W}_3 \mathbf{y},$$

$$\mathbf{W}_1 = \frac{1}{JK} \mathbf{Z}_1',$$

$$\mathbf{W}_2 = \frac{1}{IK} \mathbf{Z}_2',$$

$$\mathbf{W}_3 = \mathbf{Z}_3' = \mathbf{D}_{IJK},$$

$$\mathbf{H}_1 = \mathbf{X}_1 (\mathbf{X}_1' \mathbf{X}_1)^{-1} \mathbf{X}_1',$$

$$\mathbf{H}_2 = \mathbf{X}_2 (\mathbf{X}_2' \mathbf{X}_2)^{-1} \mathbf{X}_2',$$

$$\mathbf{H}_3 = \mathbf{X}_3 (\mathbf{X}_3' \mathbf{X}_3)^{-1} \mathbf{X}_3',$$

$$\mathbf{X}_1 = \mathbf{W}_1 \mathbf{X},$$

$$\mathbf{X}_2 = \mathbf{W}_2 \mathbf{X}, \text{ and}$$

$$\mathbf{X}_3 = [\mathbf{X} \ \mathbf{Z}_1 \ \mathbf{Z}_2].$$

A set of jointly independent chi-squared variables is necessary for deriving confidence intervals on the variance components. The distributional properties of the sums of squares in Table 2.2.2 are now examined.

Theorem 2.2.1 : Under the distributional assumptions in (2.1.1),  $R_1/(\sigma_E^2 + JK\sigma_P^2)$  is a chi-squared random variable with  $I - 2$  degrees of freedom.

Proof : Consider (2.2.1) and multiply both sides of the equation on the left by  $(\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1$

where

$\mathbf{D}_I =$  an identity matrix of order  $I$ ,

$\mathbf{H}_1 = \mathbf{X}_1(\mathbf{X}_1'\mathbf{X}_1)^{-1}\mathbf{X}_1'$ ,

$\mathbf{X}_1 = \mathbf{W}_1\mathbf{X}$ , and

$$\mathbf{W}_1 = \frac{1}{JK}\mathbf{Z}_1'.$$

It follows that

$$\begin{aligned} (\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1\mathbf{y} &= (\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1\mathbf{X}\underline{\alpha} + (\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1\mathbf{Z}_1\mathbf{p} \\ &\quad + (\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1\mathbf{Z}_2\mathbf{o} + (\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1\mathbf{Z}_3\mathbf{e}. \end{aligned} \quad (2.2.2)$$

Let  $(\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1\mathbf{y} = \mathbf{y}_1$ . Since

$$(\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1\mathbf{X} = (\mathbf{D}_I - \mathbf{H}_1)\mathbf{X}_1 = \mathbf{X}_1 - \mathbf{H}_1\mathbf{X}_1 = \mathbf{0},$$

$$\mathbf{W}_1\mathbf{Z}_1 = \frac{1}{JK}\mathbf{Z}_1'\mathbf{Z}_1 = \frac{1}{JK}JK\mathbf{D}_I = \mathbf{D}_I, \text{ and}$$

$$\mathbf{W}_1\mathbf{Z}_3 = \frac{1}{JK}\mathbf{Z}_1'\mathbf{Z}_3 = \frac{1}{JK}\mathbf{Z}_1',$$

(2.2.2) is written as

$$\mathbf{y}_1 = (\mathbf{D}_I - \mathbf{H}_1)\mathbf{p} + (\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1\mathbf{Z}_2\mathbf{o} + \frac{1}{JK}(\mathbf{D}_I - \mathbf{H}_1)\mathbf{Z}_1'\mathbf{e}.$$

Note that

$$\begin{aligned}
\mathbf{W}_1 \mathbf{Z}_2 &= \frac{1}{JK} \mathbf{Z}'_1 \mathbf{Z}_2 = \frac{1}{JK} K \underline{1}_I \underline{1}'_J = \frac{1}{J} \underline{1}_I \underline{1}'_J \text{ and} \\
(\mathbf{D}_I - \mathbf{H}_1) \mathbf{W}_1 \mathbf{Z}_2 \mathbf{Z}'_2 \mathbf{W}'_1 (\mathbf{D}_I - \mathbf{H}_1) &= (\mathbf{D}_I - \mathbf{H}_1) \frac{1}{J} \underline{1}_I \underline{1}'_J \frac{1}{J} \underline{1}_J \underline{1}'_I (\mathbf{D}_I - \mathbf{H}_1) \\
&= (\mathbf{D}_I - \mathbf{H}_1) \frac{1}{J^2} J \underline{1}_I \underline{1}'_I (\mathbf{D}_I - \mathbf{H}_1) \\
&= (\mathbf{D}_I - \mathbf{H}_1) \frac{1}{J} \underline{1}_I \underline{1}'_I (\mathbf{D}_I - \mathbf{H}_1) \\
&= \frac{1}{J} (\mathbf{D}_I - \mathbf{H}_1) \underline{1}_I [(\mathbf{D}_I - \mathbf{H}_1) \underline{1}_I]' \\
&= \frac{1}{J} \underline{0} \underline{0}' \\
&= \underline{0}
\end{aligned}$$

since  $\mathbf{H}_1$  is an idempotent matrix and

$$\begin{aligned}
(\mathbf{D}_I - \mathbf{H}_1) \underline{1}_I &= \underline{1}_I - \mathbf{X}_1 (\mathbf{X}'_1 \mathbf{X}_1)^{-1} \mathbf{X}'_1 \underline{1}_I \\
&= \underline{1}_I - \underline{1}_I \\
&= \underline{0}.
\end{aligned}$$

Considering that

$$\mathbf{Z}'_1 \mathbf{Z}_1 = JK \mathbf{D}_I,$$

the variance of  $\mathbf{y}_1$  is

$$\begin{aligned}
V(\mathbf{y}_1) &= V((\mathbf{D}_I - \mathbf{H}_1) \mathbf{p}) + V((\mathbf{D}_I - \mathbf{H}_1) \mathbf{W}_1 \mathbf{Z}_2 \mathbf{o}) + V\left(\frac{1}{JK} (\mathbf{D}_I - \mathbf{H}_1) \mathbf{Z}'_1 \mathbf{e}\right) \\
&= \sigma_P^2 (\mathbf{D}_I - \mathbf{H}_1) + \frac{1}{JK} \sigma_E^2 (\mathbf{D}_I - \mathbf{H}_1) \\
&= \frac{1}{JK} (\sigma_E^2 + JK \sigma_P^2) (\mathbf{D}_I - \mathbf{H}_1).
\end{aligned}$$

The distribution of  $R_1$  is determined by writing

$$\begin{aligned}
& \frac{R_1}{\sigma_E^2 + JK\sigma_P^2} \\
&= \mathbf{y}' \mathbf{W}'_1 (\mathbf{D}_I - \mathbf{H}_1) \left[ \frac{JK(\mathbf{D}_I - \mathbf{H}_1)}{\sigma_E^2 + JK\sigma_P^2} \right] (\mathbf{D}_I - \mathbf{H}_1) \mathbf{W}_1 \mathbf{y} \quad (2.2.3) \\
&= \mathbf{y}'_1 \left[ \frac{JK(\mathbf{D}_I - \mathbf{H}_1)}{\sigma_E^2 + JK\sigma_P^2} \right] \mathbf{y}_1
\end{aligned}$$

and noting

$$\begin{aligned}
& \left[ \frac{JK(\mathbf{D}_I - \mathbf{H}_1)}{\sigma_E^2 + JK\sigma_P^2} \right] V(\mathbf{y}_1) \\
&= \left[ \frac{JK(\mathbf{D}_I - \mathbf{H}_1)}{\sigma_E^2 + JK\sigma_P^2} \right] \frac{1}{JK} (\sigma_E^2 + JK\sigma_P^2) (\mathbf{D}_I - \mathbf{H}_1) \\
&= (\mathbf{D}_I - \mathbf{H}_1), \\
& \frac{1}{2} E(\mathbf{y}_1)' \left[ \frac{JK(\mathbf{D}_I - \mathbf{H}_1)}{\sigma_E^2 + JK\sigma_P^2} \right] (\mathbf{D}_I - \mathbf{H}_1) E(\mathbf{y}_1) \\
&= \frac{1}{2} \underline{\alpha}' \mathbf{X}' \mathbf{W}'_1 (\mathbf{D}_I - \mathbf{H}_1) \left[ \frac{JK(\mathbf{D}_I - \mathbf{H}_1)}{\sigma_E^2 + JK\sigma_P^2} \right] (\mathbf{D}_I - \mathbf{H}_1) \mathbf{W}_1 \mathbf{X} \underline{\alpha} \\
&= 0, \quad \text{and}
\end{aligned}$$

$$r(\mathbf{D}_I - \mathbf{H}_1) = I - 2.$$

By Theorem 7.3 in Searle(1987, p. 232),  $R_1/(\sigma_E^2 + JK\sigma_P^2)$  is a chi-squared random variable with  $I - 2$  degrees of freedom. ■

Theorem 2.2.2 : Under the distributional assumptions in (2.1.1),  $R_2/(\sigma_E^2 + IK\sigma_O^2)$  is a chi-squared random variable with  $J - 2$  degrees of freedom.

Proof : Multiplying (2.2.1) both sides of the equation on the left by  $(\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2$  yields that

$$\begin{aligned} (\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2\mathbf{y} &= (\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2\mathbf{X}\underline{\alpha} + (\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2\mathbf{Z}_1\mathbf{p} \quad (2.2.4) \\ &+ (\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2\mathbf{Z}_2\mathbf{o} + (\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2\mathbf{Z}_3\mathbf{e} \end{aligned}$$

where  $\mathbf{D}_J$  is an identity matrix of order  $J$ . Let  $(\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2\mathbf{y} = \mathbf{y}_2$ . Since

$$(\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2\mathbf{X} = (\mathbf{D}_J - \mathbf{H}_2)\mathbf{X}_2 = \mathbf{X}_2 - \mathbf{H}_2\mathbf{X}_2 = \mathbf{0},$$

$$\mathbf{W}_2\mathbf{Z}_1 = \frac{1}{IK}\mathbf{Z}_2'\mathbf{Z}_1 = \frac{1}{IK}K\underline{1}_J\underline{1}_I' = \frac{1}{I}\underline{1}_J\underline{1}_I',$$

$$\mathbf{W}_2\mathbf{Z}_2 = \frac{1}{IK}\mathbf{Z}_2'\mathbf{Z}_2 = \frac{1}{IK}IK\mathbf{D}_J = \mathbf{D}_J, \text{ and}$$

$$\mathbf{W}_2\mathbf{Z}_3 = \frac{1}{IK}\mathbf{Z}_2'\mathbf{Z}_3 = \frac{1}{IK}\mathbf{Z}_2',$$

(2.2.4) is written as

$$\mathbf{y}_2 = \frac{1}{I}(\mathbf{D}_J - \mathbf{H}_2)\underline{1}_J\underline{1}_I'\mathbf{p} + (\mathbf{D}_J - \mathbf{H}_2)\mathbf{o} + \frac{1}{IK}(\mathbf{D}_J - \mathbf{H}_2)\mathbf{Z}_2'\mathbf{e}.$$

Note that

$$\mathbf{Z}_2' \mathbf{Z}_2 = IK \mathbf{D}_J \text{ and}$$

$$\begin{aligned} (\mathbf{D}_J - \mathbf{H}_2) \mathbf{W}_2 \mathbf{Z}_1 \mathbf{Z}_1' \mathbf{W}_2' (\mathbf{D}_J - \mathbf{H}_2) &= (\mathbf{D}_J - \mathbf{H}_2) \frac{1}{I} \mathbf{1}_J \mathbf{1}_I' \frac{1}{I} \mathbf{1}_I \mathbf{1}_J' (\mathbf{D}_J - \mathbf{H}_2) \\ &= (\mathbf{D}_J - \mathbf{H}_2) \frac{1}{I^2} I \mathbf{1}_J \mathbf{1}_J' (\mathbf{D}_J - \mathbf{H}_2) \\ &= (\mathbf{D}_J - \mathbf{H}_2) \frac{1}{I} \mathbf{1}_J \mathbf{1}_J' (\mathbf{D}_J - \mathbf{H}_2) \\ &= \frac{1}{I} (\mathbf{D}_J - \mathbf{H}_2) \mathbf{1}_J [(\mathbf{D}_J - \mathbf{H}_2) \mathbf{1}_J]' \\ &= \frac{1}{I} \underline{0} \ \underline{0}' \\ &= \underline{0} \end{aligned}$$

since  $\mathbf{H}_2$  is an idempotent matrix and

$$\begin{aligned} (\mathbf{D}_J - \mathbf{H}_2) \mathbf{1}_J &= \mathbf{1}_J - \mathbf{X}_2 (\mathbf{X}_2' \mathbf{X}_2)^{-1} \mathbf{X}_2' \mathbf{1}_J \\ &= \mathbf{1}_J - \mathbf{1}_J \\ &= \underline{0}. \end{aligned}$$

The variance of  $\mathbf{y}_2$  is

$$\begin{aligned} V(\mathbf{y}_2) &= V\left(\frac{1}{I} (\mathbf{D}_J - \mathbf{H}_2) \mathbf{1}_J \mathbf{1}_I' \mathbf{p}\right) + V((\mathbf{D}_J - \mathbf{H}_2) \mathbf{o}) + V\left(\frac{1}{IK} (\mathbf{D}_J - \mathbf{H}_2) \mathbf{Z}_2' \mathbf{e}\right) \\ &= \sigma_O^2 (\mathbf{D}_J - \mathbf{H}_2) + \frac{1}{IK} \sigma_E^2 (\mathbf{D}_J - \mathbf{H}_2) \\ &= \frac{1}{IK} (\sigma_E^2 + IK \sigma_O^2) (\mathbf{D}_J - \mathbf{H}_2). \end{aligned}$$

The distribution of  $R_2$  is determined by writing

$$\begin{aligned}
& \frac{R_2}{\sigma_E^2 + IK\sigma_O^2} \\
&= \mathbf{y}'\mathbf{W}'_2(\mathbf{D}_J - \mathbf{H}_2) \left[ \frac{IK(\mathbf{D}_J - \mathbf{H}_2)}{\sigma_E^2 + IK\sigma_O^2} \right] (\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2\mathbf{y} \quad (2.2.5) \\
&= \mathbf{y}'_2 \left[ \frac{IK(\mathbf{D}_J - \mathbf{H}_2)}{\sigma_E^2 + IK\sigma_O^2} \right] \mathbf{y}_2
\end{aligned}$$

and noting

$$\begin{aligned}
& \left[ \frac{IK(\mathbf{D}_J - \mathbf{H}_2)}{\sigma_E^2 + IK\sigma_O^2} \right] V(\mathbf{y}_2) \\
&= \left[ \frac{IK(\mathbf{D}_J - \mathbf{H}_2)}{\sigma_E^2 + IK\sigma_O^2} \right] \frac{1}{IK} (\sigma_E^2 + IK\sigma_O^2) (\mathbf{D}_J - \mathbf{H}_2) \\
&= (\mathbf{D}_J - \mathbf{H}_2), \\
& \frac{1}{2} E(\mathbf{y}_2)' \left[ \frac{IK(\mathbf{D}_J - \mathbf{H}_2)}{\sigma_E^2 + IK\sigma_O^2} \right] E(\mathbf{y}_2) \\
&= \frac{1}{2} \underline{\alpha}' \mathbf{X}' \mathbf{W}'_2 (\mathbf{D}_J - \mathbf{H}_2) \left[ \frac{IK(\mathbf{D}_J - \mathbf{H}_2)}{\sigma_E^2 + IK\sigma_O^2} \right] (\mathbf{D}_J - \mathbf{H}_2) \mathbf{W}_2 \mathbf{X} \underline{\alpha} \\
&= 0, \quad \text{and}
\end{aligned}$$

$$r(\mathbf{D}_J - \mathbf{H}_2) = J - 2.$$

By Theorem 7.3 in Searle(1987, p. 232),  $R_2/(\sigma_E^2 + IK\sigma_O^2)$  is a chi-squared random variable with  $J - 2$  degrees of freedom. ■

Theorem 2.2.3 : Under the distributional assumptions in (2.1.1),  $R_3/\sigma_E^2$  is a chi-squared random variable with  $IJK - I - J$  degrees of freedom.

Proof : Multiplying (2.2.1) both sides of the equation on the left by  $(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3$  yields that

$$\begin{aligned} (\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{y} &= (\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{X}\underline{\alpha} + (\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{Z}_1\mathbf{p} \\ &\quad + (\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{Z}_2\mathbf{o} + (\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{Z}_3\mathbf{e}. \end{aligned}$$

It can be shown that

$$\begin{aligned} (\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{X} &= (\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{X} \\ &= \mathbf{X} - \mathbf{H}_3\mathbf{X} \\ &= \mathbf{0}, \\ \mathbf{H}_3\mathbf{W}_3\mathbf{Z}_1 &= \mathbf{Z}_1, \text{ and} \\ \mathbf{H}_3\mathbf{W}_3\mathbf{Z}_2 &= \mathbf{Z}_2 \end{aligned} \tag{2.2.6}$$

since

$$\begin{aligned} \mathbf{W}_3 &= \mathbf{Z}_3 = \mathbf{D}_{IJK}, \\ \mathbf{H}_3\mathbf{X} &= \mathbf{X}_3(\mathbf{X}_3'\mathbf{X}_3)^{-}\mathbf{X}_3'\mathbf{X} = \mathbf{X}, \\ \mathbf{H}_3\mathbf{Z}_1 &= \mathbf{X}_3(\mathbf{X}_3'\mathbf{X}_3)^{-}\mathbf{X}_3'\mathbf{Z}_1 = \mathbf{Z}_1, \text{ and} \\ \mathbf{H}_3\mathbf{Z}_2 &= \mathbf{X}_3(\mathbf{X}_3'\mathbf{X}_3)^{-}\mathbf{X}_3'\mathbf{Z}_2 = \mathbf{Z}_2. \end{aligned}$$

Let  $(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{y} = \mathbf{y}_3$ . The variance of  $\mathbf{y}_3$  is

$$\begin{aligned} V(\mathbf{y}_3) &= V((\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{X}\underline{\alpha}) + V((\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{Z}_1\mathbf{p}) \\ &\quad + V((\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{Z}_2\mathbf{o}) + V((\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3\mathbf{Z}_3\mathbf{e}) \\ &= V((\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{Z}_3\mathbf{e}) \\ &= \sigma_E^2(\mathbf{D}_{IJK} - \mathbf{H}_3). \end{aligned}$$



The distribution of  $R_3$  is determined by writing

$$\begin{aligned}\frac{R_3}{\sigma_E^2} &= \mathbf{y}' \mathbf{W}'_3 (\mathbf{D}_{IJK} - \mathbf{H}_3) \left[ \frac{(\mathbf{D}_{IJK} - \mathbf{H}_3)}{\sigma_E^2} \right] (\mathbf{D}_{IJK} - \mathbf{H}_3) \mathbf{W}_3 \mathbf{y} \quad (2.2.7) \\ &= \mathbf{y}'_3 \left[ \frac{(\mathbf{D}_{IJK} - \mathbf{H}_3)}{\sigma_E^2} \right] \mathbf{y}_3\end{aligned}$$

and noting

$$\begin{aligned}& \left[ \frac{(\mathbf{D}_{IJK} - \mathbf{H}_3)}{\sigma_E^2} \right] V(\mathbf{y}_3) \\ &= \left[ \frac{(\mathbf{D}_{IJK} - \mathbf{H}_3)}{\sigma_E^2} \right] \sigma_E^2 (\mathbf{D}_{IJK} - \mathbf{H}_3) \\ &= \mathbf{D}_{IJK} - \mathbf{H}_3, \\ & \frac{1}{2} E(\mathbf{y}_3)' \left[ \frac{(\mathbf{D}_{IJK} - \mathbf{H}_3)}{\sigma_E^2} \right] E(\mathbf{y}_3) \\ &= \frac{1}{2} \underline{\alpha}' \mathbf{X}' \mathbf{W}'_3 (\mathbf{D}_{IJK} - \mathbf{H}_3) \left[ \frac{(\mathbf{D}_{IJK} - \mathbf{H}_3)}{\sigma_E^2} \right] (\mathbf{D}_{IJK} - \mathbf{H}_3) \mathbf{W}_3 \mathbf{X} \underline{\alpha} \\ &= 0, \quad \text{and}\end{aligned}$$

$$r(\mathbf{D}_{IJK} - \mathbf{H}_3) = IJK - I - J.$$

By Theorem 7.3 in Searle(1987, p. 232),  $R_3/\sigma_E^2$  is a chi-squared random variable with  $IKJ - I - J$  degrees of freedom. ■

Theorem 2.2.4 : Under the distributional assumptions in (2.1.1),  $R_1/(\sigma_E^2 + JK\sigma_P^2)$  and  $R_3/\sigma_E^2$  are independent and  $R_2/(\sigma_E^2 + IK\sigma_O^2)$  and  $R_3/\sigma_E^2$  are independent.

Proof : It can be shown from (2.2.3) and (2.2.7) that

$$\begin{aligned}
& \mathbf{W}'_1(\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1 V(\mathbf{y})\mathbf{W}'_3(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3 \\
&= \sigma_P^2 \mathbf{W}'_1(\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1 \mathbf{Z}_1 \mathbf{Z}'_1 \mathbf{W}'_3(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3 \\
&\quad + \sigma_O^2 \mathbf{W}'_1(\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1 \mathbf{Z}_2 \mathbf{Z}'_2 \mathbf{W}'_3(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3 \\
&\quad + \sigma_E^2 \mathbf{W}'_1(\mathbf{D}_I - \mathbf{H}_1)\mathbf{W}_1 \mathbf{Z}_3 \mathbf{Z}'_3 \mathbf{W}'_3(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3 \\
&= \mathbf{0}
\end{aligned}$$

since

$$\begin{aligned}
\mathbf{Z}'_1 \mathbf{W}'_3(\mathbf{D}_{IJK} - \mathbf{H}_3) &= \mathbf{Z}'_1 - \mathbf{Z}'_1 \mathbf{H}_3 \\
&= \mathbf{Z}'_1 - \mathbf{Z}'_1 \\
&= \mathbf{0}, \\
\mathbf{Z}'_2 \mathbf{W}'_3(\mathbf{D}_{IJK} - \mathbf{H}_3) &= \mathbf{Z}'_2 - \mathbf{Z}'_2 \mathbf{H}_3 \\
&= \mathbf{Z}'_2 - \mathbf{Z}'_2 \\
&= \mathbf{0}, \quad \text{and} \\
\mathbf{W}_1 \mathbf{Z}_3 \mathbf{Z}'_3 \mathbf{W}'_3(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3 &= \mathbf{W}_1(\mathbf{D}_{IJK} - \mathbf{H}_3) \\
&= \frac{1}{JK} \mathbf{Z}'_1(\mathbf{D}_{IJK} - \mathbf{H}_3) \\
&= \frac{1}{JK} (\mathbf{Z}'_1 - \mathbf{Z}'_1 \mathbf{H}_3) \\
&= \frac{1}{JK} (\mathbf{Z}'_1 - \mathbf{Z}'_1) \\
&= \mathbf{0}.
\end{aligned}$$

By Theorem 7.4 in Searle(1987, p. 232),  $R_1/(\sigma_E^2 + JK\sigma_P^2)$  and  $R_3/\sigma_E^2$  are independent.

Similarly, it can be shown from (2.2.5) and (2.2.7) that

$$\begin{aligned}
& \mathbf{W}_2'(\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2 V(\mathbf{y})\mathbf{W}_3'(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3 \\
&= \sigma_P^2 \mathbf{W}_2'(\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2 \mathbf{Z}_1 \mathbf{Z}_1' \mathbf{W}_3'(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3 \\
&\quad + \sigma_O^2 \mathbf{W}_2'(\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2 \mathbf{Z}_2 \mathbf{Z}_2' \mathbf{W}_3'(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3 \\
&\quad + \sigma_E^2 \mathbf{W}_2'(\mathbf{D}_J - \mathbf{H}_2)\mathbf{W}_2 \mathbf{Z}_3 \mathbf{Z}_3' \mathbf{W}_3'(\mathbf{D}_{IJK} - \mathbf{H}_3)\mathbf{W}_3 \\
&= \mathbf{0}.
\end{aligned}$$

By Theorem 7.4 in Searle(1987, p. 232),  $R_2/(\sigma_E^2 + IK\sigma_O^2)$  and  $R_3/\sigma_E^2$  are independent. ■

Using the results of Theorems 2.2, the expected mean squares are

$$E(S_P^2) = \sigma_E^2 + JK\sigma_P^2 = \theta_P, \quad (2.2.8a)$$

$$E(S_O^2) = \sigma_E^2 + IK\sigma_O^2 = \theta_O, \text{ and } (2.2.8b)$$

$$E(S_E^2) = \sigma_E^2 = \theta_E. \quad (2.2.8c)$$

### 2.3 Confidence Intervals on Variance Components Using Ting et al. Method

We use the distributional results of Section 2.2 to construct confidence intervals on  $\sigma_P^2$ ,  $\sigma_O^2$ , and  $\sigma_E^2$ . Since  $R_3/\sigma_E^2 \sim \chi_{IJK-I-J}^2$ , an exact confidence interval on  $\sigma_E^2$  is obtained. An exact  $100(1 - \alpha)\%$  two-sided confidence interval on  $\sigma_E^2$  is

$$\left[ \frac{S_E^2}{F_{(\alpha/2: IJK-I-J, \infty)}} \quad ; \quad \frac{S_E^2}{F_{(1-\alpha/2: IJK-I-J, \infty)}} \right] \quad (2.3.1)$$

where  $F_{(\delta: \nu_1, \nu_2)}$  is the  $F$ -value for  $\nu_1$  and  $\nu_2$  degrees of freedom with  $\delta$  area to the right.

The variance component of  $\sigma_P^2$  can be represented by (2.2.8)

$$\sigma_P^2 = \frac{\theta_P - \theta_E}{JK}. \quad (2.3.2)$$

Ting, Burdick, Graybill, Jeyaratnam, and Lu (1990) proposed a general method for constructing confidence intervals on  $\gamma = \sum_{q=1}^P c_q \theta_q - \sum_{r=1}^Q c_r \theta_r$  where  $c_q, c_r \geq 0$ , and the sign of  $\gamma$  is unknown. The intervals are extended to the general cases where  $Q, P > 2$ . Their two-sided intervals are very close to the stated confidence coefficients. Thus a confidence interval on  $\sigma_P^2$  can be constructed using the method of Ting et al.(1990). An approximate  $100(1 - \alpha)\%$  two-sided confidence interval on  $\sigma_P^2$  is

$$\begin{aligned} \frac{1}{JK} [ S_P^2 - S_E^2 - (G_1^2 S_P^4 + H_2^2 S_E^4 + G_{12} S_P^2 S_E^2)^{\frac{1}{2}} \quad ; \\ S_P^2 - S_E^2 + (H_1^2 S_P^4 + G_2^2 S_E^4 + H_{12} S_P^2 S_E^2)^{\frac{1}{2}} ] \end{aligned} \quad (2.3.3)$$

where

$$G_1 = 1 - \frac{1}{F_{(\frac{\alpha}{2}:I-2,\infty)}},$$

$$H_2 = \frac{1}{F_{(1-\frac{\alpha}{2}:IJK-I-J,\infty)}} - 1,$$

$$G_{12} = \frac{(F_1 - 1)^2 - G_1^2 F_1^2 - H_2^2}{F_1},$$

$$H_1 = \frac{1}{F_{(1-\frac{\alpha}{2}:I-2,\infty)}} - 1,$$

$$G_2 = 1 - \frac{1}{F_{(\frac{\alpha}{2}:IJK-I-J,\infty)}},$$

$$H_{12} = \frac{(1 - F_2)^2 - H_1^2 F_2^2 - G_2^2}{F_2},$$

$$F_1 = F_{(\frac{\alpha}{2}:I-2,IJK-I-J)}, \quad \text{and}$$

$$F_2 = F_{(1-\frac{\alpha}{2}:I-2,IJK-I-J)}.$$

Since  $\sigma_P^2 > 0$ , any negative bound is defined to be zero. The variance component of  $\sigma_O^2$  can be represented by (2.2.8)

$$\sigma_O^2 = \frac{\theta_O - \theta_E}{IK}. \quad (2.3.4)$$

The same Ting et al. method can be applied to form a confidence interval on  $\sigma_O^2$ . In particular, an approximate  $100(1 - \alpha)\%$  two-sided confidence interval on  $\sigma_O^2$  is

$$\begin{aligned} & \frac{1}{IK} [ S_O^2 - S_E^2 - (G_3^2 S_O^4 + H_4^2 S_E^4 + G_{34} S_O^2 S_E^2)^{\frac{1}{2}} ; \\ & S_O^2 - S_E^2 + (H_3^2 S_O^4 + G_4^2 S_E^4 + H_{34} S_O^2 S_E^2)^{\frac{1}{2}} ] \end{aligned} \quad (2.3.5)$$

where

$$\begin{aligned} G_3 &= 1 - \frac{1}{F_{(\frac{\alpha}{2}:J-2,\infty)}}, \\ H_4 &= \frac{1}{F_{(1-\frac{\alpha}{2}:IJK-I-J,\infty)}} - 1 = H_2, \\ G_{34} &= \frac{(F_3 - 1)^2 - G_3^2 F_3^2 - H_4^2}{F_3}, \\ H_3 &= \frac{1}{F_{(1-\frac{\alpha}{2}:J-2,\infty)}} - 1, \\ G_4 &= 1 - \frac{1}{F_{(\frac{\alpha}{2}:IJK-I-J,\infty)}} = G_2, \\ H_{34} &= \frac{(1 - F_4)^2 - H_3^2 F_4^2 - G_4^2}{F_4}, \\ F_3 &= F_{(\frac{\alpha}{2}:J-2,IJK-I-J)}, \quad \text{and} \\ F_4 &= F_{(1-\frac{\alpha}{2}:J-2,IJK-I-J)}. \end{aligned}$$

TING method refers to confidence intervals using (2.3.3) and (2.3.5).

## 2.4 Generalized Confidence Intervals on Variance Components

Tsui and Weerahandi(1989) introduced the concept on generalized inference for testing hypotheses in situations where exact method do not exist. Their method can be applied to form approximate confidence intervals on variance components. Since an exact  $100(1 - \alpha)\%$  two-sided confidence interval on  $\sigma_E^2$  exists, we focus on constructing confidence intervals on  $\sigma_P^2$  and  $\sigma_O^2$ . Since  $R_1/(\sigma_E^2 + JK\sigma_P^2) \sim \chi_{I-2}^2$ ,  $\sigma_P^2$  can be written as a generalized pivotal quantity as follows:

$$\sigma_P^2 = \frac{1}{JK} \left[ \frac{(I-2)}{P^*} s_P^2 - \frac{(IJK - I - J)}{E^*} s_E^2 \right] \quad (2.4.1)$$

where  $s_P^2$  and  $s_E^2$  are, respectively, observed values of  $S_P^2$  and  $S_E^2$ ,  $P^* = (I - 2)S_P^2/(\sigma_E^2 + JK\sigma_P^2)$ , and  $E^* = (IJK - I - J)S_E^2/\sigma_E^2$ . Define  $R_P$  as the solution for  $\sigma_P^2$ . The distribution of  $R_P$  is completely determined by  $P^*$  and  $E^*$ . An approximate  $100(1 - \alpha)\%$  two-sided confidence interval on  $\sigma_P^2$  is

$$\left[ R_{P_{(\frac{\alpha}{2})}} ; R_{P_{(\frac{1-\alpha}{2})}} \right] \quad (2.4.2)$$

where  $R_{P_{(\frac{\alpha}{2})}}$  and  $R_{P_{(\frac{1-\alpha}{2})}}$  are the percentile of  $\alpha/2$  and  $1 - \alpha/2$  of the distribution  $R_P$ , respectively.

Similarly, we can form confidence intervals on  $\sigma_O^2$  using generalized pivotal quantity. Since  $R_2/(\sigma_E^2 + IK\sigma_O^2) \sim \chi_{J-2}^2$ ,  $\sigma_O^2$  can be written as a generalized pivotal quantity as follows:

$$\sigma_O^2 = \frac{1}{IK} \left[ \frac{(J-2)}{O^*} s_O^2 - \frac{(IJK - I - J)}{E^*} s_E^2 \right] \quad (2.4.3)$$

where  $s_O^2$  is an observed value of  $S_O^2$  and  $O^* = (J-2)S_O^2/(\sigma_E^2 + IK\sigma_O^2)$ . Define  $R_O$  as the solution for  $\sigma_O^2$ . The distribution of  $R_O$  is completely determined by  $O^*$  and  $E^*$ . An approximate  $100(1-\alpha)\%$  two-sided confidence interval on  $\sigma_O^2$  is

$$\left[ R_{O_{(\frac{\alpha}{2})}} \quad ; \quad R_{O_{(\frac{1-\alpha}{2})}} \right] \quad (2.4.4)$$

where  $R_{O_{(\frac{\alpha}{2})}}$  and  $R_{O_{(\frac{1-\alpha}{2})}}$  are the percentile of  $\alpha/2$  and  $1-\alpha/2$  of the distribution  $R_O$ , respectively. The GEN method refers to confidence intervals using (2.4.2) and (2.4.4).





## 2.5 Confidence Intervals on Variance Components Using SAS PROC MIXED Procedure

SAS PROC MIXED procedure can be employed to fit a variety of mixed linear models to data. It enables one to use these fitted models to make statistical inferences about data. PROC MIXED is a generalization of the GLM procedure in the sense that PROC GLM fits standard linear models and PROC MIXED fits wider class of mixed linear models. PROC MIXED fits the data using the method of restricted maximum likelihood(REML), also known as residual maximum likelihood. The procedure permits one to exhibit asymptotic covariances among variance components by using options of MIXED procedure.

In order to form confidence intervals on  $\sigma_P^2$  and  $\sigma_O^2$  using REML estimator, a PROC MIXED statement such as TABLE 2.5.1. can be performed.

**TABLE 2.5.1 An Example Statement of PROC MIXED**

```
PROC MIXED DATA=EXAMPLE ASYCOV CL ALPHA=0.10 ;  
CLASSES SIGMAP SIGMAO;  
MODEL Y = X;  
RANDOM SIGMAP SIGMAO;
```

where EXAMPLE is a data set name, ASYCOV requests asymptotic covariances among variance components, and CL and ALPHA=0.10 produce 90 % confidence intervals using REML estimators of  $\sigma_P^2$  and  $\sigma_O^2$ . CLASSES SIGMAP SIGMAO names classification variables and RANCOM SIGMAP SIGMAO defines random effects in this model.

As a result of executing PROC MIXED, an approximate confidence interval on  $\sigma_P^2$  is obtained using Wald Statistics. The interval is computed as

$$\left[ \frac{\hat{\sigma}_P^2}{F_{(1-\alpha/2;\nu,\infty)}} ; \frac{\hat{\sigma}_P^2}{F_{(\alpha/2;\nu,\infty)}} \right] \quad (2.5.1)$$

where  $\hat{\sigma}_P^2$  is the REML estimate of  $\sigma_P^2$ ,  $\nu = 2Z^2$ ,  $Z$  is the Wald Z score,

$$Z = \frac{\hat{\sigma}_P^2}{S.E.(\hat{\sigma}_P^2)}, \quad (2.5.2)$$

and  $S.E.$  stands for standard error.

Similarly, an approximate confidence interval on  $\sigma_O^2$  is obtained using Wald Statistics. The interval is computed as

$$\left[ \frac{\hat{\sigma}_O^2}{F_{(1-\alpha/2;\nu,\infty)}} ; \frac{\hat{\sigma}_O^2}{F_{(\alpha/2;\nu,\infty)}} \right] \quad (2.5.3)$$

where  $\hat{\sigma}_O^2$  is the REML estimate of  $\sigma_O^2$ ,  $\nu = 2Z^2$ , and  $Z$  is the Wald Z score.

MIXED method refers to confidence intervals using (2.5.1) and (2.5.3).

### 3. SIMULATION AND CONCLUSION

#### 3.1 Simulation Study

We compare the confidence intervals on variance components proposed from Sections 2.3 to 2.5. Computer simulation is used to compare the confidence coefficients and expected interval lengths. The criteria for analyzing the performance of the methods are: i) their ability to obtain stated confidence coefficients, and ii) the average length of two-sided confidence intervals. Although shorter average lengths are preferable, it is necessary that the methods maintain the stated confidence coefficients. Dolezal et al.(1998) used eight designs with several combinations of  $I$ ,  $J$ , and  $K$  for two-factor R & R study with fixed operators. Four more designs are added to their designs and the designs shown in Table 3.1.1 are used for simulation study.

**TABLE 3.1.1 Eight Designs Used in Simulation Study**

| $I$ | $J$ | $K$ | $I$ | $J$ | $K$ | $I$ | $J$ | $K$ |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 6   | 3   | 2   | 12  | 3   | 2   | 24  | 3   | 2   |
| 6   | 3   | 4   | 12  | 3   | 4   | 24  | 3   | 4   |
| 6   | 6   | 2   | 12  | 6   | 2   | 24  | 6   | 2   |
| 6   | 6   | 4   | 12  | 6   | 4   | 24  | 6   | 4   |

Let  $\rho = \frac{\sigma_P^2}{\sigma_P^2 + \sigma_O^2 + \sigma_E^2}$ . Without loss of generality  $\sigma_P^2 = 1 - \sigma_O^2 - \sigma_E^2$ . The values of  $\sigma_P^2$  and  $\sigma_O^2$  are varied from 0.1 to 0.8 in increments of 0.1. In particular, the values used in this study are presented in Table 3.1.2

**TABLE 3.1.2 Parameter Values Used in Simulation Study**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 0.1          | 0.1          | 0.8          | 0.2          | 0.5          | 0.3          | 0.4          | 0.4          | 0.2          |
| 0.1          | 0.2          | 0.7          | 0.2          | 0.6          | 0.2          | 0.4          | 0.5          | 0.1          |
| 0.1          | 0.3          | 0.6          | 0.2          | 0.7          | 0.1          | 0.5          | 0.1          | 0.4          |
| 0.1          | 0.4          | 0.5          | 0.3          | 0.1          | 0.6          | 0.5          | 0.2          | 0.3          |
| 0.1          | 0.5          | 0.4          | 0.3          | 0.2          | 0.5          | 0.5          | 0.3          | 0.2          |
| 0.1          | 0.6          | 0.3          | 0.3          | 0.3          | 0.4          | 0.5          | 0.4          | 0.1          |
| 0.1          | 0.7          | 0.2          | 0.3          | 0.4          | 0.3          | 0.6          | 0.1          | 0.3          |
| 0.1          | 0.8          | 0.1          | 0.3          | 0.5          | 0.2          | 0.6          | 0.2          | 0.2          |
| 0.2          | 0.1          | 0.7          | 0.3          | 0.6          | 0.1          | 0.6          | 0.3          | 0.1          |
| 0.2          | 0.2          | 0.6          | 0.4          | 0.1          | 0.5          | 0.7          | 0.1          | 0.2          |
| 0.2          | 0.3          | 0.5          | 0.4          | 0.2          | 0.4          | 0.7          | 0.2          | 0.1          |
| 0.2          | 0.4          | 0.4          | 0.4          | 0.3          | 0.3          | 0.8          | 0.1          | 0.1          |

36 combinations of  $\sigma_P^2$ ,  $\sigma_O^2$ , and  $\sigma_E^2$  in Table 3.1.2 are simulated for 2000 times for each design in Table 3.1.1. Simulated values for  $S_P^2$ ,  $S_O^2$ , and  $S_E^2$  are substituted into TING, GEN, and MIXED methods in Section 2.3 to 2.5 and the intervals are computed. Confidence coefficients are determined by counting the number of the intervals that contain the parameters. Using the normal approximation to the binomial, if the true confidence coefficient is 0.90, there is less than a 2.5 % chance that an estimated confidence coefficient based on 2000 replications will be less than 0.8866. The average lengths of the two-sided confidence intervals are calculated.

### 3.2 Simulation Results

Tables 3.2.1 to 3.2.12 and Tables 3.2.13 to 3.2.24 present simulated confidence coefficients for stated two-sided 90% confidence intervals on  $\sigma_P^2$  and  $\sigma_O^2$ , respectively. Tables 3.2.25 to 3.2.36 and Tables 3.2.37 to 3.2.48 report average confidence interval lengths for stated two-sided 90% confidence intervals on  $\sigma_P^2$  and  $\sigma_O^2$ , respectively. Figures 3.2.1 and 3.2.2 show boxplots for simulated confidence coefficients for stated two-sided 90% confidence intervals on  $\sigma_P^2$  and  $\sigma_O^2$ , respectively. Figures 3.2.3 and 3.2.4 show boxplots for average confidence interval lengths for stated two-sided 90% confidence intervals on  $\sigma_P^2$  and  $\sigma_O^2$ , respectively. The boxplots for MIXED method were not presented because it generates too much wide average confidence interval lengths when PROC MIXED executes using the data generated by random numbers for 2000 times in simulation study.

It is known from Figures 3.2.1 that TING and GEN methods for confidence intervals on  $\sigma_P^2$  generally maintain the stated confidence coefficients for all combinations of  $I$ ,  $J$ , and  $K$ . However, MIXED method in general generates conservative confidence intervals, comparing with TING and GEN. The performance of MIXED slightly improves as  $J$  and  $K$  increase. MIXED dramatically performs better especially as  $I$  increases. MIXED produces slightly larger simulated confidence coefficients than TING and GEN especially for  $I = 24$ ,  $J = 6$ , and  $K = 4$ . This is because MIXED uses Wald Z statistics in computing confidence intervals which is valid for large samples.

From Figures 3.2.2 simulated confidence coefficients for  $\sigma_O^2$  show similar trend to ones for  $\sigma_P^2$ . It is known from Figures 3.2.2 that TING and GEN methods for confidence intervals on  $\sigma_O^2$  generally maintain the stated confidence coefficients

for all combinations of  $I$ ,  $J$ , and  $K$ . However, MIXED method in general generates conservative confidence intervals, comparing with TING and GEN. The performance of MIXED slightly improves as  $J$  and  $K$  increase.

It can be noticed from Figures 3.2.3 and 3.2.4 that TING and GEN methods for average confidence interval lengths on  $\sigma_P^2$  and  $\sigma_O^2$  are very similar to each other for all combinations of  $I$ ,  $J$ , and  $K$ . MIXED method was eliminated since it produces too much wide average confidence interval lengths.



**TABLE 3.2.1 Range of Simulated Confidence**  
**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 6$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9070 | 0.9010 | 0.7872 | 0.3          | 0.5          | 0.2          | 0.8880 | 0.9015 | 0.9446 |
| 0.1          | 0.2          | 0.7          | 0.9060 | 0.8945 | 0.8170 | 0.3          | 0.6          | 0.1          | 0.8945 | 0.9040 | 0.9449 |
| 0.1          | 0.3          | 0.6          | 0.9135 | 0.9065 | 0.8653 | 0.4          | 0.1          | 0.5          | 0.8940 | 0.8915 | 0.9335 |
| 0.1          | 0.4          | 0.5          | 0.9035 | 0.9020 | 0.8577 | 0.4          | 0.2          | 0.4          | 0.9045 | 0.9100 | 0.9410 |
| 0.1          | 0.5          | 0.4          | 0.8990 | 0.9085 | 0.8663 | 0.4          | 0.3          | 0.3          | 0.8985 | 0.9055 | 0.9415 |
| 0.1          | 0.6          | 0.3          | 0.8935 | 0.8960 | 0.8926 | 0.4          | 0.4          | 0.2          | 0.9025 | 0.9065 | 0.9406 |
| 0.1          | 0.7          | 0.2          | 0.9065 | 0.9015 | 0.9269 | 0.4          | 0.5          | 0.1          | 0.8895 | 0.9030 | 0.9328 |
| 0.1          | 0.8          | 0.1          | 0.8910 | 0.9055 | 0.9303 | 0.5          | 0.1          | 0.4          | 0.9010 | 0.9080 | 0.9509 |
| 0.2          | 0.1          | 0.7          | 0.8995 | 0.9135 | 0.8924 | 0.5          | 0.2          | 0.3          | 0.8945 | 0.8960 | 0.9406 |
| 0.2          | 0.2          | 0.6          | 0.9125 | 0.9025 | 0.8894 | 0.5          | 0.3          | 0.2          | 0.8985 | 0.9025 | 0.9477 |
| 0.2          | 0.3          | 0.5          | 0.9025 | 0.9130 | 0.9149 | 0.5          | 0.4          | 0.1          | 0.8980 | 0.9070 | 0.9379 |
| 0.2          | 0.4          | 0.4          | 0.9075 | 0.9025 | 0.9150 | 0.6          | 0.1          | 0.3          | 0.9155 | 0.9055 | 0.9518 |
| 0.2          | 0.5          | 0.3          | 0.9085 | 0.8930 | 0.9298 | 0.6          | 0.2          | 0.2          | 0.8935 | 0.9055 | 0.9453 |
| 0.2          | 0.6          | 0.2          | 0.9000 | 0.9010 | 0.9301 | 0.6          | 0.3          | 0.1          | 0.8915 | 0.8990 | 0.9170 |
| 0.2          | 0.7          | 0.1          | 0.8945 | 0.8930 | 0.9437 | 0.7          | 0.1          | 0.2          | 0.8980 | 0.9005 | 0.9435 |
| 0.3          | 0.1          | 0.6          | 0.9035 | 0.9075 | 0.9178 | 0.7          | 0.2          | 0.1          | 0.8985 | 0.8945 | 0.9095 |
| 0.3          | 0.2          | 0.5          | 0.8920 | 0.8985 | 0.9238 | 0.8          | 0.1          | 0.1          | 0.8900 | 0.9100 | 0.9130 |
| 0.3          | 0.3          | 0.4          | 0.9025 | 0.9060 | 0.9332 | MAX          |              |              | 0.9155 | 0.9135 | 0.9518 |
| 0.3          | 0.4          | 0.3          | 0.8995 | 0.9025 | 0.9279 | MIN          |              |              | 0.8880 | 0.8915 | 0.7872 |

**TABLE 3.2.2 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 6$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9000 | 0.8950 | 0.8736 | 0.3          | 0.5          | 0.2          | 0.9000 | 0.8940 | 0.9469 |
| 0.1          | 0.2          | 0.7          | 0.9090 | 0.8930 | 0.8866 | 0.3          | 0.6          | 0.1          | 0.9090 | 0.9020 | 0.9244 |
| 0.1          | 0.3          | 0.6          | 0.8985 | 0.9005 | 0.9070 | 0.4          | 0.1          | 0.5          | 0.9015 | 0.9100 | 0.9411 |
| 0.1          | 0.4          | 0.5          | 0.9060 | 0.8925 | 0.9092 | 0.4          | 0.2          | 0.4          | 0.9085 | 0.8985 | 0.9483 |
| 0.1          | 0.5          | 0.4          | 0.9045 | 0.9035 | 0.9180 | 0.4          | 0.3          | 0.3          | 0.8960 | 0.9025 | 0.9464 |
| 0.1          | 0.6          | 0.3          | 0.8990 | 0.8940 | 0.9258 | 0.4          | 0.4          | 0.2          | 0.8930 | 0.8955 | 0.9434 |
| 0.1          | 0.7          | 0.2          | 0.8965 | 0.8940 | 0.9324 | 0.4          | 0.5          | 0.1          | 0.8990 | 0.8955 | 0.9180 |
| 0.1          | 0.8          | 0.1          | 0.8915 | 0.9030 | 0.9398 | 0.5          | 0.1          | 0.4          | 0.9055 | 0.8990 | 0.9423 |
| 0.2          | 0.1          | 0.7          | 0.9010 | 0.9030 | 0.9253 | 0.5          | 0.2          | 0.3          | 0.8990 | 0.8875 | 0.9429 |
| 0.2          | 0.2          | 0.6          | 0.8995 | 0.8940 | 0.9319 | 0.5          | 0.3          | 0.2          | 0.8965 | 0.8990 | 0.9340 |
| 0.2          | 0.3          | 0.5          | 0.8985 | 0.9145 | 0.9329 | 0.5          | 0.4          | 0.1          | 0.9180 | 0.8980 | 0.9065 |
| 0.2          | 0.4          | 0.4          | 0.9090 | 0.9095 | 0.9338 | 0.6          | 0.1          | 0.3          | 0.9050 | 0.9005 | 0.9409 |
| 0.2          | 0.5          | 0.3          | 0.8955 | 0.9060 | 0.9396 | 0.6          | 0.2          | 0.2          | 0.9065 | 0.8940 | 0.9290 |
| 0.2          | 0.6          | 0.2          | 0.9015 | 0.9080 | 0.9412 | 0.6          | 0.3          | 0.1          | 0.9110 | 0.9115 | 0.9145 |
| 0.2          | 0.7          | 0.1          | 0.9040 | 0.9090 | 0.9414 | 0.7          | 0.1          | 0.2          | 0.9055 | 0.8880 | 0.9260 |
| 0.3          | 0.1          | 0.6          | 0.8975 | 0.8975 | 0.9369 | 0.7          | 0.2          | 0.1          | 0.9060 | 0.9045 | 0.8975 |
| 0.3          | 0.2          | 0.5          | 0.8945 | 0.8965 | 0.9316 | 0.8          | 0.1          | 0.1          | 0.9045 | 0.8995 | 0.8945 |
| 0.3          | 0.3          | 0.4          | 0.9005 | 0.8995 | 0.9411 | MAX          |              |              | 0.9180 | 0.9145 | 0.9483 |
| 0.3          | 0.4          | 0.3          | 0.9045 | 0.9070 | 0.9373 | MIN          |              |              | 0.8915 | 0.8875 | 0.8736 |



**TABLE 3.2.3 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 6$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8975 | 0.8995 | 0.8836 | 0.3          | 0.5          | 0.2          | 0.9070 | 0.9045 | 0.9474 |
| 0.1          | 0.2          | 0.7          | 0.9005 | 0.9165 | 0.8916 | 0.3          | 0.6          | 0.1          | 0.9070 | 0.9140 | 0.9355 |
| 0.1          | 0.3          | 0.6          | 0.9020 | 0.9080 | 0.8997 | 0.4          | 0.1          | 0.5          | 0.9030 | 0.8960 | 0.9349 |
| 0.1          | 0.4          | 0.5          | 0.8925 | 0.9085 | 0.9147 | 0.4          | 0.2          | 0.4          | 0.8925 | 0.8985 | 0.9487 |
| 0.1          | 0.5          | 0.4          | 0.8960 | 0.9070 | 0.9177 | 0.4          | 0.3          | 0.3          | 0.9075 | 0.9010 | 0.9538 |
| 0.1          | 0.6          | 0.3          | 0.8890 | 0.8965 | 0.9294 | 0.4          | 0.4          | 0.2          | 0.9070 | 0.8845 | 0.9355 |
| 0.1          | 0.7          | 0.2          | 0.9150 | 0.8900 | 0.9327 | 0.4          | 0.5          | 0.1          | 0.9005 | 0.8925 | 0.9205 |
| 0.1          | 0.8          | 0.1          | 0.9015 | 0.9000 | 0.9443 | 0.5          | 0.1          | 0.4          | 0.8970 | 0.9135 | 0.9402 |
| 0.2          | 0.1          | 0.7          | 0.9010 | 0.9000 | 0.9207 | 0.5          | 0.2          | 0.3          | 0.9125 | 0.8965 | 0.9489 |
| 0.2          | 0.2          | 0.6          | 0.8860 | 0.9045 | 0.9247 | 0.5          | 0.3          | 0.2          | 0.8995 | 0.8920 | 0.9439 |
| 0.2          | 0.3          | 0.5          | 0.9065 | 0.8910 | 0.9337 | 0.5          | 0.4          | 0.1          | 0.9035 | 0.8895 | 0.9180 |
| 0.2          | 0.4          | 0.4          | 0.9000 | 0.9045 | 0.9354 | 0.6          | 0.1          | 0.3          | 0.8995 | 0.9075 | 0.9474 |
| 0.2          | 0.5          | 0.3          | 0.8885 | 0.8950 | 0.9406 | 0.6          | 0.2          | 0.2          | 0.9145 | 0.9060 | 0.9385 |
| 0.2          | 0.6          | 0.2          | 0.8980 | 0.9025 | 0.9487 | 0.6          | 0.3          | 0.1          | 0.9020 | 0.8980 | 0.9065 |
| 0.2          | 0.7          | 0.1          | 0.9045 | 0.9065 | 0.9394 | 0.7          | 0.1          | 0.2          | 0.9000 | 0.9025 | 0.9095 |
| 0.3          | 0.1          | 0.6          | 0.8985 | 0.9045 | 0.9290 | 0.7          | 0.2          | 0.1          | 0.8995 | 0.8910 | 0.9030 |
| 0.3          | 0.2          | 0.5          | 0.8910 | 0.8920 | 0.9377 | 0.8          | 0.1          | 0.1          | 0.8980 | 0.9060 | 0.9145 |
| 0.3          | 0.3          | 0.4          | 0.9015 | 0.8955 | 0.9428 | MAX          |              |              | 0.9150 | 0.9165 | 0.9538 |
| 0.3          | 0.4          | 0.3          | 0.8890 | 0.9045 | 0.9417 | MIN          |              |              | 0.8860 | 0.8845 | 0.8836 |

**TABLE 3.2.4 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 6$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8920 | 0.8965 | 0.9227 | 0.3          | 0.5          | 0.2          | 0.8900 | 0.8890 | 0.9205 |
| 0.1          | 0.2          | 0.7          | 0.9095 | 0.8860 | 0.9242 | 0.3          | 0.6          | 0.1          | 0.8965 | 0.8985 | 0.9019 |
| 0.1          | 0.3          | 0.6          | 0.9065 | 0.8990 | 0.9297 | 0.4          | 0.1          | 0.5          | 0.9015 | 0.9100 | 0.9409 |
| 0.1          | 0.4          | 0.5          | 0.8975 | 0.8990 | 0.9285 | 0.4          | 0.2          | 0.4          | 0.9040 | 0.8995 | 0.9479 |
| 0.1          | 0.5          | 0.4          | 0.8970 | 0.8870 | 0.9390 | 0.4          | 0.3          | 0.3          | 0.8995 | 0.9115 | 0.9219 |
| 0.1          | 0.6          | 0.3          | 0.8985 | 0.8975 | 0.9464 | 0.4          | 0.4          | 0.2          | 0.9010 | 0.9115 | 0.9130 |
| 0.1          | 0.7          | 0.2          | 0.9010 | 0.8970 | 0.9424 | 0.4          | 0.5          | 0.1          | 0.8980 | 0.9030 | 0.9130 |
| 0.1          | 0.8          | 0.1          | 0.8980 | 0.9015 | 0.9449 | 0.5          | 0.1          | 0.4          | 0.8965 | 0.9115 | 0.9430 |
| 0.2          | 0.1          | 0.7          | 0.8900 | 0.8980 | 0.9333 | 0.5          | 0.2          | 0.3          | 0.8985 | 0.9035 | 0.9265 |
| 0.2          | 0.2          | 0.6          | 0.8925 | 0.9010 | 0.9358 | 0.5          | 0.3          | 0.2          | 0.8920 | 0.8985 | 0.9015 |
| 0.2          | 0.3          | 0.5          | 0.8975 | 0.9000 | 0.9373 | 0.5          | 0.4          | 0.1          | 0.9205 | 0.9075 | 0.9065 |
| 0.2          | 0.4          | 0.4          | 0.8915 | 0.8900 | 0.9448 | 0.6          | 0.1          | 0.3          | 0.8965 | 0.9050 | 0.9164 |
| 0.2          | 0.5          | 0.3          | 0.8995 | 0.8880 | 0.9593 | 0.6          | 0.2          | 0.2          | 0.8960 | 0.8875 | 0.9090 |
| 0.2          | 0.6          | 0.2          | 0.8995 | 0.9005 | 0.9539 | 0.6          | 0.3          | 0.1          | 0.9075 | 0.8970 | 0.9030 |
| 0.2          | 0.7          | 0.1          | 0.8995 | 0.9080 | 0.9189 | 0.7          | 0.1          | 0.2          | 0.9105 | 0.8985 | 0.8960 |
| 0.3          | 0.1          | 0.6          | 0.9060 | 0.9065 | 0.9498 | 0.7          | 0.2          | 0.1          | 0.8885 | 0.9050 | 0.8985 |
| 0.3          | 0.2          | 0.5          | 0.8975 | 0.9015 | 0.9443 | 0.8          | 0.1          | 0.1          | 0.9005 | 0.8990 | 0.9040 |
| 0.3          | 0.3          | 0.4          | 0.9065 | 0.8865 | 0.9524 | MAX          |              |              | 0.9205 | 0.9115 | 0.9593 |
| 0.3          | 0.4          | 0.3          | 0.9035 | 0.9055 | 0.9514 | MIN          |              |              | 0.8885 | 0.8860 | 0.8960 |

**TABLE 3.2.5 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 12$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9010 | 0.9030 | 0.8568 | 0.3          | 0.5          | 0.2          | 0.8995 | 0.9075 | 0.9355 |
| 0.1          | 0.2          | 0.7          | 0.9050 | 0.9015 | 0.8739 | 0.3          | 0.6          | 0.1          | 0.8900 | 0.9025 | 0.9195 |
| 0.1          | 0.3          | 0.6          | 0.9000 | 0.9050 | 0.8795 | 0.4          | 0.1          | 0.5          | 0.9075 | 0.9015 | 0.9444 |
| 0.1          | 0.4          | 0.5          | 0.9005 | 0.8910 | 0.8884 | 0.4          | 0.2          | 0.4          | 0.9005 | 0.8975 | 0.9389 |
| 0.1          | 0.5          | 0.4          | 0.8975 | 0.9050 | 0.9067 | 0.4          | 0.3          | 0.3          | 0.9020 | 0.8960 | 0.9325 |
| 0.1          | 0.6          | 0.3          | 0.8935 | 0.8915 | 0.9374 | 0.4          | 0.4          | 0.2          | 0.8920 | 0.8860 | 0.9225 |
| 0.1          | 0.7          | 0.2          | 0.8995 | 0.9010 | 0.9231 | 0.4          | 0.5          | 0.1          | 0.9205 | 0.8920 | 0.9195 |
| 0.1          | 0.8          | 0.1          | 0.9030 | 0.8980 | 0.9370 | 0.5          | 0.1          | 0.4          | 0.9030 | 0.9050 | 0.9504 |
| 0.2          | 0.1          | 0.7          | 0.9110 | 0.8980 | 0.9064 | 0.5          | 0.2          | 0.3          | 0.9070 | 0.8975 | 0.9345 |
| 0.2          | 0.2          | 0.6          | 0.8970 | 0.9075 | 0.9220 | 0.5          | 0.3          | 0.2          | 0.9075 | 0.9195 | 0.9175 |
| 0.2          | 0.3          | 0.5          | 0.9010 | 0.9035 | 0.9178 | 0.5          | 0.4          | 0.1          | 0.9005 | 0.9075 | 0.9100 |
| 0.2          | 0.4          | 0.4          | 0.8960 | 0.8915 | 0.9323 | 0.6          | 0.1          | 0.3          | 0.9040 | 0.9060 | 0.9170 |
| 0.2          | 0.5          | 0.3          | 0.9020 | 0.8980 | 0.9369 | 0.6          | 0.2          | 0.2          | 0.9060 | 0.9160 | 0.9170 |
| 0.2          | 0.6          | 0.2          | 0.8870 | 0.9050 | 0.9449 | 0.6          | 0.3          | 0.1          | 0.9040 | 0.9015 | 0.9055 |
| 0.2          | 0.7          | 0.1          | 0.9030 | 0.9000 | 0.9275 | 0.7          | 0.1          | 0.2          | 0.8985 | 0.8880 | 0.8955 |
| 0.3          | 0.1          | 0.6          | 0.9060 | 0.9110 | 0.9284 | 0.7          | 0.2          | 0.1          | 0.8930 | 0.9050 | 0.9035 |
| 0.3          | 0.2          | 0.5          | 0.8940 | 0.9040 | 0.9402 | 0.8          | 0.1          | 0.1          | 0.9080 | 0.9010 | 0.9125 |
| 0.3          | 0.3          | 0.4          | 0.8940 | 0.8970 | 0.9389 | MAX          |              |              | 0.9205 | 0.9195 | 0.9504 |
| 0.3          | 0.4          | 0.3          | 0.9005 | 0.8920 | 0.9335 | MIN          |              |              | 0.8870 | 0.8860 | 0.8568 |

**TABLE 3.2.6 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 12$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8940 | 0.9010 | 0.9193 | 0.3          | 0.5          | 0.2          | 0.8955 | 0.9025 | 0.9140 |
| 0.1          | 0.2          | 0.7          | 0.9060 | 0.9060 | 0.9191 | 0.3          | 0.6          | 0.1          | 0.8905 | 0.9000 | 0.9085 |
| 0.1          | 0.3          | 0.6          | 0.8985 | 0.8865 | 0.9285 | 0.4          | 0.1          | 0.5          | 0.9010 | 0.9005 | 0.9250 |
| 0.1          | 0.4          | 0.5          | 0.9070 | 0.8880 | 0.9211 | 0.4          | 0.2          | 0.4          | 0.9110 | 0.9030 | 0.9270 |
| 0.1          | 0.5          | 0.4          | 0.9030 | 0.8900 | 0.9290 | 0.4          | 0.3          | 0.3          | 0.9085 | 0.9040 | 0.9205 |
| 0.1          | 0.6          | 0.3          | 0.8965 | 0.8985 | 0.9368 | 0.4          | 0.4          | 0.2          | 0.8935 | 0.9045 | 0.9155 |
| 0.1          | 0.7          | 0.2          | 0.9000 | 0.9020 | 0.9430 | 0.4          | 0.5          | 0.1          | 0.9000 | 0.8985 | 0.9015 |
| 0.1          | 0.8          | 0.1          | 0.9085 | 0.9035 | 0.9260 | 0.5          | 0.1          | 0.4          | 0.8930 | 0.9005 | 0.9204 |
| 0.2          | 0.1          | 0.7          | 0.8970 | 0.9090 | 0.9267 | 0.5          | 0.2          | 0.3          | 0.8995 | 0.8940 | 0.9200 |
| 0.2          | 0.2          | 0.6          | 0.9025 | 0.8990 | 0.9317 | 0.5          | 0.3          | 0.2          | 0.8945 | 0.8990 | 0.9075 |
| 0.2          | 0.3          | 0.5          | 0.8965 | 0.8945 | 0.9354 | 0.5          | 0.4          | 0.1          | 0.8985 | 0.9070 | 0.8995 |
| 0.2          | 0.4          | 0.4          | 0.9050 | 0.8990 | 0.9455 | 0.6          | 0.1          | 0.3          | 0.9005 | 0.8980 | 0.9135 |
| 0.2          | 0.5          | 0.3          | 0.9125 | 0.9060 | 0.9385 | 0.6          | 0.2          | 0.2          | 0.9115 | 0.9015 | 0.9065 |
| 0.2          | 0.6          | 0.2          | 0.8930 | 0.9080 | 0.9230 | 0.6          | 0.3          | 0.1          | 0.8875 | 0.9020 | 0.9010 |
| 0.2          | 0.7          | 0.1          | 0.9095 | 0.9080 | 0.9010 | 0.7          | 0.1          | 0.2          | 0.8965 | 0.9030 | 0.9160 |
| 0.3          | 0.1          | 0.6          | 0.8975 | 0.8990 | 0.9445 | 0.7          | 0.2          | 0.1          | 0.9010 | 0.9000 | 0.9060 |
| 0.3          | 0.2          | 0.5          | 0.8880 | 0.9010 | 0.9399 | 0.8          | 0.1          | 0.1          | 0.8970 | 0.8900 | 0.8905 |
| 0.3          | 0.3          | 0.4          | 0.8995 | 0.9060 | 0.9370 | MAX          |              |              | 0.9125 | 0.9105 | 0.9455 |
| 0.3          | 0.4          | 0.3          | 0.9080 | 0.9105 | 0.9130 | MIN          |              |              | 0.8875 | 0.8865 | 0.8905 |

**TABLE 3.2.7 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 12$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9105 | 0.9035 | 0.8940 | 0.3          | 0.5          | 0.2          | 0.9050 | 0.8915 | 0.9245 |
| 0.1          | 0.2          | 0.7          | 0.8940 | 0.8945 | 0.9116 | 0.3          | 0.6          | 0.1          | 0.8970 | 0.9005 | 0.9110 |
| 0.1          | 0.3          | 0.6          | 0.9040 | 0.9115 | 0.9256 | 0.4          | 0.1          | 0.5          | 0.9070 | 0.9130 | 0.9360 |
| 0.1          | 0.4          | 0.5          | 0.8980 | 0.8995 | 0.9253 | 0.4          | 0.2          | 0.4          | 0.9070 | 0.9090 | 0.9185 |
| 0.1          | 0.5          | 0.4          | 0.8990 | 0.8970 | 0.9331 | 0.4          | 0.3          | 0.3          | 0.8945 | 0.8940 | 0.9115 |
| 0.1          | 0.6          | 0.3          | 0.8970 | 0.9030 | 0.9433 | 0.4          | 0.4          | 0.2          | 0.9005 | 0.9010 | 0.9065 |
| 0.1          | 0.7          | 0.2          | 0.9025 | 0.8975 | 0.9419 | 0.4          | 0.5          | 0.1          | 0.9180 | 0.9045 | 0.9030 |
| 0.1          | 0.8          | 0.1          | 0.8950 | 0.8980 | 0.9154 | 0.5          | 0.1          | 0.4          | 0.8970 | 0.9090 | 0.9250 |
| 0.2          | 0.1          | 0.7          | 0.9075 | 0.9070 | 0.9403 | 0.5          | 0.2          | 0.3          | 0.8905 | 0.9075 | 0.9105 |
| 0.2          | 0.2          | 0.6          | 0.8980 | 0.8965 | 0.9333 | 0.5          | 0.3          | 0.2          | 0.8965 | 0.9060 | 0.9060 |
| 0.2          | 0.3          | 0.5          | 0.8990 | 0.9050 | 0.9479 | 0.5          | 0.4          | 0.1          | 0.9030 | 0.8930 | 0.9035 |
| 0.2          | 0.4          | 0.4          | 0.9060 | 0.9035 | 0.9489 | 0.6          | 0.1          | 0.3          | 0.9010 | 0.8995 | 0.9130 |
| 0.2          | 0.5          | 0.3          | 0.8910 | 0.9090 | 0.9395 | 0.6          | 0.2          | 0.2          | 0.8915 | 0.9080 | 0.8985 |
| 0.2          | 0.6          | 0.2          | 0.9055 | 0.9060 | 0.9105 | 0.6          | 0.3          | 0.1          | 0.9045 | 0.9015 | 0.9110 |
| 0.2          | 0.7          | 0.1          | 0.9070 | 0.8930 | 0.8995 | 0.7          | 0.1          | 0.2          | 0.8995 | 0.9005 | 0.9065 |
| 0.3          | 0.1          | 0.6          | 0.9085 | 0.8970 | 0.9419 | 0.7          | 0.2          | 0.1          | 0.9030 | 0.8960 | 0.8985 |
| 0.3          | 0.2          | 0.5          | 0.8960 | 0.9075 | 0.9474 | 0.8          | 0.1          | 0.1          | 0.9035 | 0.8940 | 0.9100 |
| 0.3          | 0.3          | 0.4          | 0.9060 | 0.9030 | 0.9279 | MAX          |              |              | 0.9180 | 0.9130 | 0.9489 |
| 0.3          | 0.4          | 0.3          | 0.8935 | 0.8995 | 0.9150 | MIN          |              |              | 0.8905 | 0.8915 | 0.8940 |

**TABLE 3.2.8 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 12$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9040 | 0.9115 | 0.9305 | 0.3          | 0.5          | 0.2          | 0.8980 | 0.9000 | 0.9100 |
| 0.1          | 0.2          | 0.7          | 0.8960 | 0.8975 | 0.9362 | 0.3          | 0.6          | 0.1          | 0.8990 | 0.9025 | 0.9005 |
| 0.1          | 0.3          | 0.6          | 0.8935 | 0.9025 | 0.9278 | 0.4          | 0.1          | 0.5          | 0.9090 | 0.8985 | 0.9125 |
| 0.1          | 0.4          | 0.5          | 0.8890 | 0.8840 | 0.9478 | 0.4          | 0.2          | 0.4          | 0.9030 | 0.8975 | 0.9015 |
| 0.1          | 0.5          | 0.4          | 0.9005 | 0.8965 | 0.9370 | 0.4          | 0.3          | 0.3          | 0.9015 | 0.9025 | 0.9095 |
| 0.1          | 0.6          | 0.3          | 0.9060 | 0.9050 | 0.9464 | 0.4          | 0.4          | 0.2          | 0.9010 | 0.8970 | 0.9055 |
| 0.1          | 0.7          | 0.2          | 0.8905 | 0.9040 | 0.9210 | 0.4          | 0.5          | 0.1          | 0.8995 | 0.9045 | 0.8725 |
| 0.1          | 0.8          | 0.1          | 0.8835 | 0.9055 | 0.9000 | 0.5          | 0.1          | 0.4          | 0.8870 | 0.9155 | 0.9130 |
| 0.2          | 0.1          | 0.7          | 0.8985 | 0.8840 | 0.9404 | 0.5          | 0.2          | 0.3          | 0.9035 | 0.9045 | 0.9045 |
| 0.2          | 0.2          | 0.6          | 0.9065 | 0.9045 | 0.9335 | 0.5          | 0.3          | 0.2          | 0.9045 | 0.8820 | 0.9045 |
| 0.2          | 0.3          | 0.5          | 0.8995 | 0.8960 | 0.9445 | 0.5          | 0.4          | 0.1          | 0.8995 | 0.9045 | 0.8990 |
| 0.2          | 0.4          | 0.4          | 0.8965 | 0.8990 | 0.9524 | 0.6          | 0.1          | 0.3          | 0.9060 | 0.8915 | 0.9120 |
| 0.2          | 0.5          | 0.3          | 0.8970 | 0.8975 | 0.9485 | 0.6          | 0.2          | 0.2          | 0.8975 | 0.9100 | 0.9150 |
| 0.2          | 0.6          | 0.2          | 0.8950 | 0.8965 | 0.9045 | 0.6          | 0.3          | 0.1          | 0.8955 | 0.8945 | 0.9085 |
| 0.2          | 0.7          | 0.1          | 0.8900 | 0.8995 | 0.9110 | 0.7          | 0.1          | 0.2          | 0.8960 | 0.8965 | 0.8985 |
| 0.3          | 0.1          | 0.6          | 0.8980 | 0.9030 | 0.9205 | 0.7          | 0.2          | 0.1          | 0.9030 | 0.8900 | 0.8825 |
| 0.3          | 0.2          | 0.5          | 0.8925 | 0.8985 | 0.9380 | 0.8          | 0.1          | 0.1          | 0.9025 | 0.8925 | 0.9060 |
| 0.3          | 0.3          | 0.4          | 0.8975 | 0.9000 | 0.9150 | MAX          |              |              | 0.9090 | 0.9155 | 0.9524 |
| 0.3          | 0.4          | 0.3          | 0.8975 | 0.8990 | 0.9045 | MIN          |              |              | 0.8835 | 0.8820 | 0.8725 |

**TABLE 3.2.9 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 24$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8930 | 0.8905 | 0.8791 | 0.3          | 0.5          | 0.2          | 0.8925 | 0.8985 | 0.9155 |
| 0.1          | 0.2          | 0.7          | 0.9065 | 0.9005 | 0.8927 | 0.3          | 0.6          | 0.1          | 0.8980 | 0.8825 | 0.9055 |
| 0.1          | 0.3          | 0.6          | 0.9010 | 0.9030 | 0.8996 | 0.4          | 0.1          | 0.5          | 0.8890 | 0.9020 | 0.9330 |
| 0.1          | 0.4          | 0.5          | 0.8990 | 0.9050 | 0.9086 | 0.4          | 0.2          | 0.4          | 0.8955 | 0.9060 | 0.9195 |
| 0.1          | 0.5          | 0.4          | 0.8985 | 0.8890 | 0.9199 | 0.4          | 0.3          | 0.3          | 0.9065 | 0.9090 | 0.9085 |
| 0.1          | 0.6          | 0.3          | 0.8915 | 0.8995 | 0.9333 | 0.4          | 0.4          | 0.2          | 0.8990 | 0.8940 | 0.9054 |
| 0.1          | 0.7          | 0.2          | 0.8955 | 0.8995 | 0.9450 | 0.4          | 0.5          | 0.1          | 0.9100 | 0.9135 | 0.8915 |
| 0.1          | 0.8          | 0.1          | 0.9015 | 0.9050 | 0.9035 | 0.5          | 0.1          | 0.4          | 0.8955 | 0.8995 | 0.9105 |
| 0.2          | 0.1          | 0.7          | 0.9000 | 0.8920 | 0.9157 | 0.5          | 0.2          | 0.3          | 0.9055 | 0.8985 | 0.9100 |
| 0.2          | 0.2          | 0.6          | 0.9025 | 0.8960 | 0.9314 | 0.5          | 0.3          | 0.2          | 0.9085 | 0.9100 | 0.9030 |
| 0.2          | 0.3          | 0.5          | 0.8855 | 0.9055 | 0.9465 | 0.5          | 0.4          | 0.1          | 0.9130 | 0.8950 | 0.9105 |
| 0.2          | 0.4          | 0.4          | 0.9115 | 0.9000 | 0.9294 | 0.6          | 0.1          | 0.3          | 0.8955 | 0.9035 | 0.9090 |
| 0.2          | 0.5          | 0.3          | 0.8995 | 0.9000 | 0.9365 | 0.6          | 0.2          | 0.2          | 0.8925 | 0.9140 | 0.9000 |
| 0.2          | 0.6          | 0.2          | 0.9050 | 0.9085 | 0.9200 | 0.6          | 0.3          | 0.1          | 0.9070 | 0.9075 | 0.9075 |
| 0.2          | 0.7          | 0.1          | 0.8875 | 0.9080 | 0.9110 | 0.7          | 0.1          | 0.2          | 0.8950 | 0.8935 | 0.8905 |
| 0.3          | 0.1          | 0.6          | 0.8930 | 0.9170 | 0.9350 | 0.7          | 0.2          | 0.1          | 0.8965 | 0.8905 | 0.8975 |
| 0.3          | 0.2          | 0.5          | 0.8965 | 0.9090 | 0.9375 | 0.8          | 0.1          | 0.1          | 0.9035 | 0.9140 | 0.9025 |
| 0.3          | 0.3          | 0.4          | 0.8930 | 0.9040 | 0.9155 | MAX          |              |              | 0.9130 | 0.9170 | 0.9465 |
| 0.3          | 0.4          | 0.3          | 0.9035 | 0.9095 | 0.9290 | MIN          |              |              | 0.8855 | 0.8825 | 0.8791 |



**TABLE 3.2.10 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 24$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9100 | 0.9135 | 0.9285 | 0.3          | 0.5          | 0.2          | 0.8925 | 0.9025 | 0.9085 |
| 0.1          | 0.2          | 0.7          | 0.8960 | 0.9110 | 0.9248 | 0.3          | 0.6          | 0.1          | 0.9030 | 0.8990 | 0.9170 |
| 0.1          | 0.3          | 0.6          | 0.9050 | 0.9015 | 0.9134 | 0.4          | 0.1          | 0.5          | 0.9000 | 0.8935 | 0.9165 |
| 0.1          | 0.4          | 0.5          | 0.9015 | 0.9110 | 0.9385 | 0.4          | 0.2          | 0.4          | 0.8980 | 0.9155 | 0.9100 |
| 0.1          | 0.5          | 0.4          | 0.8925 | 0.8990 | 0.9405 | 0.4          | 0.3          | 0.3          | 0.8980 | 0.9055 | 0.9160 |
| 0.1          | 0.6          | 0.3          | 0.9000 | 0.9050 | 0.9305 | 0.4          | 0.4          | 0.2          | 0.8935 | 0.8920 | 0.9000 |
| 0.1          | 0.7          | 0.2          | 0.9035 | 0.9045 | 0.9165 | 0.4          | 0.5          | 0.1          | 0.8910 | 0.9070 | 0.9100 |
| 0.1          | 0.8          | 0.1          | 0.8915 | 0.9035 | 0.9100 | 0.5          | 0.1          | 0.4          | 0.9110 | 0.9100 | 0.9035 |
| 0.2          | 0.1          | 0.7          | 0.8925 | 0.8970 | 0.9355 | 0.5          | 0.2          | 0.3          | 0.9055 | 0.8940 | 0.9075 |
| 0.2          | 0.2          | 0.6          | 0.9085 | 0.8930 | 0.9285 | 0.5          | 0.3          | 0.2          | 0.8940 | 0.8935 | 0.9005 |
| 0.2          | 0.3          | 0.5          | 0.9010 | 0.8970 | 0.9185 | 0.5          | 0.4          | 0.1          | 0.9005 | 0.8955 | 0.9030 |
| 0.2          | 0.4          | 0.4          | 0.9025 | 0.8970 | 0.9090 | 0.6          | 0.1          | 0.3          | 0.8990 | 0.8975 | 0.8990 |
| 0.2          | 0.5          | 0.3          | 0.9010 | 0.9070 | 0.9170 | 0.6          | 0.2          | 0.2          | 0.9065 | 0.8940 | 0.9070 |
| 0.2          | 0.6          | 0.2          | 0.9065 | 0.8950 | 0.9140 | 0.6          | 0.3          | 0.1          | 0.8985 | 0.8895 | 0.9030 |
| 0.2          | 0.7          | 0.1          | 0.8950 | 0.9015 | 0.8950 | 0.7          | 0.1          | 0.2          | 0.8875 | 0.9020 | 0.9011 |
| 0.3          | 0.1          | 0.6          | 0.9175 | 0.9035 | 0.9125 | 0.7          | 0.2          | 0.1          | 0.9115 | 0.8985 | 0.9045 |
| 0.3          | 0.2          | 0.5          | 0.8990 | 0.9010 | 0.9150 | 0.8          | 0.1          | 0.1          | 0.8965 | 0.9035 | 0.8965 |
| 0.3          | 0.3          | 0.4          | 0.8865 | 0.9030 | 0.9145 | MAX          |              |              | 0.9175 | 0.9155 | 0.9405 |
| 0.3          | 0.4          | 0.3          | 0.9025 | 0.9050 | 0.9125 | MIN          |              |              | 0.8865 | 0.8895 | 0.8950 |



**TABLE 3.2.11 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 24$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9025 | 0.9090 | 0.9215 | 0.3          | 0.5          | 0.2          | 0.8965 | 0.8965 | 0.9135 |
| 0.1          | 0.2          | 0.7          | 0.8920 | 0.8975 | 0.9216 | 0.3          | 0.6          | 0.1          | 0.8940 | 0.8905 | 0.9110 |
| 0.1          | 0.3          | 0.6          | 0.8950 | 0.8955 | 0.9335 | 0.4          | 0.1          | 0.5          | 0.8835 | 0.8965 | 0.9075 |
| 0.1          | 0.4          | 0.5          | 0.9110 | 0.9020 | 0.9294 | 0.4          | 0.2          | 0.4          | 0.9175 | 0.8930 | 0.9175 |
| 0.1          | 0.5          | 0.4          | 0.9000 | 0.8890 | 0.9319 | 0.4          | 0.3          | 0.3          | 0.8990 | 0.8945 | 0.8975 |
| 0.1          | 0.6          | 0.3          | 0.9145 | 0.9005 | 0.9320 | 0.4          | 0.4          | 0.2          | 0.8960 | 0.8995 | 0.9115 |
| 0.1          | 0.7          | 0.2          | 0.8955 | 0.9105 | 0.9170 | 0.4          | 0.5          | 0.1          | 0.8950 | 0.9075 | 0.8905 |
| 0.1          | 0.8          | 0.1          | 0.9025 | 0.8965 | 0.9030 | 0.5          | 0.1          | 0.4          | 0.8955 | 0.8930 | 0.8945 |
| 0.2          | 0.1          | 0.7          | 0.8975 | 0.8985 | 0.9354 | 0.5          | 0.2          | 0.3          | 0.8945 | 0.9015 | 0.9105 |
| 0.2          | 0.2          | 0.6          | 0.8985 | 0.9010 | 0.9340 | 0.5          | 0.3          | 0.2          | 0.9000 | 0.9035 | 0.8925 |
| 0.2          | 0.3          | 0.5          | 0.8980 | 0.8970 | 0.9250 | 0.5          | 0.4          | 0.1          | 0.8940 | 0.8975 | 0.8995 |
| 0.2          | 0.4          | 0.4          | 0.8940 | 0.8935 | 0.9190 | 0.6          | 0.1          | 0.3          | 0.9025 | 0.8950 | 0.8985 |
| 0.2          | 0.5          | 0.3          | 0.8985 | 0.8935 | 0.9045 | 0.6          | 0.2          | 0.2          | 0.9020 | 0.8990 | 0.9020 |
| 0.2          | 0.6          | 0.2          | 0.9050 | 0.8955 | 0.9100 | 0.6          | 0.3          | 0.1          | 0.9125 | 0.9040 | 0.9015 |
| 0.2          | 0.7          | 0.1          | 0.8855 | 0.9065 | 0.9105 | 0.7          | 0.1          | 0.2          | 0.9070 | 0.8960 | 0.8950 |
| 0.3          | 0.1          | 0.6          | 0.8955 | 0.9105 | 0.9120 | 0.7          | 0.2          | 0.1          | 0.9120 | 0.8975 | 0.9005 |
| 0.3          | 0.2          | 0.5          | 0.8940 | 0.9025 | 0.9070 | 0.8          | 0.1          | 0.1          | 0.9055 | 0.9130 | 0.8895 |
| 0.3          | 0.3          | 0.4          | 0.9060 | 0.9050 | 0.9210 | MAX          |              |              | 0.9175 | 0.9130 | 0.9354 |
| 0.3          | 0.4          | 0.3          | 0.8995 | 0.8965 | 0.9070 | MIN          |              |              | 0.8835 | 0.8890 | 0.8895 |

**TABLE 3.2.12 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 24$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8940 | 0.8880 | 0.9385 | 0.3          | 0.5          | 0.2          | 0.8890 | 0.9075 | 0.9030 |
| 0.1          | 0.2          | 0.7          | 0.9080 | 0.8985 | 0.9344 | 0.3          | 0.6          | 0.1          | 0.9000 | 0.9005 | 0.8940 |
| 0.1          | 0.3          | 0.6          | 0.9000 | 0.8980 | 0.9385 | 0.4          | 0.1          | 0.5          | 0.9005 | 0.8940 | 0.9130 |
| 0.1          | 0.4          | 0.5          | 0.9055 | 0.8935 | 0.9135 | 0.4          | 0.2          | 0.4          | 0.8930 | 0.9005 | 0.9050 |
| 0.1          | 0.5          | 0.4          | 0.9005 | 0.9035 | 0.9230 | 0.4          | 0.3          | 0.3          | 0.9005 | 0.8905 | 0.9015 |
| 0.1          | 0.6          | 0.3          | 0.9015 | 0.9005 | 0.9055 | 0.4          | 0.4          | 0.2          | 0.8960 | 0.9035 | 0.9095 |
| 0.1          | 0.7          | 0.2          | 0.8950 | 0.9005 | 0.9020 | 0.4          | 0.5          | 0.1          | 0.9110 | 0.9065 | 0.8985 |
| 0.1          | 0.8          | 0.1          | 0.9030 | 0.8950 | 0.8975 | 0.5          | 0.1          | 0.4          | 0.9075 | 0.9005 | 0.8940 |
| 0.2          | 0.1          | 0.7          | 0.9005 | 0.8975 | 0.9165 | 0.5          | 0.2          | 0.3          | 0.9080 | 0.9020 | 0.9000 |
| 0.2          | 0.2          | 0.6          | 0.9010 | 0.9000 | 0.9220 | 0.5          | 0.3          | 0.2          | 0.8995 | 0.8970 | 0.9000 |
| 0.2          | 0.3          | 0.5          | 0.9010 | 0.9150 | 0.9045 | 0.5          | 0.4          | 0.1          | 0.9025 | 0.8950 | 0.9050 |
| 0.2          | 0.4          | 0.4          | 0.8995 | 0.8940 | 0.8990 | 0.6          | 0.1          | 0.3          | 0.9045 | 0.8970 | 0.8910 |
| 0.2          | 0.5          | 0.3          | 0.9030 | 0.8940 | 0.9015 | 0.6          | 0.2          | 0.2          | 0.9085 | 0.9015 | 0.9015 |
| 0.2          | 0.6          | 0.2          | 0.9065 | 0.8975 | 0.9085 | 0.6          | 0.3          | 0.1          | 0.9105 | 0.9220 | 0.9110 |
| 0.2          | 0.7          | 0.1          | 0.8950 | 0.9025 | 0.8940 | 0.7          | 0.1          | 0.2          | 0.8955 | 0.9055 | 0.8945 |
| 0.3          | 0.1          | 0.6          | 0.9035 | 0.9115 | 0.9050 | 0.7          | 0.2          | 0.1          | 0.9030 | 0.8945 | 0.8985 |
| 0.3          | 0.2          | 0.5          | 0.9015 | 0.8885 | 0.8980 | 0.8          | 0.1          | 0.1          | 0.9030 | 0.8975 | 0.9045 |
| 0.3          | 0.3          | 0.4          | 0.8960 | 0.9010 | 0.9045 | MAX          |              |              | 0.9110 | 0.9220 | 0.9385 |
| 0.3          | 0.4          | 0.3          | 0.9010 | 0.8975 | 0.9000 | MIN          |              |              | 0.8890 | 0.8880 | 0.8910 |

**TABLE 3.2.13 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 6$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9160 | 0.8965 | 0.8370 | 0.3          | 0.5          | 0.2          | 0.8840 | 0.9115 | 0.9528 |
| 0.1          | 0.2          | 0.7          | 0.8945 | 0.9055 | 0.8890 | 0.3          | 0.6          | 0.1          | 0.9020 | 0.8975 | 0.9441 |
| 0.1          | 0.3          | 0.6          | 0.9145 | 0.8975 | 0.9105 | 0.4          | 0.1          | 0.5          | 0.9035 | 0.9055 | 0.8750 |
| 0.1          | 0.4          | 0.5          | 0.9025 | 0.8990 | 0.9195 | 0.4          | 0.2          | 0.4          | 0.9025 | 0.8955 | 0.9214 |
| 0.1          | 0.5          | 0.4          | 0.8890 | 0.9115 | 0.9380 | 0.4          | 0.3          | 0.3          | 0.8975 | 0.9025 | 0.9336 |
| 0.1          | 0.6          | 0.3          | 0.9020 | 0.9000 | 0.9392 | 0.4          | 0.4          | 0.2          | 0.8935 | 0.8960 | 0.9466 |
| 0.1          | 0.7          | 0.2          | 0.8920 | 0.8940 | 0.9486 | 0.4          | 0.5          | 0.1          | 0.9065 | 0.9070 | 0.9458 |
| 0.1          | 0.8          | 0.1          | 0.9055 | 0.8820 | 0.9540 | 0.5          | 0.1          | 0.4          | 0.9120 | 0.8955 | 0.8819 |
| 0.2          | 0.1          | 0.7          | 0.8995 | 0.9135 | 0.8924 | 0.5          | 0.2          | 0.3          | 0.9105 | 0.9070 | 0.9296 |
| 0.2          | 0.2          | 0.6          | 0.8965 | 0.8975 | 0.9011 | 0.5          | 0.3          | 0.2          | 0.9035 | 0.8985 | 0.9342 |
| 0.2          | 0.3          | 0.5          | 0.8980 | 0.9000 | 0.9204 | 0.5          | 0.4          | 0.1          | 0.9085 | 0.8850 | 0.9447 |
| 0.2          | 0.4          | 0.4          | 0.9000 | 0.9090 | 0.9333 | 0.6          | 0.1          | 0.3          | 0.8895 | 0.9125 | 0.8926 |
| 0.2          | 0.5          | 0.3          | 0.8960 | 0.8990 | 0.9381 | 0.6          | 0.2          | 0.2          | 0.8955 | 0.8935 | 0.9388 |
| 0.2          | 0.6          | 0.2          | 0.8955 | 0.8905 | 0.9452 | 0.6          | 0.3          | 0.1          | 0.9035 | 0.8885 | 0.9554 |
| 0.2          | 0.7          | 0.1          | 0.9000 | 0.9025 | 0.9523 | 0.7          | 0.1          | 0.2          | 0.9015 | 0.9020 | 0.9279 |
| 0.3          | 0.1          | 0.6          | 0.9020 | 0.9080 | 0.8515 | 0.7          | 0.2          | 0.1          | 0.9000 | 0.9045 | 0.9499 |
| 0.3          | 0.2          | 0.5          | 0.8945 | 0.9025 | 0.9131 | 0.8          | 0.1          | 0.1          | 0.9030 | 0.8995 | 0.9313 |
| 0.3          | 0.3          | 0.4          | 0.9065 | 0.9020 | 0.9406 | MAX          |              |              | 0.9160 | 0.9125 | 0.9554 |
| 0.3          | 0.4          | 0.3          | 0.9120 | 0.9080 | 0.9369 | MIN          |              |              | 0.8840 | 0.8820 | 0.8370 |

**TABLE 3.2.14 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 6$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9000 | 0.8925 | 0.8800 | 0.3          | 0.5          | 0.2          | 0.9040 | 0.9120 | 0.9480 |
| 0.1          | 0.2          | 0.7          | 0.9070 | 0.8965 | 0.9244 | 0.3          | 0.6          | 0.1          | 0.9085 | 0.9040 | 0.9516 |
| 0.1          | 0.3          | 0.6          | 0.8960 | 0.8905 | 0.9401 | 0.4          | 0.1          | 0.5          | 0.8980 | 0.9010 | 0.9165 |
| 0.1          | 0.4          | 0.5          | 0.9020 | 0.9025 | 0.9345 | 0.4          | 0.2          | 0.4          | 0.9060 | 0.8915 | 0.9182 |
| 0.1          | 0.5          | 0.4          | 0.8930 | 0.8920 | 0.9470 | 0.4          | 0.3          | 0.3          | 0.8940 | 0.9110 | 0.9438 |
| 0.1          | 0.6          | 0.3          | 0.9035 | 0.9015 | 0.9372 | 0.4          | 0.4          | 0.2          | 0.9000 | 0.8995 | 0.9444 |
| 0.1          | 0.7          | 0.2          | 0.8935 | 0.8980 | 0.9451 | 0.4          | 0.5          | 0.1          | 0.9015 | 0.8950 | 0.9486 |
| 0.1          | 0.8          | 0.1          | 0.8990 | 0.8865 | 0.9562 | 0.5          | 0.1          | 0.4          | 0.9010 | 0.9050 | 0.9215 |
| 0.2          | 0.1          | 0.7          | 0.8980 | 0.8940 | 0.8887 | 0.5          | 0.2          | 0.3          | 0.8940 | 0.8945 | 0.9358 |
| 0.2          | 0.2          | 0.6          | 0.9030 | 0.9105 | 0.9271 | 0.5          | 0.3          | 0.2          | 0.8935 | 0.8940 | 0.9440 |
| 0.2          | 0.3          | 0.5          | 0.9110 | 0.9005 | 0.9348 | 0.5          | 0.4          | 0.1          | 0.9155 | 0.9025 | 0.9478 |
| 0.2          | 0.4          | 0.4          | 0.9035 | 0.8990 | 0.9266 | 0.6          | 0.1          | 0.3          | 0.9085 | 0.9050 | 0.9136 |
| 0.2          | 0.5          | 0.3          | 0.9080 | 0.9060 | 0.9537 | 0.6          | 0.2          | 0.2          | 0.9000 | 0.8930 | 0.9371 |
| 0.2          | 0.6          | 0.2          | 0.9085 | 0.9005 | 0.9490 | 0.6          | 0.3          | 0.1          | 0.9005 | 0.8885 | 0.9499 |
| 0.2          | 0.7          | 0.1          | 0.9075 | 0.8930 | 0.9446 | 0.7          | 0.1          | 0.2          | 0.9055 | 0.8965 | 0.9274 |
| 0.3          | 0.1          | 0.6          | 0.9000 | 0.9040 | 0.9088 | 0.7          | 0.2          | 0.1          | 0.9080 | 0.9075 | 0.9458 |
| 0.3          | 0.2          | 0.5          | 0.9115 | 0.9055 | 0.9324 | 0.8          | 0.1          | 0.1          | 0.9110 | 0.9045 | 0.9471 |
| 0.3          | 0.3          | 0.4          | 0.8940 | 0.8950 | 0.9426 | MAX          |              |              | 0.9155 | 0.9120 | 0.9562 |
| 0.3          | 0.4          | 0.3          | 0.9020 | 0.8960 | 0.9411 | MIN          |              |              | 0.8930 | 0.8865 | 0.8800 |

**TABLE 3.2.15 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 6$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8830 | 0.8980 | 0.8838 | 0.3          | 0.5          | 0.2          | 0.8930 | 0.9005 | 0.9385 |
| 0.1          | 0.2          | 0.7          | 0.9065 | 0.9000 | 0.9231 | 0.3          | 0.6          | 0.1          | 0.8910 | 0.9005 | 0.9200 |
| 0.1          | 0.3          | 0.6          | 0.9055 | 0.9070 | 0.9372 | 0.4          | 0.1          | 0.5          | 0.9030 | 0.9075 | 0.9045 |
| 0.1          | 0.4          | 0.5          | 0.9000 | 0.8930 | 0.9441 | 0.4          | 0.2          | 0.4          | 0.9035 | 0.8965 | 0.9427 |
| 0.1          | 0.5          | 0.4          | 0.9005 | 0.9045 | 0.9468 | 0.4          | 0.3          | 0.3          | 0.8955 | 0.8865 | 0.9427 |
| 0.1          | 0.6          | 0.3          | 0.9055 | 0.9030 | 0.9424 | 0.4          | 0.4          | 0.2          | 0.9025 | 0.9080 | 0.9455 |
| 0.1          | 0.7          | 0.2          | 0.8920 | 0.9020 | 0.9254 | 0.4          | 0.5          | 0.1          | 0.9000 | 0.9000 | 0.9180 |
| 0.1          | 0.8          | 0.1          | 0.9220 | 0.8855 | 0.9025 | 0.5          | 0.1          | 0.4          | 0.9050 | 0.8935 | 0.9229 |
| 0.2          | 0.1          | 0.7          | 0.8960 | 0.9035 | 0.8940 | 0.5          | 0.2          | 0.3          | 0.8910 | 0.8945 | 0.9449 |
| 0.2          | 0.2          | 0.6          | 0.9070 | 0.9030 | 0.9368 | 0.5          | 0.3          | 0.2          | 0.8980 | 0.9005 | 0.9564 |
| 0.2          | 0.3          | 0.5          | 0.8995 | 0.9060 | 0.9392 | 0.5          | 0.4          | 0.1          | 0.8855 | 0.9040 | 0.9174 |
| 0.2          | 0.4          | 0.4          | 0.8885 | 0.9005 | 0.9427 | 0.6          | 0.1          | 0.3          | 0.8850 | 0.9070 | 0.9264 |
| 0.2          | 0.5          | 0.3          | 0.8965 | 0.9075 | 0.9473 | 0.6          | 0.2          | 0.2          | 0.9130 | 0.8985 | 0.9393 |
| 0.2          | 0.6          | 0.2          | 0.9045 | 0.9055 | 0.9245 | 0.6          | 0.3          | 0.1          | 0.8945 | 0.8925 | 0.9309 |
| 0.2          | 0.7          | 0.1          | 0.8885 | 0.8985 | 0.8990 | 0.7          | 0.1          | 0.2          | 0.9010 | 0.9160 | 0.9411 |
| 0.3          | 0.1          | 0.6          | 0.8890 | 0.9110 | 0.8892 | 0.7          | 0.2          | 0.1          | 0.8930 | 0.8940 | 0.9458 |
| 0.3          | 0.2          | 0.5          | 0.8890 | 0.8915 | 0.9291 | 0.8          | 0.1          | 0.1          | 0.9030 | 0.8850 | 0.9443 |
| 0.3          | 0.3          | 0.4          | 0.9040 | 0.9070 | 0.9408 | MAX          |              |              | 0.9220 | 0.9160 | 0.9564 |
| 0.3          | 0.4          | 0.3          | 0.9080 | 0.8905 | 0.9474 | MIN          |              |              | 0.8830 | 0.8850 | 0.8838 |

**TABLE 3.2.16 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 6$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9020 | 0.8975 | 0.9181 | 0.3          | 0.5          | 0.2          | 0.9020 | 0.9000 | 0.9035 |
| 0.1          | 0.2          | 0.7          | 0.9025 | 0.8985 | 0.9400 | 0.3          | 0.6          | 0.1          | 0.9075 | 0.8995 | 0.9050 |
| 0.1          | 0.3          | 0.6          | 0.8960 | 0.9105 | 0.9532 | 0.4          | 0.1          | 0.5          | 0.8895 | 0.9045 | 0.9346 |
| 0.1          | 0.4          | 0.5          | 0.9140 | 0.8975 | 0.9439 | 0.4          | 0.2          | 0.4          | 0.8900 | 0.9235 | 0.9478 |
| 0.1          | 0.5          | 0.4          | 0.8985 | 0.8990 | 0.9400 | 0.4          | 0.3          | 0.3          | 0.9025 | 0.8945 | 0.9524 |
| 0.1          | 0.6          | 0.3          | 0.8960 | 0.9035 | 0.9200 | 0.4          | 0.4          | 0.2          | 0.9120 | 0.8965 | 0.9174 |
| 0.1          | 0.7          | 0.2          | 0.8935 | 0.8975 | 0.8989 | 0.4          | 0.5          | 0.1          | 0.8935 | 0.9010 | 0.9120 |
| 0.1          | 0.8          | 0.1          | 0.9015 | 0.9020 | 0.9040 | 0.5          | 0.1          | 0.4          | 0.9040 | 0.9025 | 0.9422 |
| 0.2          | 0.1          | 0.7          | 0.9015 | 0.9005 | 0.9135 | 0.5          | 0.2          | 0.3          | 0.9125 | 0.9035 | 0.9473 |
| 0.2          | 0.2          | 0.6          | 0.8985 | 0.9060 | 0.9443 | 0.5          | 0.3          | 0.2          | 0.9020 | 0.9010 | 0.9119 |
| 0.2          | 0.3          | 0.5          | 0.9070 | 0.9000 | 0.9513 | 0.5          | 0.4          | 0.1          | 0.9115 | 0.8990 | 0.9140 |
| 0.2          | 0.4          | 0.4          | 0.9065 | 0.8945 | 0.9534 | 0.6          | 0.1          | 0.3          | 0.9025 | 0.8990 | 0.9393 |
| 0.2          | 0.5          | 0.3          | 0.8920 | 0.9110 | 0.9255 | 0.6          | 0.2          | 0.2          | 0.9050 | 0.9110 | 0.9434 |
| 0.2          | 0.6          | 0.2          | 0.8845 | 0.9065 | 0.9065 | 0.6          | 0.3          | 0.1          | 0.8965 | 0.8985 | 0.9140 |
| 0.2          | 0.7          | 0.1          | 0.9005 | 0.9030 | 0.9080 | 0.7          | 0.1          | 0.2          | 0.8940 | 0.8980 | 0.9537 |
| 0.3          | 0.1          | 0.6          | 0.8975 | 0.8955 | 0.9313 | 0.7          | 0.2          | 0.1          | 0.8945 | 0.8945 | 0.9255 |
| 0.3          | 0.2          | 0.5          | 0.9070 | 0.8920 | 0.9290 | 0.8          | 0.1          | 0.1          | 0.8995 | 0.8915 | 0.9429 |
| 0.3          | 0.3          | 0.4          | 0.9025 | 0.8955 | 0.9534 | MAX          |              |              | 0.9140 | 0.9235 | 0.9537 |
| 0.3          | 0.4          | 0.3          | 0.9080 | 0.8930 | 0.9282 | MIN          |              |              | 0.8845 | 0.8915 | 0.8989 |

**TABLE 3.2.17 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 12$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8990 | 0.8920 | 0.8874 | 0.3          | 0.5          | 0.2          | 0.9075 | 0.9075 | 0.9463 |
| 0.1          | 0.2          | 0.7          | 0.9090 | 0.8995 | 0.9337 | 0.3          | 0.6          | 0.1          | 0.8960 | 0.8930 | 0.9486 |
| 0.1          | 0.3          | 0.6          | 0.9080 | 0.9030 | 0.9390 | 0.4          | 0.1          | 0.5          | 0.8810 | 0.9060 | 0.8984 |
| 0.1          | 0.4          | 0.5          | 0.8845 | 0.9065 | 0.9376 | 0.4          | 0.2          | 0.4          | 0.8960 | 0.8940 | 0.9341 |
| 0.1          | 0.5          | 0.4          | 0.8975 | 0.9065 | 0.9436 | 0.4          | 0.3          | 0.3          | 0.9110 | 0.8965 | 0.9432 |
| 0.1          | 0.6          | 0.3          | 0.9050 | 0.8990 | 0.9045 | 0.4          | 0.4          | 0.2          | 0.8995 | 0.9060 | 0.9468 |
| 0.1          | 0.7          | 0.2          | 0.8960 | 0.8975 | 0.9483 | 0.4          | 0.5          | 0.1          | 0.8910 | 0.8875 | 0.9455 |
| 0.1          | 0.8          | 0.1          | 0.9010 | 0.9040 | 0.9490 | 0.5          | 0.1          | 0.4          | 0.8940 | 0.8920 | 0.9180 |
| 0.2          | 0.1          | 0.7          | 0.9065 | 0.9040 | 0.9037 | 0.5          | 0.2          | 0.3          | 0.9080 | 0.8940 | 0.9438 |
| 0.2          | 0.2          | 0.6          | 0.9005 | 0.8965 | 0.9216 | 0.5          | 0.3          | 0.2          | 0.9050 | 0.9115 | 0.9513 |
| 0.2          | 0.3          | 0.5          | 0.9000 | 0.9005 | 0.9354 | 0.5          | 0.4          | 0.1          | 0.9050 | 0.9000 | 0.9530 |
| 0.2          | 0.4          | 0.4          | 0.9065 | 0.8985 | 0.9354 | 0.6          | 0.1          | 0.3          | 0.9060 | 0.9050 | 0.9221 |
| 0.2          | 0.5          | 0.3          | 0.9075 | 0.9055 | 0.9454 | 0.6          | 0.2          | 0.2          | 0.8925 | 0.8985 | 0.9503 |
| 0.2          | 0.6          | 0.2          | 0.8915 | 0.8955 | 0.9424 | 0.6          | 0.3          | 0.1          | 0.9030 | 0.8980 | 0.9458 |
| 0.2          | 0.7          | 0.1          | 0.8940 | 0.8960 | 0.9593 | 0.7          | 0.1          | 0.2          | 0.8815 | 0.9065 | 0.9311 |
| 0.3          | 0.1          | 0.6          | 0.8990 | 0.9030 | 0.8968 | 0.7          | 0.2          | 0.1          | 0.9090 | 0.9050 | 0.9349 |
| 0.3          | 0.2          | 0.5          | 0.9005 | 0.8960 | 0.9232 | 0.8          | 0.1          | 0.1          | 0.8935 | 0.9110 | 0.9490 |
| 0.3          | 0.3          | 0.4          | 0.9130 | 0.9075 | 0.9452 | MAX          |              |              | 0.9130 | 0.9115 | 0.9593 |
| 0.3          | 0.4          | 0.3          | 0.8980 | 0.8995 | 0.9446 | MIN          |              |              | 0.8810 | 0.8875 | 0.8874 |



**TABLE 3.2.18 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 12$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8935 | 0.9005 | 0.9137 | 0.3          | 0.5          | 0.2          | 0.8905 | 0.8980 | 0.9441 |
| 0.1          | 0.2          | 0.7          | 0.8895 | 0.8930 | 0.9289 | 0.3          | 0.6          | 0.1          | 0.9075 | 0.8990 | 0.9418 |
| 0.1          | 0.3          | 0.6          | 0.8855 | 0.9075 | 0.9377 | 0.4          | 0.1          | 0.5          | 0.9060 | 0.9065 | 0.9366 |
| 0.1          | 0.4          | 0.5          | 0.8955 | 0.8804 | 0.9376 | 0.4          | 0.2          | 0.4          | 0.8905 | 0.9095 | 0.9529 |
| 0.1          | 0.5          | 0.4          | 0.8975 | 0.9110 | 0.9558 | 0.4          | 0.3          | 0.3          | 0.9000 | 0.9035 | 0.9510 |
| 0.1          | 0.6          | 0.3          | 0.8975 | 0.9065 | 0.9505 | 0.4          | 0.4          | 0.2          | 0.9065 | 0.9080 | 0.9490 |
| 0.1          | 0.7          | 0.2          | 0.9000 | 0.8835 | 0.9467 | 0.4          | 0.5          | 0.1          | 0.8975 | 0.9005 | 0.9518 |
| 0.1          | 0.8          | 0.1          | 0.9090 | 0.9005 | 0.9172 | 0.5          | 0.1          | 0.4          | 0.8975 | 0.9060 | 0.9372 |
| 0.2          | 0.1          | 0.7          | 0.9025 | 0.9065 | 0.9146 | 0.5          | 0.2          | 0.3          | 0.9050 | 0.8980 | 0.9491 |
| 0.2          | 0.2          | 0.6          | 0.9050 | 0.8975 | 0.9332 | 0.5          | 0.3          | 0.2          | 0.9015 | 0.8945 | 0.9492 |
| 0.2          | 0.3          | 0.5          | 0.9095 | 0.9035 | 0.9431 | 0.5          | 0.4          | 0.1          | 0.9020 | 0.8945 | 0.9472 |
| 0.2          | 0.4          | 0.4          | 0.8970 | 0.9130 | 0.9349 | 0.6          | 0.1          | 0.3          | 0.8945 | 0.8965 | 0.9298 |
| 0.2          | 0.5          | 0.3          | 0.9015 | 0.8935 | 0.9523 | 0.6          | 0.2          | 0.2          | 0.9050 | 0.8980 | 0.9508 |
| 0.2          | 0.6          | 0.2          | 0.9045 | 0.9055 | 0.9496 | 0.6          | 0.3          | 0.1          | 0.8905 | 0.9005 | 0.9477 |
| 0.2          | 0.7          | 0.1          | 0.9055 | 0.8940 | 0.9376 | 0.7          | 0.1          | 0.2          | 0.9120 | 0.9025 | 0.9383 |
| 0.3          | 0.1          | 0.6          | 0.8970 | 0.8920 | 0.9272 | 0.7          | 0.2          | 0.1          | 0.8875 | 0.8960 | 0.9495 |
| 0.3          | 0.2          | 0.5          | 0.8920 | 0.8980 | 0.9399 | 0.8          | 0.1          | 0.1          | 0.9015 | 0.9115 | 0.9489 |
| 0.3          | 0.3          | 0.4          | 0.8955 | 0.9020 | 0.9453 | MAX          |              |              | 0.9120 | 0.9130 | 0.9558 |
| 0.3          | 0.4          | 0.3          | 0.8955 | 0.9070 | 0.9513 | MIN          |              |              | 0.8855 | 0.8804 | 0.9137 |



**TABLE 3.2.19 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 12$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8930 | 0.9030 | 0.9214 | 0.3          | 0.5          | 0.2          | 0.8960 | 0.8980 | 0.9050 |
| 0.1          | 0.2          | 0.7          | 0.9015 | 0.8890 | 0.9442 | 0.3          | 0.6          | 0.1          | 0.8980 | 0.9055 | 0.9085 |
| 0.1          | 0.3          | 0.6          | 0.8990 | 0.9045 | 0.9462 | 0.4          | 0.1          | 0.5          | 0.8985 | 0.9020 | 0.9337 |
| 0.1          | 0.4          | 0.5          | 0.9080 | 0.8815 | 0.9469 | 0.4          | 0.2          | 0.4          | 0.8950 | 0.9045 | 0.9437 |
| 0.1          | 0.5          | 0.4          | 0.9025 | 0.9030 | 0.9359 | 0.4          | 0.3          | 0.3          | 0.9030 | 0.9010 | 0.9499 |
| 0.1          | 0.6          | 0.3          | 0.8955 | 0.9020 | 0.9209 | 0.4          | 0.4          | 0.2          | 0.8980 | 0.9000 | 0.9209 |
| 0.1          | 0.7          | 0.2          | 0.9015 | 0.9085 | 0.9035 | 0.4          | 0.5          | 0.1          | 0.9015 | 0.8925 | 0.9040 |
| 0.1          | 0.8          | 0.1          | 0.9055 | 0.9015 | 0.9025 | 0.5          | 0.1          | 0.4          | 0.9040 | 0.8920 | 0.9400 |
| 0.2          | 0.1          | 0.7          | 0.8955 | 0.8960 | 0.9200 | 0.5          | 0.2          | 0.3          | 0.9015 | 0.9005 | 0.9528 |
| 0.2          | 0.2          | 0.6          | 0.8950 | 0.9015 | 0.9430 | 0.5          | 0.3          | 0.2          | 0.9060 | 0.9015 | 0.9209 |
| 0.2          | 0.3          | 0.5          | 0.9035 | 0.9045 | 0.9528 | 0.5          | 0.4          | 0.1          | 0.9085 | 0.8930 | 0.9140 |
| 0.2          | 0.4          | 0.4          | 0.8900 | 0.8950 | 0.9474 | 0.6          | 0.1          | 0.3          | 0.8905 | 0.9075 | 0.9404 |
| 0.2          | 0.5          | 0.3          | 0.8965 | 0.8975 | 0.9100 | 0.6          | 0.2          | 0.2          | 0.9095 | 0.9020 | 0.9434 |
| 0.2          | 0.6          | 0.2          | 0.8870 | 0.8970 | 0.9055 | 0.6          | 0.3          | 0.1          | 0.9045 | 0.8930 | 0.9030 |
| 0.2          | 0.7          | 0.1          | 0.9130 | 0.9040 | 0.9040 | 0.7          | 0.1          | 0.2          | 0.9015 | 0.8930 | 0.9426 |
| 0.3          | 0.1          | 0.6          | 0.8995 | 0.9005 | 0.9425 | 0.7          | 0.2          | 0.1          | 0.9040 | 0.9015 | 0.9205 |
| 0.3          | 0.2          | 0.5          | 0.9000 | 0.8970 | 0.9353 | 0.8          | 0.1          | 0.1          | 0.9075 | 0.8970 | 0.9439 |
| 0.3          | 0.3          | 0.4          | 0.9030 | 0.8875 | 0.9418 | MAX          |              |              | 0.9130 | 0.9130 | 0.9528 |
| 0.3          | 0.4          | 0.3          | 0.9090 | 0.9130 | 0.9354 | MIN          |              |              | 0.8870 | 0.8815 | 0.9025 |

**TABLE 3.2.20 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 12$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8895 | 0.8920 | 0.9405 | 0.3          | 0.5          | 0.2          | 0.8935 | 0.9095 | 0.9110 |
| 0.1          | 0.2          | 0.7          | 0.9060 | 0.9065 | 0.9553 | 0.3          | 0.6          | 0.1          | 0.8995 | 0.9030 | 0.9010 |
| 0.1          | 0.3          | 0.6          | 0.8950 | 0.8925 | 0.9414 | 0.4          | 0.1          | 0.5          | 0.9040 | 0.9055 | 0.9366 |
| 0.1          | 0.4          | 0.5          | 0.8970 | 0.9075 | 0.9279 | 0.4          | 0.2          | 0.4          | 0.8990 | 0.9035 | 0.9498 |
| 0.1          | 0.5          | 0.4          | 0.9065 | 0.8915 | 0.9115 | 0.4          | 0.3          | 0.3          | 0.9065 | 0.8855 | 0.9024 |
| 0.1          | 0.6          | 0.3          | 0.9130 | 0.8950 | 0.9060 | 0.4          | 0.4          | 0.2          | 0.9020 | 0.9010 | 0.9110 |
| 0.1          | 0.7          | 0.2          | 0.9005 | 0.9080 | 0.8980 | 0.4          | 0.5          | 0.1          | 0.8980 | 0.8960 | 0.9080 |
| 0.1          | 0.8          | 0.1          | 0.8980 | 0.9050 | 0.8960 | 0.5          | 0.1          | 0.4          | 0.8915 | 0.8980 | 0.9463 |
| 0.2          | 0.1          | 0.7          | 0.8970 | 0.8865 | 0.9337 | 0.5          | 0.2          | 0.3          | 0.9070 | 0.8935 | 0.9324 |
| 0.2          | 0.2          | 0.6          | 0.9060 | 0.9065 | 0.9371 | 0.5          | 0.3          | 0.2          | 0.8850 | 0.8970 | 0.8950 |
| 0.2          | 0.3          | 0.5          | 0.8915 | 0.8970 | 0.9294 | 0.5          | 0.4          | 0.1          | 0.9005 | 0.8935 | 0.9080 |
| 0.2          | 0.4          | 0.4          | 0.9085 | 0.9095 | 0.9550 | 0.6          | 0.1          | 0.3          | 0.9050 | 0.9055 | 0.9478 |
| 0.2          | 0.5          | 0.3          | 0.9065 | 0.9040 | 0.9199 | 0.6          | 0.2          | 0.2          | 0.9115 | 0.8970 | 0.9500 |
| 0.2          | 0.6          | 0.2          | 0.8965 | 0.8975 | 0.9025 | 0.6          | 0.3          | 0.1          | 0.9080 | 0.9070 | 0.8980 |
| 0.2          | 0.7          | 0.1          | 0.8870 | 0.9005 | 0.9015 | 0.7          | 0.1          | 0.2          | 0.8940 | 0.8890 | 0.9529 |
| 0.3          | 0.1          | 0.6          | 0.8980 | 0.9025 | 0.9347 | 0.7          | 0.2          | 0.1          | 0.8980 | 0.9005 | 0.9210 |
| 0.3          | 0.2          | 0.5          | 0.8925 | 0.8995 | 0.9470 | 0.8          | 0.1          | 0.1          | 0.8860 | 0.9015 | 0.9115 |
| 0.3          | 0.3          | 0.4          | 0.9035 | 0.9075 | 0.9290 | MAX          |              |              | 0.9130 | 0.9095 | 0.9553 |
| 0.3          | 0.4          | 0.3          | 0.8990 | 0.8980 | 0.9200 | MIN          |              |              | 0.8850 | 0.8855 | 0.8950 |

**TABLE 3.2.21 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 24$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9100 | 0.9040 | 0.9128 | 0.3          | 0.5          | 0.2          | 0.8985 | 0.8950 | 0.9491 |
| 0.1          | 0.2          | 0.7          | 0.8940 | 0.9115 | 0.9363 | 0.3          | 0.6          | 0.1          | 0.9020 | 0.8985 | 0.9453 |
| 0.1          | 0.3          | 0.6          | 0.8980 | 0.8970 | 0.9459 | 0.4          | 0.1          | 0.5          | 0.8980 | 0.8960 | 0.9293 |
| 0.1          | 0.4          | 0.5          | 0.8965 | 0.9050 | 0.9492 | 0.4          | 0.2          | 0.4          | 0.8875 | 0.9070 | 0.9392 |
| 0.1          | 0.5          | 0.4          | 0.9115 | 0.8925 | 0.9430 | 0.4          | 0.3          | 0.3          | 0.9080 | 0.8990 | 0.9461 |
| 0.1          | 0.6          | 0.3          | 0.8930 | 0.9080 | 0.9447 | 0.4          | 0.4          | 0.2          | 0.9015 | 0.8945 | 0.9499 |
| 0.1          | 0.7          | 0.2          | 0.9095 | 0.8875 | 0.9482 | 0.4          | 0.5          | 0.1          | 0.8975 | 0.8940 | 0.9478 |
| 0.1          | 0.8          | 0.1          | 0.8955 | 0.8895 | 0.9244 | 0.5          | 0.1          | 0.4          | 0.9000 | 0.8980 | 0.9386 |
| 0.2          | 0.1          | 0.7          | 0.9035 | 0.8980 | 0.9252 | 0.5          | 0.2          | 0.3          | 0.8815 | 0.9020 | 0.9477 |
| 0.2          | 0.2          | 0.6          | 0.8915 | 0.8945 | 0.9430 | 0.5          | 0.3          | 0.2          | 0.9050 | 0.8990 | 0.9506 |
| 0.2          | 0.3          | 0.5          | 0.8935 | 0.8940 | 0.9424 | 0.5          | 0.4          | 0.1          | 0.8920 | 0.8980 | 0.9410 |
| 0.2          | 0.4          | 0.4          | 0.9015 | 0.9025 | 0.9455 | 0.6          | 0.1          | 0.3          | 0.9040 | 0.9055 | 0.9408 |
| 0.2          | 0.5          | 0.3          | 0.8805 | 0.8905 | 0.9520 | 0.6          | 0.2          | 0.2          | 0.9145 | 0.9010 | 0.9562 |
| 0.2          | 0.6          | 0.2          | 0.8985 | 0.9065 | 0.9577 | 0.6          | 0.3          | 0.1          | 0.9045 | 0.8970 | 0.9577 |
| 0.2          | 0.7          | 0.1          | 0.8980 | 0.9050 | 0.9323 | 0.7          | 0.1          | 0.2          | 0.8885 | 0.8875 | 0.9401 |
| 0.3          | 0.1          | 0.6          | 0.8885 | 0.8995 | 0.9214 | 0.7          | 0.2          | 0.1          | 0.8965 | 0.9080 | 0.9500 |
| 0.3          | 0.2          | 0.5          | 0.9005 | 0.8970 | 0.9385 | 0.8          | 0.1          | 0.1          | 0.9110 | 0.9115 | 0.9542 |
| 0.3          | 0.3          | 0.4          | 0.8960 | 0.8920 | 0.9501 | MAX          |              |              | 0.9145 | 0.9115 | 0.9577 |
| 0.3          | 0.4          | 0.3          | 0.9050 | 0.9050 | 0.9421 | MIN          |              |              | 0.8805 | 0.8875 | 0.9128 |

**TABLE 3.2.22 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 24$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9070 | 0.9055 | 0.9355 | 0.3          | 0.5          | 0.2          | 0.8950 | 0.8890 | 0.9396 |
| 0.1          | 0.2          | 0.7          | 0.8965 | 0.9005 | 0.9445 | 0.3          | 0.6          | 0.1          | 0.9015 | 0.9085 | 0.9168 |
| 0.1          | 0.3          | 0.6          | 0.8915 | 0.8920 | 0.9576 | 0.4          | 0.1          | 0.5          | 0.9010 | 0.9020 | 0.9338 |
| 0.1          | 0.4          | 0.5          | 0.8910 | 0.9005 | 0.9502 | 0.4          | 0.2          | 0.4          | 0.8995 | 0.8945 | 0.9408 |
| 0.1          | 0.5          | 0.4          | 0.9010 | 0.8920 | 0.9471 | 0.4          | 0.3          | 0.3          | 0.9095 | 0.8960 | 0.9508 |
| 0.1          | 0.6          | 0.3          | 0.9015 | 0.9030 | 0.9527 | 0.4          | 0.4          | 0.2          | 0.9015 | 0.9000 | 0.9400 |
| 0.1          | 0.7          | 0.2          | 0.8990 | 0.8950 | 0.9283 | 0.4          | 0.5          | 0.1          | 0.9065 | 0.9015 | 0.9193 |
| 0.1          | 0.8          | 0.1          | 0.8880 | 0.9015 | 0.9189 | 0.5          | 0.1          | 0.4          | 0.8985 | 0.9035 | 0.9308 |
| 0.2          | 0.1          | 0.7          | 0.8845 | 0.9035 | 0.9476 | 0.5          | 0.2          | 0.3          | 0.9055 | 0.8925 | 0.9442 |
| 0.2          | 0.2          | 0.6          | 0.8950 | 0.8940 | 0.9408 | 0.5          | 0.3          | 0.2          | 0.9040 | 0.8940 | 0.9535 |
| 0.2          | 0.3          | 0.5          | 0.9055 | 0.8990 | 0.9482 | 0.5          | 0.4          | 0.1          | 0.8955 | 0.9080 | 0.9253 |
| 0.2          | 0.4          | 0.4          | 0.8975 | 0.9025 | 0.9489 | 0.6          | 0.1          | 0.3          | 0.8850 | 0.8960 | 0.9399 |
| 0.2          | 0.5          | 0.3          | 0.9000 | 0.9015 | 0.9460 | 0.6          | 0.2          | 0.2          | 0.8925 | 0.9080 | 0.9494 |
| 0.2          | 0.6          | 0.2          | 0.8930 | 0.8955 | 0.9502 | 0.6          | 0.3          | 0.1          | 0.9005 | 0.9125 | 0.9462 |
| 0.2          | 0.7          | 0.1          | 0.9005 | 0.9050 | 0.9164 | 0.7          | 0.1          | 0.2          | 0.8995 | 0.8940 | 0.9402 |
| 0.3          | 0.1          | 0.6          | 0.9025 | 0.9090 | 0.9323 | 0.7          | 0.2          | 0.1          | 0.8990 | 0.9015 | 0.9581 |
| 0.3          | 0.2          | 0.5          | 0.9055 | 0.8965 | 0.9492 | 0.8          | 0.1          | 0.1          | 0.9115 | 0.9125 | 0.9499 |
| 0.3          | 0.3          | 0.4          | 0.9020 | 0.8995 | 0.9511 | MAX          |              |              | 0.9115 | 0.9125 | 0.9581 |
| 0.3          | 0.4          | 0.3          | 0.9065 | 0.8885 | 0.9456 | MIN          |              |              | 0.8845 | 0.8885 | 0.9164 |

**TABLE 3.2.23 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 24$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.9050 | 0.8975 | 0.9323 | 0.3          | 0.5          | 0.2          | 0.9020 | 0.8745 | 0.9100 |
| 0.1          | 0.2          | 0.7          | 0.9030 | 0.9070 | 0.9418 | 0.3          | 0.6          | 0.1          | 0.9020 | 0.9075 | 0.9000 |
| 0.1          | 0.3          | 0.6          | 0.8965 | 0.8975 | 0.9494 | 0.4          | 0.1          | 0.5          | 0.8995 | 0.8980 | 0.9427 |
| 0.1          | 0.4          | 0.5          | 0.9010 | 0.8985 | 0.9350 | 0.4          | 0.2          | 0.4          | 0.9105 | 0.8970 | 0.9524 |
| 0.1          | 0.5          | 0.4          | 0.9040 | 0.9070 | 0.9020 | 0.4          | 0.3          | 0.3          | 0.9075 | 0.8940 | 0.9134 |
| 0.1          | 0.6          | 0.3          | 0.9025 | 0.8925 | 0.9105 | 0.4          | 0.4          | 0.2          | 0.8970 | 0.9015 | 0.9160 |
| 0.1          | 0.7          | 0.2          | 0.9110 | 0.9125 | 0.9010 | 0.4          | 0.5          | 0.1          | 0.8975 | 0.9025 | 0.8920 |
| 0.1          | 0.8          | 0.1          | 0.9045 | 0.8975 | 0.8880 | 0.5          | 0.1          | 0.4          | 0.9035 | 0.9060 | 0.9486 |
| 0.2          | 0.1          | 0.7          | 0.8970 | 0.8905 | 0.9376 | 0.5          | 0.2          | 0.3          | 0.9125 | 0.9040 | 0.9354 |
| 0.2          | 0.2          | 0.6          | 0.8925 | 0.8995 | 0.9453 | 0.5          | 0.3          | 0.2          | 0.8905 | 0.8795 | 0.9125 |
| 0.2          | 0.3          | 0.5          | 0.8975 | 0.8975 | 0.9419 | 0.5          | 0.4          | 0.1          | 0.9000 | 0.8875 | 0.9070 |
| 0.2          | 0.4          | 0.4          | 0.9075 | 0.9045 | 0.9230 | 0.6          | 0.1          | 0.3          | 0.9045 | 0.8950 | 0.9558 |
| 0.2          | 0.5          | 0.3          | 0.8995 | 0.9095 | 0.8990 | 0.6          | 0.2          | 0.2          | 0.8870 | 0.9085 | 0.9079 |
| 0.2          | 0.6          | 0.2          | 0.9045 | 0.8970 | 0.9035 | 0.6          | 0.3          | 0.1          | 0.9095 | 0.9025 | 0.8965 |
| 0.2          | 0.7          | 0.1          | 0.9030 | 0.9125 | 0.8965 | 0.7          | 0.1          | 0.2          | 0.9085 | 0.8990 | 0.9435 |
| 0.3          | 0.1          | 0.6          | 0.9030 | 0.8995 | 0.9414 | 0.7          | 0.2          | 0.1          | 0.8975 | 0.9075 | 0.9060 |
| 0.3          | 0.2          | 0.5          | 0.8890 | 0.9045 | 0.9509 | 0.8          | 0.1          | 0.1          | 0.8950 | 0.8855 | 0.9144 |
| 0.3          | 0.3          | 0.4          | 0.9065 | 0.9050 | 0.9280 | MAX          |              |              | 0.9125 | 0.9125 | 0.9558 |
| 0.3          | 0.4          | 0.3          | 0.9055 | 0.8940 | 0.9509 | MIN          |              |              | 0.8870 | 0.8745 | 0.8880 |

**TABLE 3.2.24 Range of Simulated Confidence**

**Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$**

**when  $I = 24$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | MIXED  |
|--------------|--------------|--------------|--------|--------|--------|--------------|--------------|--------------|--------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8945 | 0.9025 | 0.9512 | 0.3          | 0.5          | 0.2          | 0.9045 | 0.8865 | 0.9005 |
| 0.1          | 0.2          | 0.7          | 0.8940 | 0.9030 | 0.9424 | 0.3          | 0.6          | 0.1          | 0.9010 | 0.8945 | 0.8895 |
| 0.1          | 0.3          | 0.6          | 0.8985 | 0.9080 | 0.9225 | 0.4          | 0.1          | 0.5          | 0.9085 | 0.9025 | 0.9478 |
| 0.1          | 0.4          | 0.5          | 0.8905 | 0.9060 | 0.9030 | 0.4          | 0.2          | 0.4          | 0.9050 | 0.9080 | 0.9190 |
| 0.1          | 0.5          | 0.4          | 0.9110 | 0.9085 | 0.9030 | 0.4          | 0.3          | 0.3          | 0.9065 | 0.8980 | 0.9065 |
| 0.1          | 0.6          | 0.3          | 0.8870 | 0.8875 | 0.9045 | 0.4          | 0.4          | 0.2          | 0.9075 | 0.8945 | 0.9055 |
| 0.1          | 0.7          | 0.2          | 0.9070 | 0.8920 | 0.8970 | 0.4          | 0.5          | 0.1          | 0.9115 | 0.8965 | 0.9110 |
| 0.1          | 0.8          | 0.1          | 0.8895 | 0.8945 | 0.8940 | 0.5          | 0.1          | 0.4          | 0.9145 | 0.9080 | 0.9539 |
| 0.2          | 0.1          | 0.7          | 0.8990 | 0.8835 | 0.9418 | 0.5          | 0.2          | 0.3          | 0.9115 | 0.8870 | 0.9130 |
| 0.2          | 0.2          | 0.6          | 0.8960 | 0.9030 | 0.9389 | 0.5          | 0.3          | 0.2          | 0.9075 | 0.9065 | 0.9010 |
| 0.2          | 0.3          | 0.5          | 0.9010 | 0.8970 | 0.9055 | 0.5          | 0.4          | 0.1          | 0.9150 | 0.8970 | 0.9030 |
| 0.2          | 0.4          | 0.4          | 0.8940 | 0.9060 | 0.9025 | 0.6          | 0.1          | 0.3          | 0.8960 | 0.9070 | 0.9263 |
| 0.2          | 0.5          | 0.3          | 0.9010 | 0.8975 | 0.9020 | 0.6          | 0.2          | 0.2          | 0.8935 | 0.9005 | 0.9015 |
| 0.2          | 0.6          | 0.2          | 0.9035 | 0.8950 | 0.9025 | 0.6          | 0.3          | 0.1          | 0.8920 | 0.8950 | 0.9000 |
| 0.2          | 0.7          | 0.1          | 0.9090 | 0.9015 | 0.8970 | 0.7          | 0.1          | 0.2          | 0.8940 | 0.8990 | 0.9124 |
| 0.3          | 0.1          | 0.6          | 0.9020 | 0.8995 | 0.9429 | 0.7          | 0.2          | 0.1          | 0.9020 | 0.8960 | 0.9070 |
| 0.3          | 0.2          | 0.5          | 0.8920 | 0.8920 | 0.9175 | 0.8          | 0.1          | 0.1          | 0.8945 | 0.9055 | 0.9080 |
| 0.3          | 0.3          | 0.4          | 0.8855 | 0.9060 | 0.9130 | MAX          |              |              | 0.9150 | 0.9105 | 0.9539 |
| 0.3          | 0.4          | 0.3          | 0.8990 | 0.9105 | 0.9100 | MIN          |              |              | 0.8855 | 0.8835 | 0.8895 |

**TABLE 3.2.25 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 6$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 1.1262 | 1.1460 | 0.3          | 0.5          | 0.2          | 1.7132 | 1.6978 |
| 0.1          | 0.2          | 0.7          | 1.0601 | 1.1089 | 0.3          | 0.6          | 0.1          | 1.6253 | 1.6331 |
| 0.1          | 0.3          | 0.6          | 1.0163 | 0.9922 | 0.4          | 0.1          | 0.5          | 2.5179 | 2.4996 |
| 0.1          | 0.4          | 0.5          | 0.9339 | 0.9247 | 0.4          | 0.2          | 0.4          | 2.4328 | 2.4076 |
| 0.1          | 0.5          | 0.4          | 0.8474 | 0.8290 | 0.4          | 0.3          | 0.3          | 2.2953 | 2.3254 |
| 0.1          | 0.6          | 0.3          | 0.7598 | 0.7649 | 0.4          | 0.4          | 0.2          | 2.2911 | 2.2928 |
| 0.1          | 0.7          | 0.2          | 0.6877 | 0.6984 | 0.4          | 0.5          | 0.1          | 2.1744 | 2.1580 |
| 0.1          | 0.8          | 0.1          | 0.6200 | 0.6064 | 0.5          | 0.1          | 0.4          | 2.9832 | 2.9482 |
| 0.2          | 0.1          | 0.7          | 1.6787 | 1.6088 | 0.5          | 0.2          | 0.3          | 2.8803 | 2.9150 |
| 0.2          | 0.2          | 0.6          | 1.5198 | 1.5357 | 0.5          | 0.3          | 0.2          | 2.8137 | 2.7727 |
| 0.2          | 0.3          | 0.5          | 1.4796 | 1.4629 | 0.5          | 0.4          | 0.1          | 2.6849 | 2.6597 |
| 0.2          | 0.4          | 0.4          | 1.3743 | 1.3793 | 0.6          | 0.1          | 0.3          | 3.2913 | 3.3660 |
| 0.2          | 0.5          | 0.3          | 1.2931 | 1.3437 | 0.6          | 0.2          | 0.2          | 3.3513 | 3.2406 |
| 0.2          | 0.6          | 0.2          | 1.2074 | 1.2236 | 0.6          | 0.3          | 0.1          | 3.2318 | 3.2366 |
| 0.2          | 0.7          | 0.1          | 1.1204 | 1.1385 | 0.7          | 0.1          | 0.2          | 3.9461 | 3.8537 |
| 0.3          | 0.1          | 0.6          | 2.0503 | 2.0786 | 0.7          | 0.2          | 0.1          | 3.7367 | 3.7273 |
| 0.3          | 0.2          | 0.5          | 1.9672 | 1.9690 | 0.8          | 0.1          | 0.1          | 4.3023 | 4.2727 |
| 0.3          | 0.3          | 0.4          | 1.9139 | 1.8609 | MAX          |              |              | 4.3023 | 4.2727 |
| 0.3          | 0.4          | 0.3          | 1.7874 | 1.8308 | MIN          |              |              | 0.6200 | 0.6064 |

**TABLE 3.2.26 Range of Average Interval Lengths**

**for 90% Two-sided Intervals on  $\sigma_P^2$**

**when  $I = 6$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8489 | 0.8715 | 0.3          | 0.5          | 0.2          | 1.6354 | 1.6691 |
| 0.1          | 0.2          | 0.7          | 0.8012 | 0.8012 | 0.3          | 0.6          | 0.1          | 1.5952 | 1.6152 |
| 0.1          | 0.3          | 0.6          | 0.7635 | 0.7589 | 0.4          | 0.1          | 0.5          | 2.2548 | 2.2801 |
| 0.1          | 0.4          | 0.5          | 0.9345 | 0.7224 | 0.4          | 0.2          | 0.4          | 2.1952 | 2.2485 |
| 0.1          | 0.5          | 0.4          | 0.6867 | 0.6917 | 0.4          | 0.3          | 0.3          | 2.1831 | 2.2602 |
| 0.1          | 0.6          | 0.3          | 0.6560 | 0.6582 | 0.4          | 0.4          | 0.2          | 2.1780 | 2.1948 |
| 0.1          | 0.7          | 0.2          | 0.6093 | 0.6217 | 0.4          | 0.5          | 0.1          | 2.1104 | 2.1622 |
| 0.1          | 0.8          | 0.1          | 0.5752 | 0.5551 | 0.5          | 0.1          | 0.4          | 2.7140 | 2.7444 |
| 0.2          | 0.1          | 0.7          | 1.3199 | 1.3714 | 0.5          | 0.2          | 0.3          | 2.7360 | 2.7795 |
| 0.2          | 0.2          | 0.6          | 1.3138 | 1.2801 | 0.5          | 0.3          | 0.2          | 2.6933 | 2.6976 |
| 0.2          | 0.3          | 0.5          | 1.2663 | 1.2550 | 0.5          | 0.4          | 0.1          | 2.5901 | 2.6117 |
| 0.2          | 0.4          | 0.4          | 1.2039 | 1.2075 | 0.6          | 0.1          | 0.3          | 3.2218 | 3.1447 |
| 0.2          | 0.5          | 0.3          | 1.2111 | 1.1407 | 0.6          | 0.2          | 0.2          | 3.1824 | 3.2126 |
| 0.2          | 0.6          | 0.2          | 1.1123 | 1.1606 | 0.6          | 0.3          | 0.1          | 3.1398 | 3.1563 |
| 0.2          | 0.7          | 0.1          | 1.0878 | 1.0996 | 0.7          | 0.1          | 0.2          | 3.6908 | 3.7148 |
| 0.3          | 0.1          | 0.6          | 1.7907 | 1.8806 | 0.7          | 0.2          | 0.1          | 3.6514 | 3.6651 |
| 0.3          | 0.2          | 0.5          | 1.7740 | 1.7825 | 0.8          | 0.1          | 0.1          | 4.2062 | 4.2487 |
| 0.3          | 0.3          | 0.4          | 1.7156 | 1.7179 | MAX          |              |              | 4.2062 | 4.2487 |
| 0.3          | 0.4          | 0.3          | 1.7133 | 1.6674 | MIN          |              |              | 0.5752 | 0.5551 |



**TABLE 3.2.27 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 6$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8508 | 0.8383 | 0.3          | 0.5          | 0.2          | 1.6025 | 1.6570 |
| 0.1          | 0.2          | 0.7          | 0.7830 | 0.8057 | 0.3          | 0.6          | 0.1          | 1.5881 | 1.5725 |
| 0.1          | 0.3          | 0.6          | 0.7899 | 0.7624 | 0.4          | 0.1          | 0.5          | 2.3088 | 2.2571 |
| 0.1          | 0.4          | 0.5          | 0.7277 | 0.7254 | 0.4          | 0.2          | 0.4          | 2.2425 | 2.2332 |
| 0.1          | 0.5          | 0.4          | 0.6917 | 0.7132 | 0.4          | 0.3          | 0.3          | 2.2592 | 2.1384 |
| 0.1          | 0.6          | 0.3          | 0.6379 | 0.6631 | 0.4          | 0.4          | 0.2          | 2.1749 | 2.1462 |
| 0.1          | 0.7          | 0.2          | 0.5940 | 0.6072 | 0.4          | 0.5          | 0.1          | 2.1150 | 2.1448 |
| 0.1          | 0.8          | 0.1          | 0.5578 | 0.5784 | 0.5          | 0.1          | 0.4          | 2.8589 | 2.7558 |
| 0.2          | 0.1          | 0.7          | 1.3285 | 1.3379 | 0.5          | 0.2          | 0.3          | 2.7084 | 2.7267 |
| 0.2          | 0.2          | 0.6          | 1.3196 | 1.2925 | 0.5          | 0.3          | 0.2          | 2.6523 | 2.7369 |
| 0.2          | 0.3          | 0.5          | 1.2612 | 1.2511 | 0.5          | 0.4          | 0.1          | 2.6438 | 2.6737 |
| 0.2          | 0.4          | 0.4          | 1.1981 | 1.2074 | 0.6          | 0.1          | 0.3          | 3.2162 | 3.1791 |
| 0.2          | 0.5          | 0.3          | 1.1836 | 1.1755 | 0.6          | 0.2          | 0.2          | 3.1647 | 3.1806 |
| 0.2          | 0.6          | 0.2          | 1.1243 | 1.1135 | 0.6          | 0.3          | 0.1          | 3.1363 | 3.1557 |
| 0.2          | 0.7          | 0.1          | 1.0783 | 1.0714 | 0.7          | 0.1          | 0.2          | 3.6981 | 3.7417 |
| 0.3          | 0.1          | 0.6          | 1.8027 | 1.7598 | 0.7          | 0.2          | 0.1          | 3.7953 | 3.5948 |
| 0.3          | 0.2          | 0.5          | 1.8013 | 1.7862 | 0.8          | 0.1          | 0.1          | 4.1315 | 4.1805 |
| 0.3          | 0.3          | 0.4          | 1.7210 | 1.7837 | MAX          |              |              | 4.1315 | 4.1805 |
| 0.3          | 0.4          | 0.3          | 1.7349 | 1.7014 | MIN          |              |              | 0.5578 | 0.5784 |

**TABLE 3.2.28 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 6$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.6856 | 0.6994 | 0.3          | 0.5          | 0.2          | 1.6187 | 1.6479 |
| 0.1          | 0.2          | 0.7          | 0.6577 | 0.6718 | 0.3          | 0.6          | 0.1          | 1.5872 | 1.5873 |
| 0.1          | 0.3          | 0.6          | 0.6625 | 0.6562 | 0.4          | 0.1          | 0.5          | 2.1623 | 2.1605 |
| 0.1          | 0.4          | 0.5          | 0.6316 | 0.6106 | 0.4          | 0.2          | 0.4          | 2.1626 | 2.1880 |
| 0.1          | 0.5          | 0.4          | 0.6176 | 0.6128 | 0.4          | 0.3          | 0.3          | 2.1362 | 2.1148 |
| 0.1          | 0.6          | 0.3          | 0.5757 | 0.5857 | 0.4          | 0.4          | 0.2          | 2.1480 | 2.0860 |
| 0.1          | 0.7          | 0.2          | 0.5565 | 0.5621 | 0.4          | 0.5          | 0.1          | 2.1074 | 2.0822 |
| 0.1          | 0.8          | 0.1          | 0.5539 | 0.5329 | 0.5          | 0.1          | 0.4          | 2.6991 | 2.7021 |
| 0.2          | 0.1          | 0.7          | 1.2075 | 1.2039 | 0.5          | 0.2          | 0.3          | 2.6475 | 2.6507 |
| 0.2          | 0.2          | 0.6          | 1.1877 | 1.1883 | 0.5          | 0.3          | 0.2          | 2.7089 | 2.6345 |
| 0.2          | 0.3          | 0.5          | 1.1588 | 1.1493 | 0.5          | 0.4          | 0.1          | 2.5572 | 2.5863 |
| 0.2          | 0.4          | 0.4          | 1.1093 | 1.1666 | 0.6          | 0.1          | 0.3          | 3.1689 | 3.0689 |
| 0.2          | 0.5          | 0.3          | 1.0893 | 1.0911 | 0.6          | 0.2          | 0.2          | 3.1532 | 3.1717 |
| 0.2          | 0.6          | 0.2          | 1.0752 | 1.0800 | 0.6          | 0.3          | 0.1          | 3.1307 | 3.0856 |
| 0.2          | 0.7          | 0.1          | 1.0358 | 1.0460 | 0.7          | 0.1          | 0.2          | 3.6902 | 3.7087 |
| 0.3          | 0.1          | 0.6          | 1.7433 | 1.6839 | 0.7          | 0.2          | 0.1          | 3.7953 | 3.6354 |
| 0.3          | 0.2          | 0.5          | 1.6505 | 1.6605 | 0.8          | 0.1          | 0.1          | 4.1976 | 4.1821 |
| 0.3          | 0.3          | 0.4          | 1.6624 | 1.6819 | MAX          |              |              | 4.1976 | 4.1821 |
| 0.3          | 0.4          | 0.3          | 1.5716 | 1.6746 | MIN          |              |              | 0.5539 | 0.5329 |

**TABLE 3.2.29** Range of Average Interval Lengths  
for 90% Two-sided Intervals on  $\sigma_P^2$   
when  $I = 12$ ,  $J = 3$ , and  $K = 2$

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.4382 | 0.4434 | 0.3          | 0.5          | 0.2          | 0.6465 | 0.6598 |
| 0.1          | 0.2          | 0.7          | 0.4202 | 0.4170 | 0.3          | 0.6          | 0.1          | 0.6422 | 0.6275 |
| 0.1          | 0.3          | 0.6          | 0.3831 | 0.3736 | 0.4          | 0.1          | 0.5          | 0.9651 | 0.9847 |
| 0.1          | 0.4          | 0.5          | 0.3522 | 0.3619 | 0.4          | 0.2          | 0.4          | 0.9289 | 0.9289 |
| 0.1          | 0.5          | 0.4          | 0.3316 | 0.3303 | 0.4          | 0.3          | 0.3          | 0.9007 | 0.9051 |
| 0.1          | 0.6          | 0.3          | 0.2970 | 0.2946 | 0.4          | 0.4          | 0.2          | 0.8690 | 0.8595 |
| 0.1          | 0.7          | 0.2          | 0.2613 | 0.2645 | 0.4          | 0.5          | 0.1          | 0.8162 | 0.8246 |
| 0.1          | 0.8          | 0.1          | 0.2341 | 0.2332 | 0.5          | 0.1          | 0.4          | 1.1471 | 1.1356 |
| 0.2          | 0.1          | 0.7          | 0.6279 | 0.6383 | 0.5          | 0.2          | 0.3          | 1.1031 | 1.1030 |
| 0.2          | 0.2          | 0.6          | 0.6033 | 0.5918 | 0.5          | 0.3          | 0.2          | 1.0619 | 1.0580 |
| 0.2          | 0.3          | 0.5          | 0.5767 | 0.5650 | 0.5          | 0.4          | 0.1          | 1.0237 | 1.0297 |
| 0.2          | 0.4          | 0.4          | 0.5302 | 0.5315 | 0.6          | 0.1          | 0.3          | 1.3237 | 1.3202 |
| 0.2          | 0.5          | 0.3          | 0.4937 | 0.5057 | 0.6          | 0.2          | 0.2          | 1.2601 | 1.2582 |
| 0.2          | 0.6          | 0.2          | 0.4680 | 0.4634 | 0.6          | 0.3          | 0.1          | 1.2342 | 1.2132 |
| 0.2          | 0.7          | 0.1          | 0.4293 | 0.4347 | 0.7          | 0.1          | 0.2          | 1.4781 | 1.4720 |
| 0.3          | 0.1          | 0.6          | 0.7921 | 0.7976 | 0.7          | 0.2          | 0.1          | 1.4455 | 1.4215 |
| 0.3          | 0.2          | 0.5          | 0.7693 | 0.7435 | 0.8          | 0.1          | 0.1          | 1.6322 | 1.6153 |
| 0.3          | 0.3          | 0.4          | 0.7342 | 0.7370 | MAX          |              |              | 1.6322 | 1.6153 |
| 0.3          | 0.4          | 0.3          | 0.6993 | 0.7007 | MIN          |              |              | 0.2341 | 0.2332 |

**TABLE 3.2.30 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 12$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.3293 | 0.3287 | 0.3          | 0.5          | 0.2          | 0.6280 | 0.6236 |
| 0.1          | 0.2          | 0.7          | 0.3095 | 0.3154 | 0.3          | 0.6          | 0.1          | 0.6148 | 0.6095 |
| 0.1          | 0.3          | 0.6          | 0.2979 | 0.2964 | 0.4          | 0.1          | 0.5          | 0.8790 | 0.8925 |
| 0.1          | 0.4          | 0.5          | 0.2833 | 0.2807 | 0.4          | 0.2          | 0.4          | 0.8558 | 0.8674 |
| 0.1          | 0.5          | 0.4          | 0.2639 | 0.2667 | 0.4          | 0.3          | 0.3          | 0.8567 | 0.8452 |
| 0.1          | 0.6          | 0.3          | 0.2489 | 0.2520 | 0.4          | 0.4          | 0.2          | 0.8259 | 0.8290 |
| 0.1          | 0.7          | 0.2          | 0.2350 | 0.2298 | 0.4          | 0.5          | 0.1          | 0.8018 | 0.8131 |
| 0.1          | 0.8          | 0.1          | 0.2148 | 0.2150 | 0.5          | 0.1          | 0.4          | 1.0665 | 1.0734 |
| 0.2          | 0.1          | 0.7          | 0.5127 | 0.5161 | 0.5          | 0.2          | 0.3          | 1.0581 | 1.0546 |
| 0.2          | 0.2          | 0.6          | 0.5028 | 0.4995 | 0.5          | 0.3          | 0.2          | 1.0375 | 1.0290 |
| 0.2          | 0.3          | 0.5          | 0.4753 | 0.4877 | 0.5          | 0.4          | 0.1          | 1.0121 | 1.0072 |
| 0.2          | 0.4          | 0.4          | 0.4606 | 0.4643 | 0.6          | 0.1          | 0.3          | 1.2315 | 1.2440 |
| 0.2          | 0.5          | 0.3          | 0.4547 | 0.4598 | 0.6          | 0.2          | 0.2          | 1.2309 | 1.2316 |
| 0.2          | 0.6          | 0.2          | 0.4354 | 0.4348 | 0.6          | 0.3          | 0.1          | 1.2190 | 1.2114 |
| 0.2          | 0.7          | 0.1          | 0.4148 | 0.4188 | 0.7          | 0.1          | 0.2          | 1.4114 | 1.4443 |
| 0.3          | 0.1          | 0.6          | 0.7054 | 0.6892 | 0.7          | 0.2          | 0.1          | 1.4095 | 1.4008 |
| 0.3          | 0.2          | 0.5          | 0.6909 | 0.6794 | 0.8          | 0.1          | 0.1          | 1.6047 | 1.5720 |
| 0.3          | 0.3          | 0.4          | 0.6707 | 0.6655 | MAX          |              |              | 1.6047 | 1.5720 |
| 0.3          | 0.4          | 0.3          | 0.6347 | 0.6398 | MIN          |              |              | 0.2148 | 0.2150 |

**TABLE 3.2.31 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 12$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.3248 | 0.3245 | 0.3          | 0.5          | 0.2          | 0.6360 | 0.6222 |
| 0.1          | 0.2          | 0.7          | 0.3110 | 0.3113 | 0.3          | 0.6          | 0.1          | 0.6136 | 0.6233 |
| 0.1          | 0.3          | 0.6          | 0.2972 | 0.2975 | 0.4          | 0.1          | 0.5          | 0.8763 | 0.8710 |
| 0.1          | 0.4          | 0.5          | 0.2744 | 0.2839 | 0.4          | 0.2          | 0.4          | 0.8849 | 0.8488 |
| 0.1          | 0.5          | 0.4          | 0.2601 | 0.2658 | 0.4          | 0.3          | 0.3          | 0.8562 | 0.8491 |
| 0.1          | 0.6          | 0.3          | 0.2507 | 0.2448 | 0.4          | 0.4          | 0.2          | 0.8220 | 0.8251 |
| 0.1          | 0.7          | 0.2          | 0.2314 | 0.2343 | 0.4          | 0.5          | 0.1          | 0.8053 | 0.8124 |
| 0.1          | 0.8          | 0.1          | 0.2109 | 0.2159 | 0.5          | 0.1          | 0.4          | 1.0709 | 1.0670 |
| 0.2          | 0.1          | 0.7          | 0.5068 | 0.5200 | 0.5          | 0.2          | 0.3          | 1.0436 | 1.0403 |
| 0.2          | 0.2          | 0.6          | 0.4917 | 0.4908 | 0.5          | 0.3          | 0.2          | 1.0357 | 1.0344 |
| 0.2          | 0.3          | 0.5          | 0.4770 | 0.4735 | 0.5          | 0.4          | 0.1          | 1.0170 | 1.0024 |
| 0.2          | 0.4          | 0.4          | 0.4678 | 0.4659 | 0.6          | 0.1          | 0.3          | 1.2538 | 1.2596 |
| 0.2          | 0.5          | 0.3          | 0.4483 | 0.4520 | 0.6          | 0.2          | 0.2          | 1.2389 | 1.2171 |
| 0.2          | 0.6          | 0.2          | 0.4299 | 0.4258 | 0.6          | 0.3          | 0.1          | 1.2082 | 1.2040 |
| 0.2          | 0.7          | 0.1          | 0.4113 | 0.4174 | 0.7          | 0.1          | 0.2          | 1.4421 | 1.4005 |
| 0.3          | 0.1          | 0.6          | 0.6939 | 0.6963 | 0.7          | 0.2          | 0.1          | 1.4331 | 1.4412 |
| 0.3          | 0.2          | 0.5          | 0.6742 | 0.6872 | 0.8          | 0.1          | 0.1          | 1.6483 | 1.6099 |
| 0.3          | 0.3          | 0.4          | 0.6518 | 0.6693 | MAX          |              |              | 1.6483 | 1.6099 |
| 0.3          | 0.4          | 0.3          | 0.6466 | 0.6466 | MIN          |              |              | 0.2109 | 0.2159 |

**TABLE 3.2.32 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 12$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.2605 | 0.2635 | 0.3          | 0.5          | 0.2          | 0.6158 | 0.6123 |
| 0.1          | 0.2          | 0.7          | 0.2584 | 0.2552 | 0.3          | 0.6          | 0.1          | 0.6052 | 0.6076 |
| 0.1          | 0.3          | 0.6          | 0.2473 | 0.2454 | 0.4          | 0.1          | 0.5          | 0.8452 | 0.8424 |
| 0.1          | 0.4          | 0.5          | 0.2426 | 0.2388 | 0.4          | 0.2          | 0.4          | 0.8394 | 0.8309 |
| 0.1          | 0.5          | 0.4          | 0.2308 | 0.2323 | 0.4          | 0.3          | 0.3          | 0.8161 | 0.8263 |
| 0.1          | 0.6          | 0.3          | 0.2250 | 0.2182 | 0.4          | 0.4          | 0.2          | 0.8112 | 0.8061 |
| 0.1          | 0.7          | 0.2          | 0.2189 | 0.2177 | 0.4          | 0.5          | 0.1          | 0.7868 | 0.7981 |
| 0.1          | 0.8          | 0.1          | 0.2103 | 0.2070 | 0.5          | 0.1          | 0.4          | 1.0402 | 1.0267 |
| 0.2          | 0.1          | 0.7          | 0.4495 | 0.4552 | 0.5          | 0.2          | 0.3          | 1.0266 | 1.0287 |
| 0.2          | 0.2          | 0.6          | 0.4434 | 0.4510 | 0.5          | 0.3          | 0.2          | 0.9928 | 1.0287 |
| 0.2          | 0.3          | 0.5          | 0.4402 | 0.4442 | 0.5          | 0.4          | 0.1          | 1.0051 | 0.9920 |
| 0.2          | 0.4          | 0.4          | 0.4305 | 0.4295 | 0.6          | 0.1          | 0.3          | 1.1955 | 1.2161 |
| 0.2          | 0.5          | 0.3          | 0.4293 | 0.4261 | 0.6          | 0.2          | 0.2          | 1.2033 | 1.2160 |
| 0.2          | 0.6          | 0.2          | 0.4140 | 0.4171 | 0.6          | 0.3          | 0.1          | 1.2127 | 1.2295 |
| 0.2          | 0.7          | 0.1          | 0.4114 | 0.4039 | 0.7          | 0.1          | 0.2          | 1.4049 | 1.4312 |
| 0.3          | 0.1          | 0.6          | 0.6504 | 0.6397 | 0.7          | 0.2          | 0.1          | 1.3963 | 1.3820 |
| 0.3          | 0.2          | 0.5          | 0.6440 | 0.6376 | 0.8          | 0.1          | 0.1          | 1.5969 | 1.6171 |
| 0.3          | 0.3          | 0.4          | 0.6300 | 0.6248 | MAX          |              |              | 1.5969 | 1.6171 |
| 0.3          | 0.4          | 0.3          | 0.6120 | 0.6163 | MIN          |              |              | 0.2103 | 0.2070 |

**TABLE 3.2.33 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 24$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.2573 | 0.2549 | 0.3          | 0.5          | 0.2          | 0.3769 | 0.3816 |
| 0.1          | 0.2          | 0.7          | 0.2441 | 0.2438 | 0.3          | 0.6          | 0.1          | 0.3632 | 0.3586 |
| 0.1          | 0.3          | 0.6          | 0.2257 | 0.2232 | 0.4          | 0.1          | 0.5          | 0.5499 | 0.5516 |
| 0.1          | 0.4          | 0.5          | 0.2100 | 0.2077 | 0.4          | 0.2          | 0.4          | 0.5266 | 0.5287 |
| 0.1          | 0.5          | 0.4          | 0.1898 | 0.1916 | 0.4          | 0.3          | 0.3          | 0.5128 | 0.5140 |
| 0.1          | 0.6          | 0.3          | 0.1732 | 0.1713 | 0.4          | 0.4          | 0.2          | 0.4915 | 0.4859 |
| 0.1          | 0.7          | 0.2          | 0.1515 | 0.1549 | 0.4          | 0.5          | 0.1          | 0.4676 | 0.4723 |
| 0.1          | 0.8          | 0.1          | 0.1337 | 0.1324 | 0.5          | 0.1          | 0.4          | 0.6509 | 0.6453 |
| 0.2          | 0.1          | 0.7          | 0.3592 | 0.3619 | 0.5          | 0.2          | 0.3          | 0.6280 | 0.6278 |
| 0.2          | 0.2          | 0.6          | 0.3421 | 0.3450 | 0.5          | 0.3          | 0.2          | 0.6024 | 0.5991 |
| 0.2          | 0.3          | 0.5          | 0.3208 | 0.3208 | 0.5          | 0.4          | 0.1          | 0.5889 | 0.5862 |
| 0.2          | 0.4          | 0.4          | 0.3066 | 0.3065 | 0.6          | 0.1          | 0.3          | 0.7437 | 0.7283 |
| 0.2          | 0.5          | 0.3          | 0.2848 | 0.2895 | 0.6          | 0.2          | 0.2          | 0.7192 | 0.7176 |
| 0.2          | 0.6          | 0.2          | 0.2630 | 0.2644 | 0.6          | 0.3          | 0.1          | 0.6997 | 0.6996 |
| 0.2          | 0.7          | 0.1          | 0.2472 | 0.2458 | 0.7          | 0.1          | 0.2          | 0.8452 | 0.8361 |
| 0.3          | 0.1          | 0.6          | 0.4520 | 0.4533 | 0.7          | 0.2          | 0.1          | 0.8084 | 0.8150 |
| 0.3          | 0.2          | 0.5          | 0.4358 | 0.4387 | 0.8          | 0.1          | 0.1          | 0.9246 | 0.9261 |
| 0.3          | 0.3          | 0.4          | 0.4204 | 0.4200 | MAX          |              |              | 0.9246 | 0.9261 |
| 0.3          | 0.4          | 0.3          | 0.3981 | 0.3963 | MIN          |              |              | 0.1337 | 0.1324 |

**TABLE 3.2.34 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 24$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.1901 | 0.1905 | 0.3          | 0.5          | 0.2          | 0.3578 | 0.3559 |
| 0.1          | 0.2          | 0.7          | 0.1803 | 0.1818 | 0.3          | 0.6          | 0.1          | 0.3499 | 0.3560 |
| 0.1          | 0.3          | 0.6          | 0.1707 | 0.1707 | 0.4          | 0.1          | 0.5          | 0.5006 | 0.5032 |
| 0.1          | 0.4          | 0.5          | 0.1596 | 0.1633 | 0.4          | 0.2          | 0.4          | 0.4969 | 0.4898 |
| 0.1          | 0.5          | 0.4          | 0.1522 | 0.1536 | 0.4          | 0.3          | 0.3          | 0.4832 | 0.4834 |
| 0.1          | 0.6          | 0.3          | 0.1411 | 0.1435 | 0.4          | 0.4          | 0.2          | 0.4706 | 0.4781 |
| 0.1          | 0.7          | 0.2          | 0.1316 | 0.1324 | 0.4          | 0.5          | 0.1          | 0.4651 | 0.4644 |
| 0.1          | 0.8          | 0.1          | 0.1232 | 0.1225 | 0.5          | 0.1          | 0.4          | 0.6064 | 0.6020 |
| 0.2          | 0.1          | 0.7          | 0.2940 | 0.2946 | 0.5          | 0.2          | 0.3          | 0.5978 | 0.5980 |
| 0.2          | 0.2          | 0.6          | 0.2829 | 0.2858 | 0.5          | 0.3          | 0.2          | 0.5920 | 0.5755 |
| 0.2          | 0.3          | 0.5          | 0.2752 | 0.2737 | 0.5          | 0.4          | 0.1          | 0.5738 | 0.5778 |
| 0.2          | 0.4          | 0.4          | 0.2634 | 0.2660 | 0.6          | 0.1          | 0.3          | 0.7047 | 0.7095 |
| 0.2          | 0.5          | 0.3          | 0.2569 | 0.2540 | 0.6          | 0.2          | 0.2          | 0.7041 | 0.7059 |
| 0.2          | 0.6          | 0.2          | 0.2411 | 0.2469 | 0.6          | 0.3          | 0.1          | 0.6895 | 0.6912 |
| 0.2          | 0.7          | 0.1          | 0.2352 | 0.2398 | 0.7          | 0.1          | 0.2          | 0.8116 | 0.8194 |
| 0.3          | 0.1          | 0.6          | 0.3906 | 0.4007 | 0.7          | 0.2          | 0.1          | 0.8004 | 0.8101 |
| 0.3          | 0.2          | 0.5          | 0.3859 | 0.3894 | 0.8          | 0.1          | 0.1          | 0.9224 | 0.9135 |
| 0.3          | 0.3          | 0.4          | 0.3772 | 0.3816 | MAX          |              |              | 0.9224 | 0.9135 |
| 0.3          | 0.4          | 0.3          | 0.3711 | 0.3652 | MIN          |              |              | 0.1232 | 0.1225 |



**TABLE 3.2.35 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 24$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.1896 | 0.1898 | 0.3          | 0.5          | 0.2          | 0.3598 | 0.3617 |
| 0.1          | 0.2          | 0.7          | 0.1793 | 0.1818 | 0.3          | 0.6          | 0.1          | 0.3517 | 0.3497 |
| 0.1          | 0.3          | 0.6          | 0.1680 | 0.1713 | 0.4          | 0.1          | 0.5          | 0.5064 | 0.5005 |
| 0.1          | 0.4          | 0.5          | 0.1624 | 0.1603 | 0.4          | 0.2          | 0.4          | 0.4918 | 0.4981 |
| 0.1          | 0.5          | 0.4          | 0.1508 | 0.1522 | 0.4          | 0.3          | 0.3          | 0.4855 | 0.4833 |
| 0.1          | 0.6          | 0.3          | 0.1393 | 0.1418 | 0.4          | 0.4          | 0.2          | 0.4673 | 0.4744 |
| 0.1          | 0.7          | 0.2          | 0.1313 | 0.1324 | 0.4          | 0.5          | 0.1          | 0.4584 | 0.4643 |
| 0.1          | 0.8          | 0.1          | 0.1224 | 0.1249 | 0.5          | 0.1          | 0.4          | 0.6106 | 0.6012 |
| 0.2          | 0.1          | 0.7          | 0.2977 | 0.2964 | 0.5          | 0.2          | 0.3          | 0.5957 | 0.5901 |
| 0.2          | 0.2          | 0.6          | 0.2819 | 0.2810 | 0.5          | 0.3          | 0.2          | 0.5901 | 0.5830 |
| 0.2          | 0.3          | 0.5          | 0.2747 | 0.2751 | 0.5          | 0.4          | 0.1          | 0.5800 | 0.5808 |
| 0.2          | 0.4          | 0.4          | 0.2665 | 0.2652 | 0.6          | 0.1          | 0.3          | 0.7104 | 0.7125 |
| 0.2          | 0.5          | 0.3          | 0.2534 | 0.2571 | 0.6          | 0.2          | 0.2          | 0.7045 | 0.6836 |
| 0.2          | 0.6          | 0.2          | 0.2467 | 0.2454 | 0.6          | 0.3          | 0.1          | 0.6855 | 0.6794 |
| 0.2          | 0.7          | 0.1          | 0.2382 | 0.2379 | 0.7          | 0.1          | 0.2          | 0.8183 | 0.8114 |
| 0.3          | 0.1          | 0.6          | 0.3944 | 0.3991 | 0.7          | 0.2          | 0.1          | 0.8055 | 0.8010 |
| 0.3          | 0.2          | 0.5          | 0.3900 | 0.3844 | 0.8          | 0.1          | 0.1          | 0.9131 | 0.9106 |
| 0.3          | 0.3          | 0.4          | 0.3745 | 0.3800 | MAX          |              |              | 0.9131 | 0.9106 |
| 0.3          | 0.4          | 0.3          | 0.3675 | 0.3720 | MIN          |              |              | 0.1224 | 0.1249 |

**TABLE 3.2.36 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_P^2$**   
**when  $I = 24$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.1518 | 0.1504 | 0.3          | 0.5          | 0.2          | 0.3500 | 0.3474 |
| 0.1          | 0.2          | 0.7          | 0.1469 | 0.1461 | 0.3          | 0.6          | 0.1          | 0.3422 | 0.3471 |
| 0.1          | 0.3          | 0.6          | 0.1410 | 0.1420 | 0.4          | 0.1          | 0.5          | 0.4760 | 0.4741 |
| 0.1          | 0.4          | 0.5          | 0.1365 | 0.1370 | 0.4          | 0.2          | 0.4          | 0.4760 | 0.4733 |
| 0.1          | 0.5          | 0.4          | 0.1326 | 0.1326 | 0.4          | 0.3          | 0.3          | 0.4709 | 0.4665 |
| 0.1          | 0.6          | 0.3          | 0.1262 | 0.1295 | 0.4          | 0.4          | 0.2          | 0.4638 | 0.4633 |
| 0.1          | 0.7          | 0.2          | 0.1231 | 0.1217 | 0.4          | 0.5          | 0.1          | 0.4579 | 0.4571 |
| 0.1          | 0.8          | 0.1          | 0.1180 | 0.1157 | 0.5          | 0.1          | 0.4          | 0.5828 | 0.5875 |
| 0.2          | 0.1          | 0.7          | 0.2590 | 0.2589 | 0.5          | 0.2          | 0.3          | 0.5824 | 0.5818 |
| 0.2          | 0.2          | 0.6          | 0.2567 | 0.2545 | 0.5          | 0.3          | 0.2          | 0.5730 | 0.5698 |
| 0.2          | 0.3          | 0.5          | 0.2534 | 0.2500 | 0.5          | 0.4          | 0.1          | 0.5711 | 0.5683 |
| 0.2          | 0.4          | 0.4          | 0.2483 | 0.2449 | 0.6          | 0.1          | 0.3          | 0.7023 | 0.6885 |
| 0.2          | 0.5          | 0.3          | 0.2449 | 0.2441 | 0.6          | 0.2          | 0.2          | 0.6893 | 0.6867 |
| 0.2          | 0.6          | 0.2          | 0.2363 | 0.2357 | 0.6          | 0.3          | 0.1          | 0.6855 | 0.6840 |
| 0.2          | 0.7          | 0.1          | 0.2314 | 0.2307 | 0.7          | 0.1          | 0.2          | 0.8007 | 0.8087 |
| 0.3          | 0.1          | 0.6          | 0.3698 | 0.3695 | 0.7          | 0.2          | 0.1          | 0.8007 | 0.7879 |
| 0.3          | 0.2          | 0.5          | 0.3586 | 0.3617 | 0.8          | 0.1          | 0.1          | 0.9117 | 0.9074 |
| 0.3          | 0.3          | 0.4          | 0.3632 | 0.3590 | MAX          |              |              | 0.9117 | 0.9074 |
| 0.3          | 0.4          | 0.3          | 0.3526 | 0.3541 | MIN          |              |              | 0.1180 | 0.1157 |

**TABLE 3.2.37 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 6$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      |
|--------------|--------------|--------------|----------|----------|--------------|--------------|--------------|----------|----------|
| 0.1          | 0.1          | 0.8          | 41.2280  | 39.9970  | 0.3          | 0.5          | 0.2          | 128.6260 | 133.6180 |
| 0.1          | 0.2          | 0.7          | 66.7740  | 64.4340  | 0.3          | 0.6          | 0.1          | 160.3300 | 166.4220 |
| 0.1          | 0.3          | 0.6          | 84.7690  | 89.1080  | 0.4          | 0.1          | 0.5          | 35.0400  | 36.2870  |
| 0.1          | 0.4          | 0.5          | 118.6260 | 112.5690 | 0.4          | 0.2          | 0.4          | 56.2780  | 60.5430  |
| 0.1          | 0.5          | 0.4          | 138.6160 | 138.7830 | 0.4          | 0.3          | 0.3          | 84.4010  | 81.8600  |
| 0.1          | 0.6          | 0.3          | 155.6330 | 161.2230 | 0.4          | 0.4          | 0.2          | 104.0160 | 107.6760 |
| 0.1          | 0.7          | 0.2          | 175.0060 | 173.9400 | 0.4          | 0.5          | 0.1          | 124.7860 | 125.1090 |
| 0.1          | 0.8          | 0.1          | 206.3010 | 199.6560 | 0.5          | 0.1          | 0.4          | 34.8120  | 34.5300  |
| 0.2          | 0.1          | 0.7          | 39.8220  | 42.1850  | 0.5          | 0.2          | 0.3          | 54.6980  | 58.0090  |
| 0.2          | 0.2          | 0.6          | 64.6690  | 61.2710  | 0.5          | 0.3          | 0.2          | 81.5130  | 80.2250  |
| 0.2          | 0.3          | 0.5          | 86.6470  | 87.5220  | 0.5          | 0.4          | 0.1          | 100.0820 | 108.1530 |
| 0.2          | 0.4          | 0.4          | 109.6170 | 112.6760 | 0.6          | 0.1          | 0.3          | 31.5960  | 29.5770  |
| 0.2          | 0.5          | 0.3          | 129.9920 | 144.2040 | 0.6          | 0.2          | 0.2          | 58.9650  | 56.8200  |
| 0.2          | 0.6          | 0.2          | 159.8200 | 175.6120 | 0.6          | 0.3          | 0.1          | 77.4030  | 79.3600  |
| 0.2          | 0.7          | 0.1          | 178.1340 | 172.2840 | 0.7          | 0.1          | 0.2          | 29.0740  | 27.9340  |
| 0.3          | 0.1          | 0.6          | 39.4330  | 38.5810  | 0.7          | 0.2          | 0.1          | 52.4770  | 52.1490  |
| 0.3          | 0.2          | 0.5          | 63.2580  | 58.7850  | 0.8          | 0.1          | 0.1          | 26.9850  | 25.8890  |
| 0.3          | 0.3          | 0.4          | 87.0310  | 85.6460  | MAX          |              |              | 206.3010 | 199.6560 |
| 0.3          | 0.4          | 0.3          | 108.3340 | 109.2060 | MIN          |              |              | 26.9850  | 25.8890  |

**TABLE 3.2.38 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 6$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      |
|--------------|--------------|--------------|----------|----------|--------------|--------------|--------------|----------|----------|
| 0.1          | 0.1          | 0.8          | 34.9660  | 34.1150  | 0.3          | 0.5          | 0.2          | 128.7660 | 124.3280 |
| 0.1          | 0.2          | 0.7          | 61.4870  | 58.3610  | 0.3          | 0.6          | 0.1          | 157.3990 | 154.1850 |
| 0.1          | 0.3          | 0.6          | 82.6490  | 82.9950  | 0.4          | 0.1          | 0.5          | 31.9690  | 30.3390  |
| 0.1          | 0.4          | 0.5          | 111.0430 | 105.0830 | 0.4          | 0.2          | 0.4          | 56.1160  | 55.3820  |
| 0.1          | 0.5          | 0.4          | 137.3810 | 133.8720 | 0.4          | 0.3          | 0.3          | 83.1180  | 80.9270  |
| 0.1          | 0.6          | 0.3          | 156.9460 | 158.7980 | 0.4          | 0.4          | 0.2          | 102.1030 | 104.1390 |
| 0.1          | 0.7          | 0.2          | 183.3230 | 184.5570 | 0.4          | 0.5          | 0.1          | 128.3220 | 128.1520 |
| 0.1          | 0.8          | 0.1          | 190.2220 | 205.0110 | 0.5          | 0.1          | 0.4          | 29.8150  | 30.7960  |
| 0.2          | 0.1          | 0.7          | 33.9000  | 32.1030  | 0.5          | 0.2          | 0.3          | 56.2670  | 56.1730  |
| 0.2          | 0.2          | 0.6          | 59.0870  | 56.6090  | 0.5          | 0.3          | 0.2          | 80.4930  | 78.2860  |
| 0.2          | 0.3          | 0.5          | 79.2270  | 80.5710  | 0.5          | 0.4          | 0.1          | 96.5560  | 108.3320 |
| 0.2          | 0.4          | 0.4          | 99.8950  | 106.7420 | 0.6          | 0.1          | 0.3          | 28.1470  | 27.4130  |
| 0.2          | 0.5          | 0.3          | 126.6320 | 131.0580 | 0.6          | 0.2          | 0.2          | 51.1990  | 56.1010  |
| 0.2          | 0.6          | 0.2          | 149.0080 | 152.7570 | 0.6          | 0.3          | 0.1          | 77.6700  | 77.9640  |
| 0.2          | 0.7          | 0.1          | 181.0060 | 181.8180 | 0.7          | 0.1          | 0.2          | 26.6460  | 28.3690  |
| 0.3          | 0.1          | 0.6          | 31.5170  | 30.4120  | 0.7          | 0.2          | 0.1          | 48.2520  | 51.4130  |
| 0.3          | 0.2          | 0.5          | 54.6210  | 52.5150  | 0.8          | 0.1          | 0.1          | 25.3970  | 26.1900  |
| 0.3          | 0.3          | 0.4          | 80.5730  | 82.4390  | MAX          |              |              | 190.2220 | 205.0110 |
| 0.3          | 0.4          | 0.3          | 103.7140 | 107.9850 | MIN          |              |              | 25.3970  | 26.1900  |

**TABLE 3.2.39 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 6$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.8802 | 0.8496 | 0.3          | 0.5          | 0.2          | 2.7586 | 2.6532 |
| 0.1          | 0.2          | 0.7          | 1.3039 | 1.3295 | 0.3          | 0.6          | 0.1          | 3.2640 | 3.1628 |
| 0.1          | 0.3          | 0.6          | 1.8046 | 1.8823 | 0.4          | 0.1          | 0.5          | 0.7252 | 0.7344 |
| 0.1          | 0.4          | 0.5          | 2.2831 | 2.3246 | 0.4          | 0.2          | 0.4          | 1.2052 | 1.2277 |
| 0.1          | 0.5          | 0.4          | 2.7097 | 2.8030 | 0.4          | 0.3          | 0.3          | 1.7190 | 1.6729 |
| 0.1          | 0.6          | 0.3          | 3.1840 | 3.2328 | 0.4          | 0.4          | 0.2          | 2.1499 | 2.1697 |
| 0.1          | 0.7          | 0.2          | 3.8538 | 3.7468 | 0.4          | 0.5          | 0.1          | 2.6532 | 2.6220 |
| 0.1          | 0.8          | 0.1          | 4.2047 | 4.2895 | 0.5          | 0.1          | 0.4          | 0.6933 | 0.7029 |
| 0.2          | 0.1          | 0.7          | 0.8337 | 0.8072 | 0.5          | 0.2          | 0.3          | 1.1735 | 1.1775 |
| 0.2          | 0.2          | 0.6          | 1.2829 | 1.3029 | 0.5          | 0.3          | 0.2          | 1.6598 | 1.6898 |
| 0.2          | 0.3          | 0.5          | 1.7607 | 1.7249 | 0.5          | 0.4          | 0.1          | 2.1970 | 2.0730 |
| 0.2          | 0.4          | 0.4          | 2.2660 | 2.2629 | 0.6          | 0.1          | 0.3          | 0.6486 | 0.6517 |
| 0.2          | 0.5          | 0.3          | 2.6810 | 2.7209 | 0.6          | 0.2          | 0.2          | 1.1241 | 1.0951 |
| 0.2          | 0.6          | 0.2          | 3.1897 | 3.2032 | 0.6          | 0.3          | 0.1          | 1.5885 | 1.5944 |
| 0.2          | 0.7          | 0.1          | 3.6999 | 3.6668 | 0.7          | 0.1          | 0.2          | 0.6122 | 0.5902 |
| 0.3          | 0.1          | 0.6          | 0.7683 | 0.7628 | 0.7          | 0.2          | 0.1          | 1.0755 | 1.1022 |
| 0.3          | 0.2          | 0.5          | 1.2476 | 1.2453 | 0.8          | 0.1          | 0.1          | 0.5826 | 0.5604 |
| 0.3          | 0.3          | 0.4          | 1.6864 | 1.7232 | MAX          |              |              | 4.2047 | 4.2895 |
| 0.3          | 0.4          | 0.3          | 2.2280 | 2.2085 | MIN          |              |              | 0.5826 | 0.5604 |

**TABLE 3.2.40 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 6$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.6912 | 0.6968 | 0.3          | 0.5          | 0.2          | 2.6518 | 2.6503 |
| 0.1          | 0.2          | 0.7          | 1.1958 | 1.2137 | 0.3          | 0.6          | 0.1          | 3.1121 | 3.1406 |
| 0.1          | 0.3          | 0.6          | 1.6794 | 1.6995 | 0.4          | 0.1          | 0.5          | 0.6163 | 0.6271 |
| 0.1          | 0.4          | 0.5          | 2.1703 | 2.1986 | 0.4          | 0.2          | 0.4          | 1.1347 | 1.1003 |
| 0.1          | 0.5          | 0.4          | 2.7144 | 2.6531 | 0.4          | 0.3          | 0.3          | 1.6010 | 1.6362 |
| 0.1          | 0.6          | 0.3          | 3.2157 | 3.1804 | 0.4          | 0.4          | 0.2          | 2.1057 | 2.1140 |
| 0.1          | 0.7          | 0.2          | 3.5585 | 3.7412 | 0.4          | 0.5          | 0.1          | 2.5862 | 2.5754 |
| 0.1          | 0.8          | 0.1          | 4.1661 | 4.2859 | 0.5          | 0.1          | 0.4          | 0.5888 | 0.6199 |
| 0.2          | 0.1          | 0.7          | 0.6831 | 0.6654 | 0.5          | 0.2          | 0.3          | 1.1027 | 1.1020 |
| 0.2          | 0.2          | 0.6          | 1.1782 | 1.1966 | 0.5          | 0.3          | 0.2          | 1.5560 | 1.6127 |
| 0.2          | 0.3          | 0.5          | 1.6276 | 1.7187 | 0.5          | 0.4          | 0.1          | 2.0594 | 2.1038 |
| 0.2          | 0.4          | 0.4          | 2.1932 | 2.1579 | 0.6          | 0.1          | 0.3          | 0.5916 | 0.5796 |
| 0.2          | 0.5          | 0.3          | 2.7086 | 2.6640 | 0.6          | 0.2          | 0.2          | 1.0926 | 1.1068 |
| 0.2          | 0.6          | 0.2          | 3.1815 | 3.1943 | 0.6          | 0.3          | 0.1          | 1.6288 | 1.5678 |
| 0.2          | 0.7          | 0.1          | 3.5845 | 3.6426 | 0.7          | 0.1          | 0.2          | 0.5778 | 0.5540 |
| 0.3          | 0.1          | 0.6          | 0.6441 | 0.6501 | 0.7          | 0.2          | 0.1          | 1.0818 | 1.0655 |
| 0.3          | 0.2          | 0.5          | 1.1612 | 1.1510 | 0.8          | 0.1          | 0.1          | 0.5574 | 0.5398 |
| 0.3          | 0.3          | 0.4          | 1.6360 | 1.6926 | MAX          |              |              | 4.1661 | 4.2859 |
| 0.3          | 0.4          | 0.3          | 2.0746 | 2.1283 | MIN          |              |              | 0.5574 | 0.5398 |

**TABLE 3.2.41 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 12$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      |
|--------------|--------------|--------------|----------|----------|--------------|--------------|--------------|----------|----------|
| 0.1          | 0.1          | 0.8          | 34.2360  | 34.6380  | 0.3          | 0.5          | 0.2          | 128.7850 | 129.3130 |
| 0.1          | 0.2          | 0.7          | 57.6980  | 58.2530  | 0.3          | 0.6          | 0.1          | 157.9580 | 152.1130 |
| 0.1          | 0.3          | 0.6          | 83.5680  | 81.0600  | 0.4          | 0.1          | 0.5          | 33.0630  | 29.0530  |
| 0.1          | 0.4          | 0.5          | 111.9440 | 102.0030 | 0.4          | 0.2          | 0.4          | 56.1230  | 57.8670  |
| 0.1          | 0.5          | 0.4          | 128.0870 | 130.3090 | 0.4          | 0.3          | 0.3          | 78.9920  | 79.4960  |
| 0.1          | 0.6          | 0.3          | 151.8230 | 157.8610 | 0.4          | 0.4          | 0.2          | 103.5410 | 99.2340  |
| 0.1          | 0.7          | 0.2          | 174.5010 | 181.8950 | 0.4          | 0.5          | 0.1          | 125.8790 | 134.9990 |
| 0.1          | 0.8          | 0.1          | 207.3970 | 211.8480 | 0.5          | 0.1          | 0.4          | 31.0470  | 28.2320  |
| 0.2          | 0.1          | 0.7          | 32.5940  | 33.1180  | 0.5          | 0.2          | 0.3          | 51.9080  | 56.6400  |
| 0.2          | 0.2          | 0.6          | 58.8100  | 59.0010  | 0.5          | 0.3          | 0.2          | 76.9310  | 74.8750  |
| 0.2          | 0.3          | 0.5          | 80.6940  | 81.8940  | 0.5          | 0.4          | 0.1          | 104.0590 | 98.2220  |
| 0.2          | 0.4          | 0.4          | 108.9360 | 106.5810 | 0.6          | 0.1          | 0.3          | 27.4060  | 27.4840  |
| 0.2          | 0.5          | 0.3          | 126.3520 | 123.8040 | 0.6          | 0.2          | 0.2          | 51.7690  | 56.0890  |
| 0.2          | 0.6          | 0.2          | 156.5070 | 153.0520 | 0.6          | 0.3          | 0.1          | 77.3460  | 75.0640  |
| 0.2          | 0.7          | 0.1          | 180.9660 | 179.8620 | 0.7          | 0.1          | 0.2          | 28.8710  | 25.7870  |
| 0.3          | 0.1          | 0.6          | 32.5660  | 31.7720  | 0.7          | 0.2          | 0.1          | 51.5540  | 50.7930  |
| 0.3          | 0.2          | 0.5          | 58.2670  | 56.7880  | 0.8          | 0.1          | 0.1          | 26.2830  | 24.9890  |
| 0.3          | 0.3          | 0.4          | 81.8020  | 81.9000  | MAX          |              |              | 207.3970 | 211.8480 |
| 0.3          | 0.4          | 0.3          | 104.2830 | 103.8270 | MIN          |              |              | 26.2830  | 24.9890  |

**TABLE 3.2.42 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 12$ ,  $J = 3$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      |
|--------------|--------------|--------------|----------|----------|--------------|--------------|--------------|----------|----------|
| 0.1          | 0.1          | 0.8          | 29.5520  | 29.7570  | 0.3          | 0.5          | 0.2          | 139.3480 | 130.4570 |
| 0.1          | 0.2          | 0.7          | 53.1010  | 57.8540  | 0.3          | 0.6          | 0.1          | 145.1240 | 148.0940 |
| 0.1          | 0.3          | 0.6          | 79.3340  | 76.0030  | 0.4          | 0.1          | 0.5          | 28.6110  | 26.9420  |
| 0.1          | 0.4          | 0.5          | 102.5410 | 106.9470 | 0.4          | 0.2          | 0.4          | 53.9970  | 52.7470  |
| 0.1          | 0.5          | 0.4          | 135.1940 | 126.8820 | 0.4          | 0.3          | 0.3          | 79.7700  | 78.8660  |
| 0.1          | 0.6          | 0.3          | 156.9340 | 159.6790 | 0.4          | 0.4          | 0.2          | 99.4980  | 102.3800 |
| 0.1          | 0.7          | 0.2          | 178.0260 | 191.2700 | 0.4          | 0.5          | 0.1          | 127.6320 | 126.5050 |
| 0.1          | 0.8          | 0.1          | 197.8040 | 203.7820 | 0.5          | 0.1          | 0.4          | 27.9790  | 26.8280  |
| 0.2          | 0.1          | 0.7          | 28.2740  | 30.0160  | 0.5          | 0.2          | 0.3          | 53.0480  | 51.4480  |
| 0.2          | 0.2          | 0.6          | 52.0030  | 55.1680  | 0.5          | 0.3          | 0.2          | 76.7250  | 77.7970  |
| 0.2          | 0.3          | 0.5          | 77.5070  | 77.4770  | 0.5          | 0.4          | 0.1          | 98.9830  | 96.0550  |
| 0.2          | 0.4          | 0.4          | 106.1150 | 97.6990  | 0.6          | 0.1          | 0.3          | 26.6620  | 26.1740  |
| 0.2          | 0.5          | 0.3          | 127.8760 | 132.9160 | 0.6          | 0.2          | 0.2          | 50.2850  | 53.4620  |
| 0.2          | 0.6          | 0.2          | 146.9840 | 150.3130 | 0.6          | 0.3          | 0.1          | 78.2460  | 75.2920  |
| 0.2          | 0.7          | 0.1          | 170.1280 | 181.4810 | 0.7          | 0.1          | 0.2          | 25.6230  | 26.3460  |
| 0.3          | 0.1          | 0.6          | 27.8920  | 28.3180  | 0.7          | 0.2          | 0.1          | 51.8640  | 53.4990  |
| 0.3          | 0.2          | 0.5          | 52.8650  | 54.3430  | 0.8          | 0.1          | 0.1          | 26.0170  | 25.7650  |
| 0.3          | 0.3          | 0.4          | 76.9570  | 78.5890  | MAX          |              |              | 197.8040 | 203.7820 |
| 0.3          | 0.4          | 0.3          | 102.4960 | 105.0220 | MIN          |              |              | 25.6230  | 25.7650  |



**TABLE 3.2.43 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 12$ ,  $J = 6$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.6971 | 0.6895 | 0.3          | 0.5          | 0.2          | 2.6554 | 2.6170 |
| 0.1          | 0.2          | 0.7          | 1.1915 | 1.1863 | 0.3          | 0.6          | 0.1          | 3.1686 | 3.1372 |
| 0.1          | 0.3          | 0.6          | 1.6620 | 1.7220 | 0.4          | 0.1          | 0.5          | 0.6253 | 0.6349 |
| 0.1          | 0.4          | 0.5          | 2.1783 | 2.2143 | 0.4          | 0.2          | 0.4          | 1.1412 | 1.1442 |
| 0.1          | 0.5          | 0.4          | 2.6066 | 2.6390 | 0.4          | 0.3          | 0.3          | 1.6307 | 1.6405 |
| 0.1          | 0.6          | 0.3          | 3.1918 | 3.2009 | 0.4          | 0.4          | 0.2          | 2.1313 | 2.1109 |
| 0.1          | 0.7          | 0.2          | 3.5913 | 3.7158 | 0.4          | 0.5          | 0.1          | 2.6183 | 2.5723 |
| 0.1          | 0.8          | 0.1          | 4.1242 | 4.2819 | 0.5          | 0.1          | 0.4          | 0.6037 | 0.6039 |
| 0.2          | 0.1          | 0.7          | 0.6773 | 0.6729 | 0.5          | 0.2          | 0.3          | 1.1116 | 1.1070 |
| 0.2          | 0.2          | 0.6          | 1.1897 | 1.1577 | 0.5          | 0.3          | 0.2          | 1.5919 | 1.6073 |
| 0.2          | 0.3          | 0.5          | 1.6679 | 1.6712 | 0.5          | 0.4          | 0.1          | 2.1348 | 2.0885 |
| 0.2          | 0.4          | 0.4          | 2.1859 | 2.1870 | 0.6          | 0.1          | 0.3          | 0.5832 | 0.5762 |
| 0.2          | 0.5          | 0.3          | 2.6830 | 2.6749 | 0.6          | 0.2          | 0.2          | 1.0764 | 1.0940 |
| 0.2          | 0.6          | 0.2          | 3.0723 | 3.1910 | 0.6          | 0.3          | 0.1          | 1.5967 | 1.6170 |
| 0.2          | 0.7          | 0.1          | 3.5987 | 3.6025 | 0.7          | 0.1          | 0.2          | 0.5636 | 0.5601 |
| 0.3          | 0.1          | 0.6          | 0.6379 | 0.6738 | 0.7          | 0.2          | 0.1          | 1.0784 | 1.0433 |
| 0.3          | 0.2          | 0.5          | 1.1530 | 1.1579 | 0.8          | 0.1          | 0.1          | 0.5403 | 0.5517 |
| 0.3          | 0.3          | 0.4          | 1.6816 | 1.6852 | MAX          |              |              | 4.1242 | 4.2819 |
| 0.3          | 0.4          | 0.3          | 2.1269 | 2.1440 | MIN          |              |              | 0.5403 | 0.5517 |

**TABLE 3.2.44 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 12$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.5996 | 0.6150 | 0.3          | 0.5          | 0.2          | 2.6491 | 2.6087 |
| 0.1          | 0.2          | 0.7          | 1.0942 | 1.1161 | 0.3          | 0.6          | 0.1          | 3.0902 | 3.1345 |
| 0.1          | 0.3          | 0.6          | 1.6222 | 1.6620 | 0.4          | 0.1          | 0.5          | 0.5782 | 0.5733 |
| 0.1          | 0.4          | 0.5          | 2.1383 | 2.1092 | 0.4          | 0.2          | 0.4          | 1.0971 | 1.0932 |
| 0.1          | 0.5          | 0.4          | 2.5889 | 2.6310 | 0.4          | 0.3          | 0.3          | 1.5684 | 1.6301 |
| 0.1          | 0.6          | 0.3          | 3.1887 | 3.1113 | 0.4          | 0.4          | 0.2          | 2.0939 | 2.0955 |
| 0.1          | 0.7          | 0.2          | 3.5777 | 3.5740 | 0.4          | 0.5          | 0.1          | 2.5857 | 2.6041 |
| 0.1          | 0.8          | 0.1          | 4.1022 | 4.0877 | 0.5          | 0.1          | 0.4          | 0.5625 | 0.5772 |
| 0.2          | 0.1          | 0.7          | 0.5989 | 0.6047 | 0.5          | 0.2          | 0.3          | 1.0819 | 1.1155 |
| 0.2          | 0.2          | 0.6          | 1.1216 | 1.1243 | 0.5          | 0.3          | 0.2          | 1.6372 | 1.6048 |
| 0.2          | 0.3          | 0.5          | 1.6409 | 1.6360 | 0.5          | 0.4          | 0.1          | 2.0774 | 2.1342 |
| 0.2          | 0.4          | 0.4          | 2.1032 | 2.1265 | 0.6          | 0.1          | 0.3          | 0.5412 | 0.5653 |
| 0.2          | 0.5          | 0.3          | 2.6589 | 2.6416 | 0.6          | 0.2          | 0.2          | 1.0562 | 1.0817 |
| 0.2          | 0.6          | 0.2          | 3.1740 | 3.1414 | 0.6          | 0.3          | 0.1          | 1.5593 | 1.5667 |
| 0.2          | 0.7          | 0.1          | 3.6724 | 3.6737 | 0.7          | 0.1          | 0.2          | 0.5500 | 0.5448 |
| 0.3          | 0.1          | 0.6          | 0.5755 | 0.5880 | 0.7          | 0.2          | 0.1          | 1.0966 | 1.0558 |
| 0.3          | 0.2          | 0.5          | 1.0959 | 1.1118 | 0.8          | 0.1          | 0.1          | 0.5352 | 0.5277 |
| 0.3          | 0.3          | 0.4          | 1.6297 | 1.5976 | MAX          |              |              | 4.1022 | 4.0877 |
| 0.3          | 0.4          | 0.3          | 2.1644 | 2.0909 | MIN          |              |              | 0.5352 | 0.5277 |

**TABLE 3.2.45 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 24$ ,  $J = 3$ , and  $K = 2$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      |
|--------------|--------------|--------------|----------|----------|--------------|--------------|--------------|----------|----------|
| 0.1          | 0.1          | 0.8          | 27.4860  | 28.6610  | 0.3          | 0.5          | 0.2          | 133.5450 | 126.3010 |
| 0.1          | 0.2          | 0.7          | 53.4370  | 51.4770  | 0.3          | 0.6          | 0.1          | 160.3030 | 149.6080 |
| 0.1          | 0.3          | 0.6          | 75.2240  | 77.1490  | 0.4          | 0.1          | 0.5          | 27.8870  | 29.7940  |
| 0.1          | 0.4          | 0.5          | 105.6260 | 109.9170 | 0.4          | 0.2          | 0.4          | 54.9520  | 50.4320  |
| 0.1          | 0.5          | 0.4          | 131.0810 | 132.3230 | 0.4          | 0.3          | 0.3          | 74.1450  | 76.0780  |
| 0.1          | 0.6          | 0.3          | 164.1510 | 148.4710 | 0.4          | 0.4          | 0.2          | 103.3260 | 102.8240 |
| 0.1          | 0.7          | 0.2          | 172.6020 | 181.5040 | 0.4          | 0.5          | 0.1          | 132.0460 | 129.3730 |
| 0.1          | 0.8          | 0.1          | 205.1960 | 211.2450 | 0.5          | 0.1          | 0.4          | 28.2570  | 28.5490  |
| 0.2          | 0.1          | 0.7          | 28.8070  | 30.3300  | 0.5          | 0.2          | 0.3          | 52.5110  | 55.6220  |
| 0.2          | 0.2          | 0.6          | 53.6660  | 55.6890  | 0.5          | 0.3          | 0.2          | 80.7900  | 77.0920  |
| 0.2          | 0.3          | 0.5          | 78.8980  | 84.8860  | 0.5          | 0.4          | 0.1          | 105.9270 | 100.3460 |
| 0.2          | 0.4          | 0.4          | 100.8070 | 103.4990 | 0.6          | 0.1          | 0.3          | 25.4230  | 25.9830  |
| 0.2          | 0.5          | 0.3          | 134.9150 | 130.6110 | 0.6          | 0.2          | 0.2          | 49.2190  | 51.6510  |
| 0.2          | 0.6          | 0.2          | 159.4260 | 147.3140 | 0.6          | 0.3          | 0.1          | 78.7470  | 76.5410  |
| 0.2          | 0.7          | 0.1          | 179.0820 | 181.5500 | 0.7          | 0.1          | 0.2          | 27.6110  | 25.2810  |
| 0.3          | 0.1          | 0.6          | 29.0230  | 28.9950  | 0.7          | 0.2          | 0.1          | 51.1270  | 48.4810  |
| 0.3          | 0.2          | 0.5          | 54.1230  | 52.3180  | 0.8          | 0.1          | 0.1          | 25.4910  | 24.7330  |
| 0.3          | 0.3          | 0.4          | 82.7330  | 82.0180  | MAX          |              |              | 205.1960 | 211.2450 |
| 0.3          | 0.4          | 0.3          | 98.3360  | 104.4720 | MIN          |              |              | 25.4230  | 24.7330  |

**TABLE 3.2.46 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 24$ ,  $J = 3$ , and  $K = 4$**

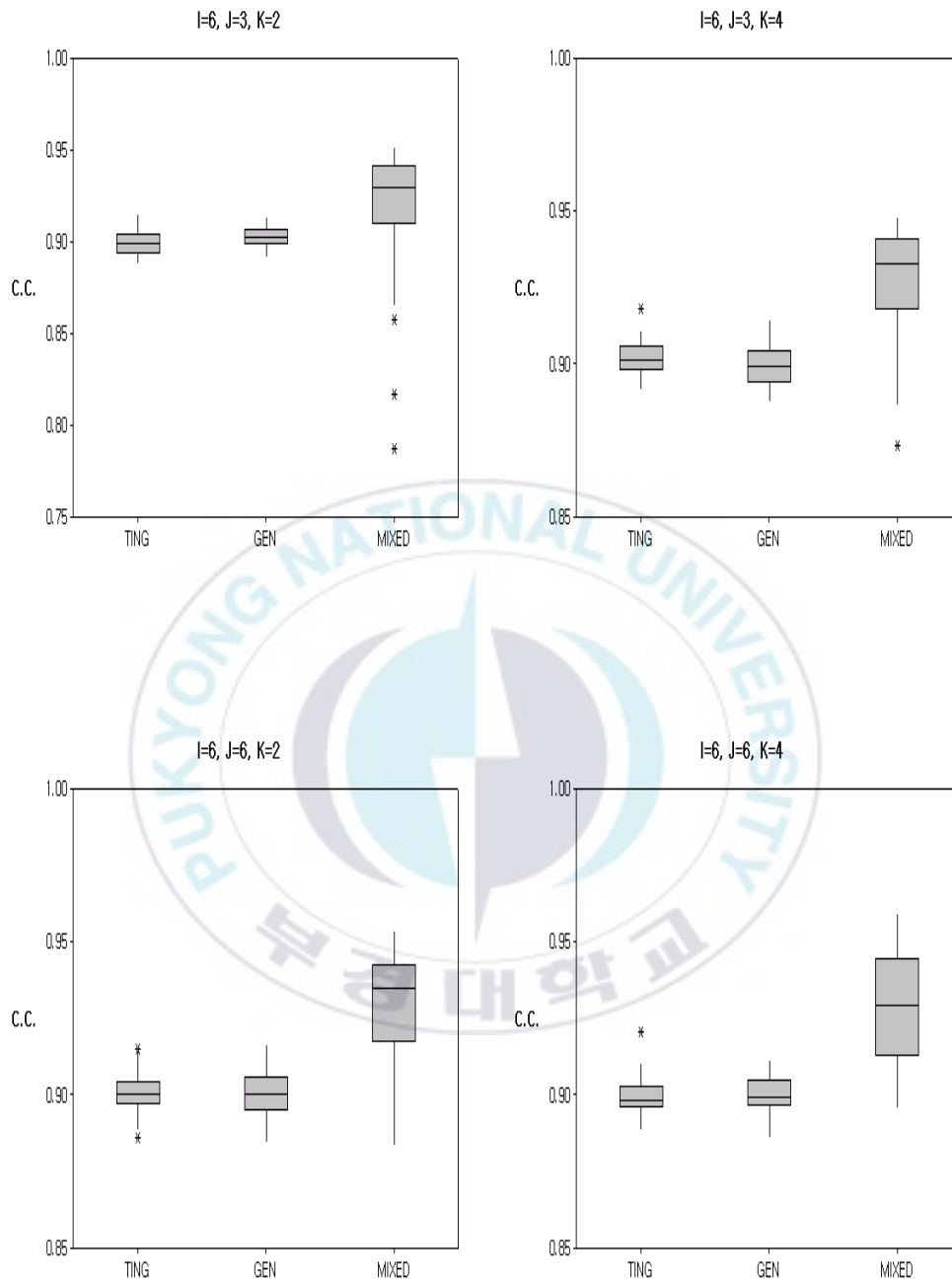
| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING     | GEN      |
|--------------|--------------|--------------|----------|----------|--------------|--------------|--------------|----------|----------|
| 0.1          | 0.1          | 0.8          | 27.0070  | 27.3250  | 0.3          | 0.5          | 0.2          | 126.6620 | 130.0570 |
| 0.1          | 0.2          | 0.7          | 53.1470  | 52.9450  | 0.3          | 0.6          | 0.1          | 159.4130 | 155.5530 |
| 0.1          | 0.3          | 0.6          | 76.5400  | 80.8150  | 0.4          | 0.1          | 0.5          | 26.8090  | 26.7110  |
| 0.1          | 0.4          | 0.5          | 102.7540 | 105.1570 | 0.4          | 0.2          | 0.4          | 54.0760  | 52.3040  |
| 0.1          | 0.5          | 0.4          | 127.6640 | 123.2050 | 0.4          | 0.3          | 0.3          | 77.6300  | 79.6960  |
| 0.1          | 0.6          | 0.3          | 165.6880 | 150.4870 | 0.4          | 0.4          | 0.2          | 105.0850 | 106.0740 |
| 0.1          | 0.7          | 0.2          | 182.5380 | 170.0140 | 0.4          | 0.5          | 0.1          | 134.0360 | 130.9680 |
| 0.1          | 0.8          | 0.1          | 216.4460 | 206.6890 | 0.5          | 0.1          | 0.4          | 27.1090  | 26.5270  |
| 0.2          | 0.1          | 0.7          | 28.0110  | 27.4400  | 0.5          | 0.2          | 0.3          | 52.2250  | 53.2230  |
| 0.2          | 0.2          | 0.6          | 53.9890  | 51.3830  | 0.5          | 0.3          | 0.2          | 77.9930  | 76.7690  |
| 0.2          | 0.3          | 0.5          | 77.0940  | 78.5240  | 0.5          | 0.4          | 0.1          | 103.2420 | 102.5400 |
| 0.2          | 0.4          | 0.4          | 109.4740 | 103.6290 | 0.6          | 0.1          | 0.3          | 26.4440  | 26.1880  |
| 0.2          | 0.5          | 0.3          | 128.5670 | 129.1990 | 0.6          | 0.2          | 0.2          | 52.4730  | 48.8490  |
| 0.2          | 0.6          | 0.2          | 161.9280 | 151.7190 | 0.6          | 0.3          | 0.1          | 76.9280  | 74.7030  |
| 0.2          | 0.7          | 0.1          | 171.8740 | 173.4900 | 0.7          | 0.1          | 0.2          | 24.9920  | 25.7320  |
| 0.3          | 0.1          | 0.6          | 27.0030  | 27.4190  | 0.7          | 0.2          | 0.1          | 47.2500  | 51.1660  |
| 0.3          | 0.2          | 0.5          | 51.6950  | 51.9850  | 0.8          | 0.1          | 0.1          | 24.9220  | 25.2500  |
| 0.3          | 0.3          | 0.4          | 71.9060  | 77.6490  | MAX          |              |              | 216.4460 | 206.6890 |
| 0.3          | 0.4          | 0.3          | 104.1280 | 108.8730 | MIN          |              |              | 24.9220  | 25.2500  |

**TABLE 3.2.47 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 24$ ,  $J = 6$ , and  $K = 2$**

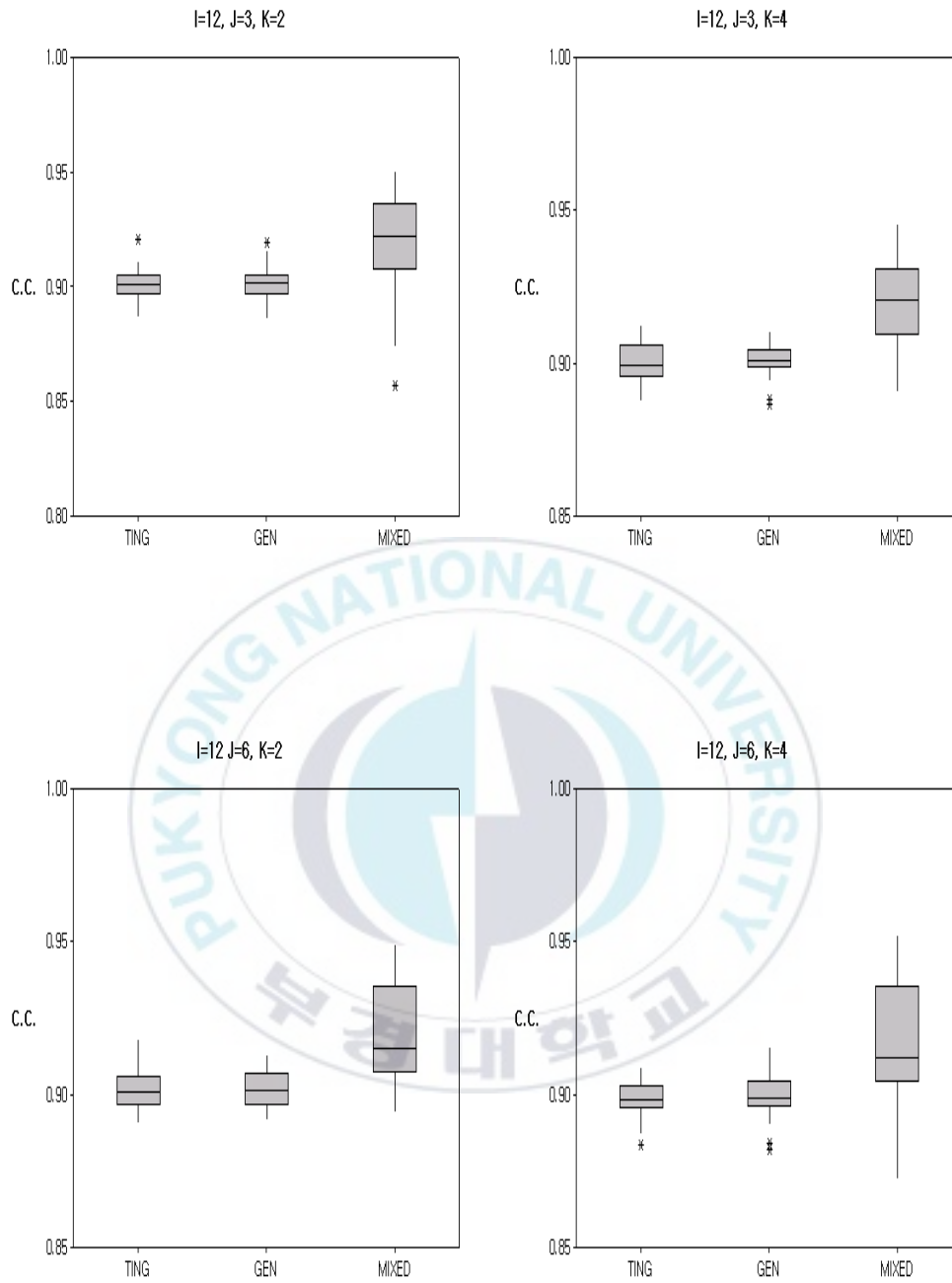
| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.5953 | 0.6034 | 0.3          | 0.5          | 0.2          | 2.6400 | 2.6372 |
| 0.1          | 0.2          | 0.7          | 1.1105 | 1.1176 | 0.3          | 0.6          | 0.1          | 3.1089 | 3.1461 |
| 0.1          | 0.3          | 0.6          | 1.6202 | 1.6091 | 0.4          | 0.1          | 0.5          | 0.5622 | 0.5755 |
| 0.1          | 0.4          | 0.5          | 2.0854 | 2.0567 | 0.4          | 0.2          | 0.4          | 1.0435 | 1.0855 |
| 0.1          | 0.5          | 0.4          | 2.5841 | 2.6898 | 0.4          | 0.3          | 0.3          | 1.5793 | 1.6253 |
| 0.1          | 0.6          | 0.3          | 3.1539 | 3.2110 | 0.4          | 0.4          | 0.2          | 2.1097 | 2.0743 |
| 0.1          | 0.7          | 0.2          | 3.5694 | 3.6434 | 0.4          | 0.5          | 0.1          | 2.5776 | 2.6866 |
| 0.1          | 0.8          | 0.1          | 4.1620 | 4.0718 | 0.5          | 0.1          | 0.4          | 0.5722 | 0.5548 |
| 0.2          | 0.1          | 0.7          | 0.5894 | 0.6050 | 0.5          | 0.2          | 0.3          | 1.0477 | 1.0787 |
| 0.2          | 0.2          | 0.6          | 1.1204 | 1.1141 | 0.5          | 0.3          | 0.2          | 1.6052 | 1.5245 |
| 0.2          | 0.3          | 0.5          | 1.6110 | 1.6034 | 0.5          | 0.4          | 0.1          | 2.1582 | 2.0721 |
| 0.2          | 0.4          | 0.4          | 2.1201 | 2.0978 | 0.6          | 0.1          | 0.3          | 0.5596 | 0.5604 |
| 0.2          | 0.5          | 0.3          | 2.6830 | 2.5645 | 0.6          | 0.2          | 0.2          | 1.0789 | 1.0479 |
| 0.2          | 0.6          | 0.2          | 3.1731 | 3.1560 | 0.6          | 0.3          | 0.1          | 1.5856 | 1.5559 |
| 0.2          | 0.7          | 0.1          | 3.6258 | 3.5766 | 0.7          | 0.1          | 0.2          | 0.5509 | 0.5492 |
| 0.3          | 0.1          | 0.6          | 0.5828 | 0.5925 | 0.7          | 0.2          | 0.1          | 1.0427 | 1.0873 |
| 0.3          | 0.2          | 0.5          | 1.1061 | 1.0700 | 0.8          | 0.1          | 0.1          | 0.5321 | 0.5339 |
| 0.3          | 0.3          | 0.4          | 1.5929 | 1.5846 | MAX          |              |              | 4.1620 | 4.0718 |
| 0.3          | 0.4          | 0.3          | 2.1730 | 2.1615 | MIN          |              |              | 0.5321 | 0.5339 |

**TABLE 3.2.48 Range of Average Interval Lengths**  
**for 90% Two-sided Intervals on  $\sigma_O^2$**   
**when  $I = 24$ ,  $J = 6$ , and  $K = 4$**

| $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    | $\sigma_P^2$ | $\sigma_O^2$ | $\sigma_E^2$ | TING   | GEN    |
|--------------|--------------|--------------|--------|--------|--------------|--------------|--------------|--------|--------|
| 0.1          | 0.1          | 0.8          | 0.5559 | 0.5664 | 0.3          | 0.5          | 0.2          | 2.6311 | 2.6410 |
| 0.1          | 0.2          | 0.7          | 1.0805 | 1.1029 | 0.3          | 0.6          | 0.1          | 3.2010 | 3.1442 |
| 0.1          | 0.3          | 0.6          | 1.5343 | 1.6080 | 0.4          | 0.1          | 0.5          | 0.5584 | 0.5482 |
| 0.1          | 0.4          | 0.5          | 2.0939 | 2.1470 | 0.4          | 0.2          | 0.4          | 1.0550 | 1.0675 |
| 0.1          | 0.5          | 0.4          | 2.6083 | 2.5855 | 0.4          | 0.3          | 0.3          | 1.5761 | 1.6048 |
| 0.1          | 0.6          | 0.3          | 3.1946 | 3.0974 | 0.4          | 0.4          | 0.2          | 2.1019 | 2.0531 |
| 0.1          | 0.7          | 0.2          | 3.8067 | 3.6484 | 0.4          | 0.5          | 0.1          | 2.6268 | 2.5773 |
| 0.1          | 0.8          | 0.1          | 4.1850 | 4.1526 | 0.5          | 0.1          | 0.4          | 0.5421 | 0.5326 |
| 0.2          | 0.1          | 0.7          | 0.5557 | 0.5688 | 0.5          | 0.2          | 0.3          | 1.0709 | 1.0758 |
| 0.2          | 0.2          | 0.6          | 1.0520 | 1.0727 | 0.5          | 0.3          | 0.2          | 1.5399 | 1.5848 |
| 0.2          | 0.3          | 0.5          | 1.5754 | 1.5669 | 0.5          | 0.4          | 0.1          | 2.0340 | 2.0714 |
| 0.2          | 0.4          | 0.4          | 2.0792 | 2.0928 | 0.6          | 0.1          | 0.3          | 0.5318 | 0.5469 |
| 0.2          | 0.5          | 0.3          | 2.5827 | 2.7061 | 0.6          | 0.2          | 0.2          | 1.0676 | 1.0864 |
| 0.2          | 0.6          | 0.2          | 3.1827 | 3.2555 | 0.6          | 0.3          | 0.1          | 1.5508 | 1.6257 |
| 0.2          | 0.7          | 0.1          | 3.6921 | 3.7204 | 0.7          | 0.1          | 0.2          | 0.5363 | 0.5255 |
| 0.3          | 0.1          | 0.6          | 0.5703 | 0.5451 | 0.7          | 0.2          | 0.1          | 1.0587 | 1.0498 |
| 0.3          | 0.2          | 0.5          | 1.0725 | 1.0493 | 0.8          | 0.1          | 0.1          | 0.5264 | 0.5277 |
| 0.3          | 0.3          | 0.4          | 1.6222 | 1.5900 | MAX          |              |              | 4.1850 | 4.1526 |
| 0.3          | 0.4          | 0.3          | 2.0683 | 2.1199 | MIN          |              |              | 0.5264 | 0.5255 |

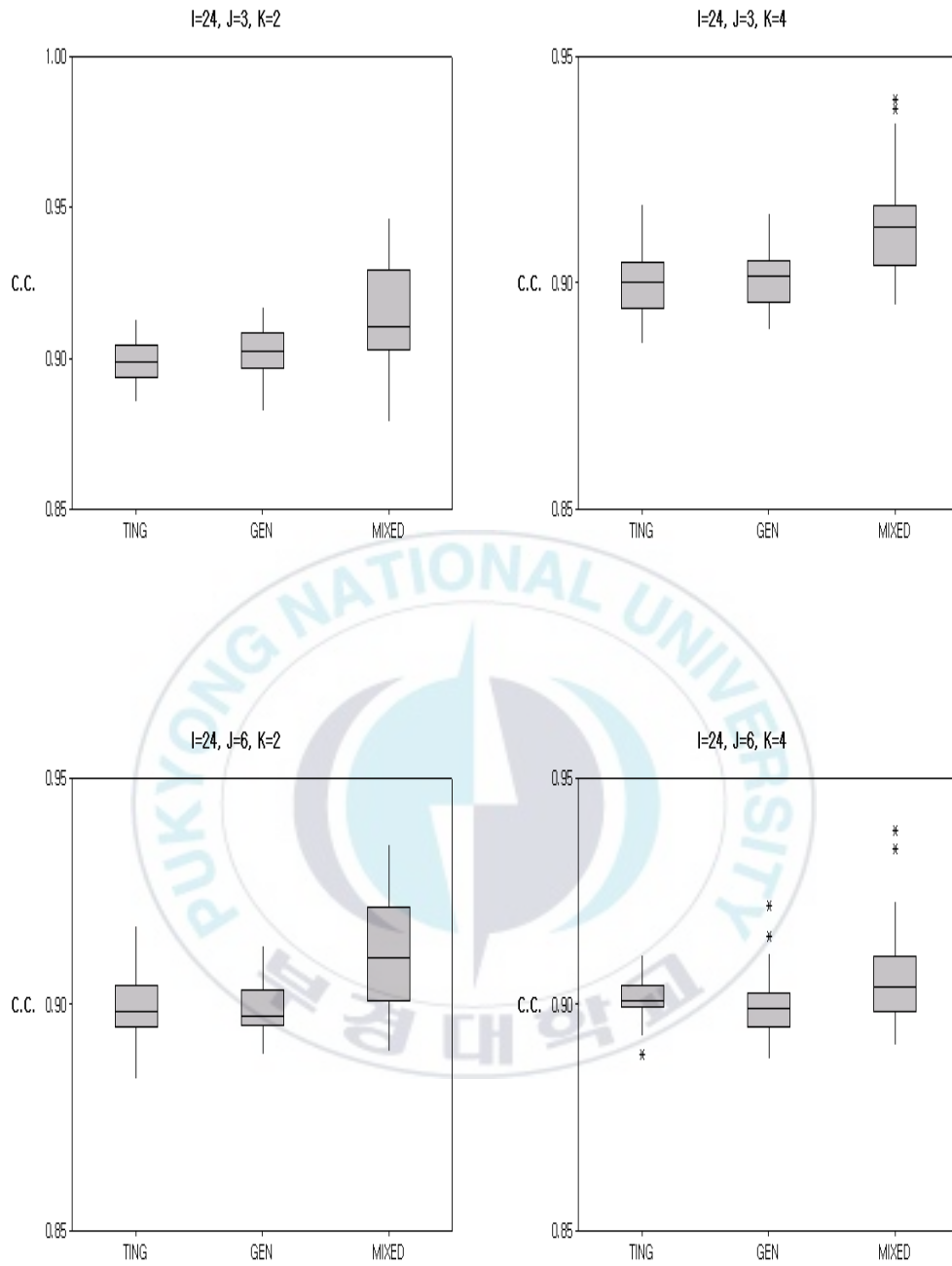


*Figure 3.2.1.a* Boxplots for Simulated Confidence Coefficients  
for 90% Two-sided Intervals on  $\sigma_P^2$

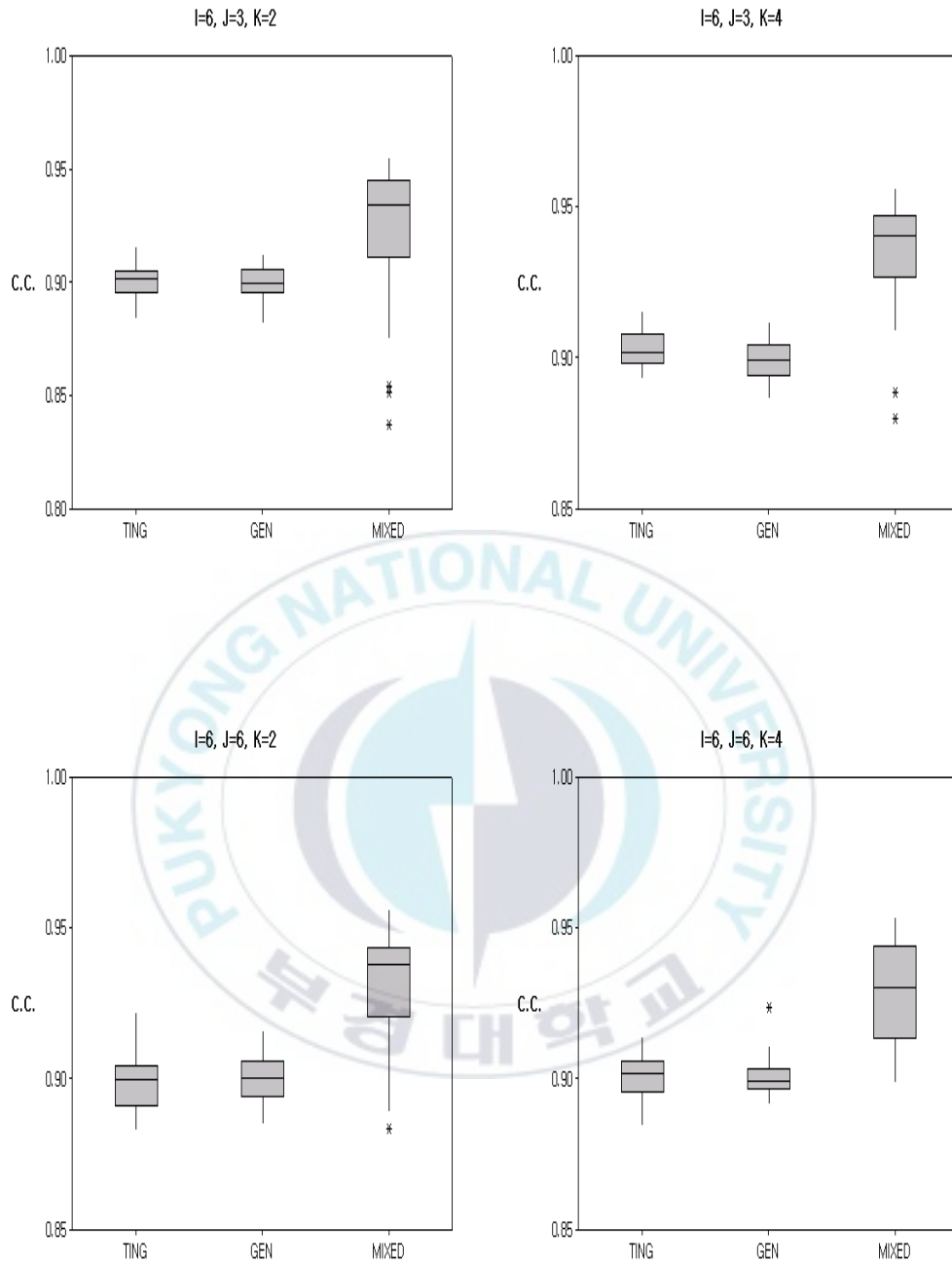


*Figure 3.2.1.b* Boxplots for Simulated Confidence Coefficients  
for 90% Two-sided Intervals on  $\sigma_P^2$

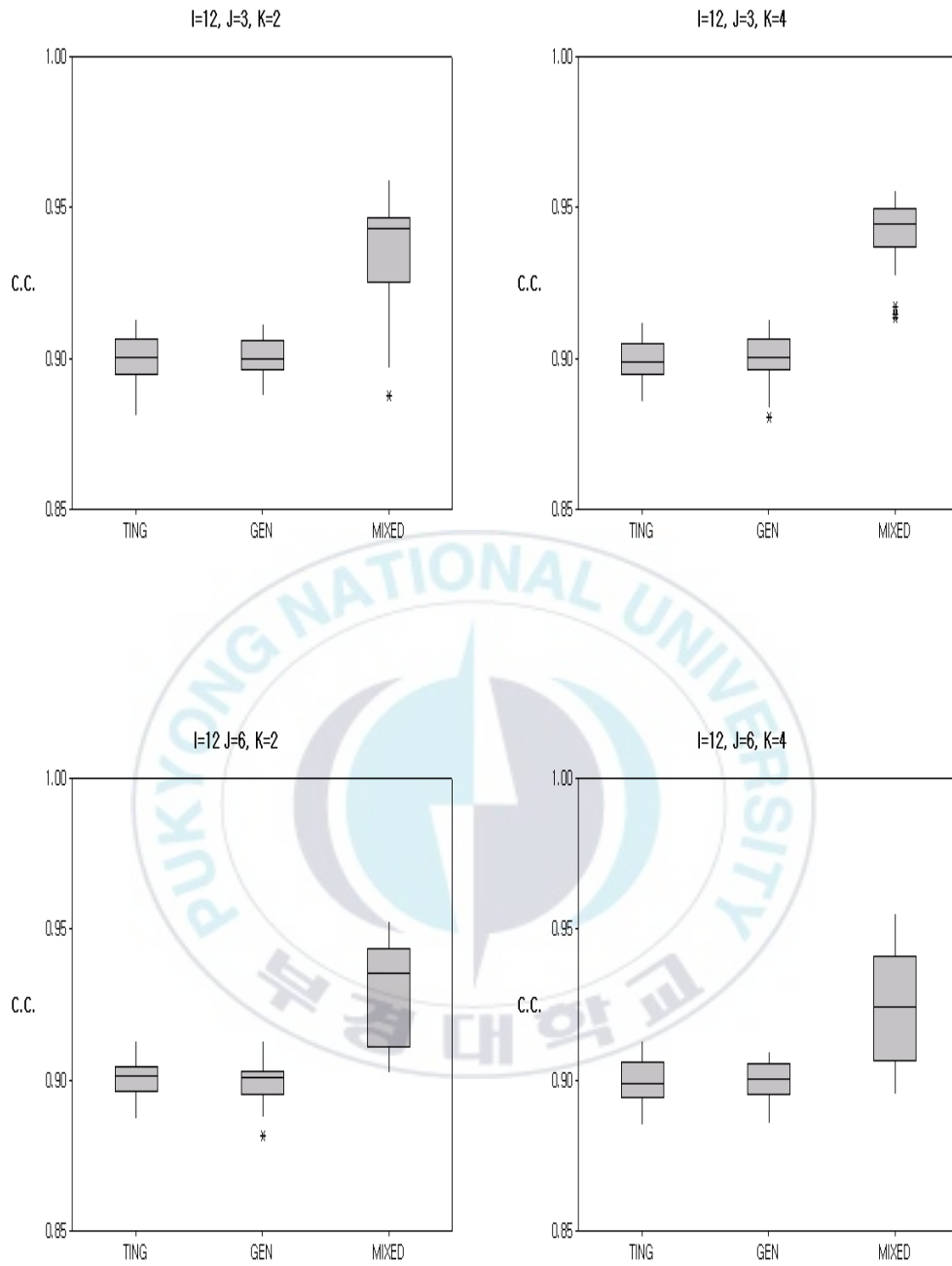




*Figure 3.2.1.c* Boxplots for Simulated Confidence Coefficients  
for 90% Two-sided Intervals on  $\sigma_P^2$



*Figure 3.2.2.a* Boxplots for Simulated Confidence Coefficients for 90% Two-sided Intervals on  $\sigma_O^2$



*Figure 3.2.2.b* Boxplots for Simulated Confidence Coefficients  
for 90% Two-sided Intervals on  $\sigma_O^2$

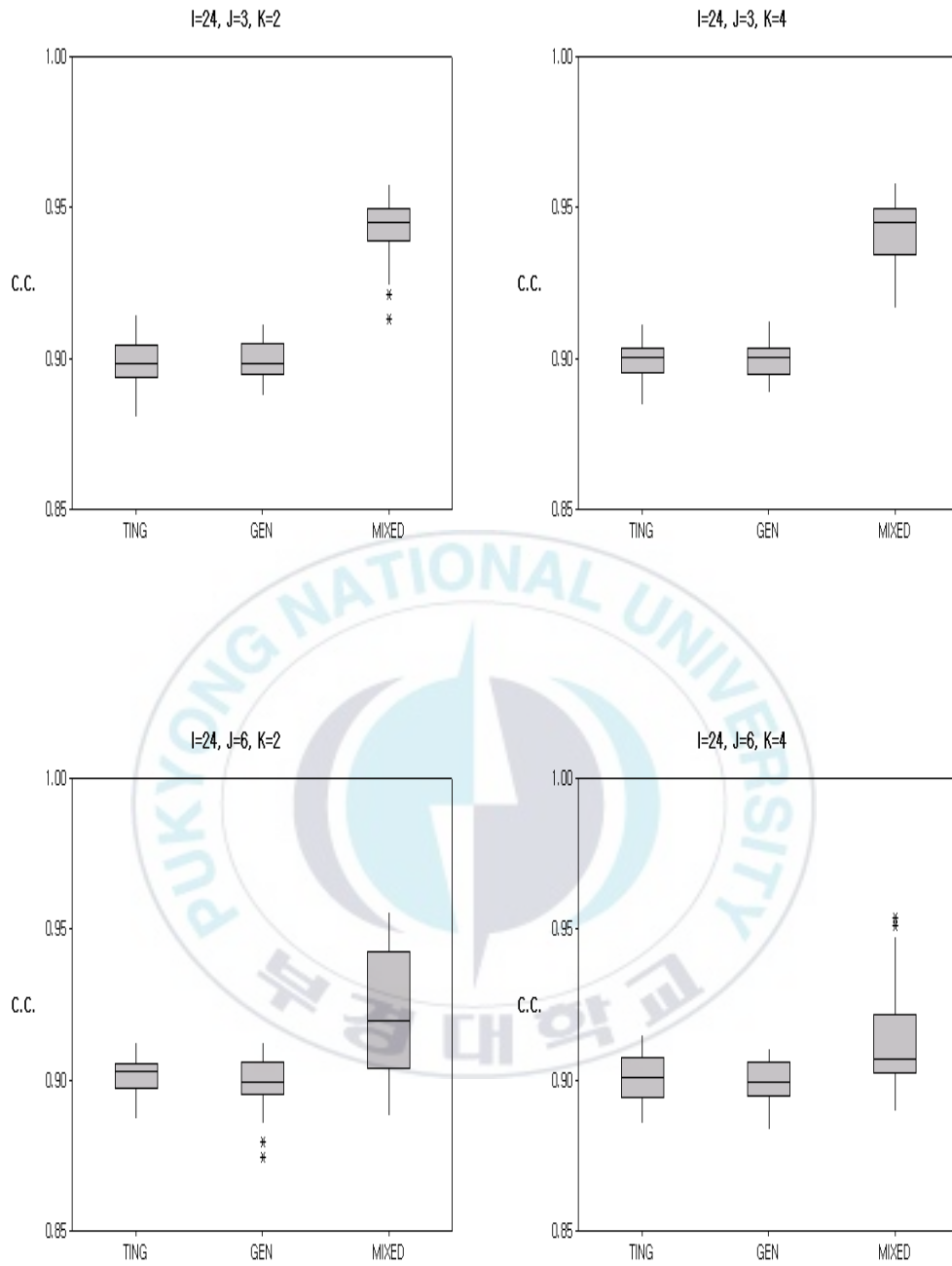
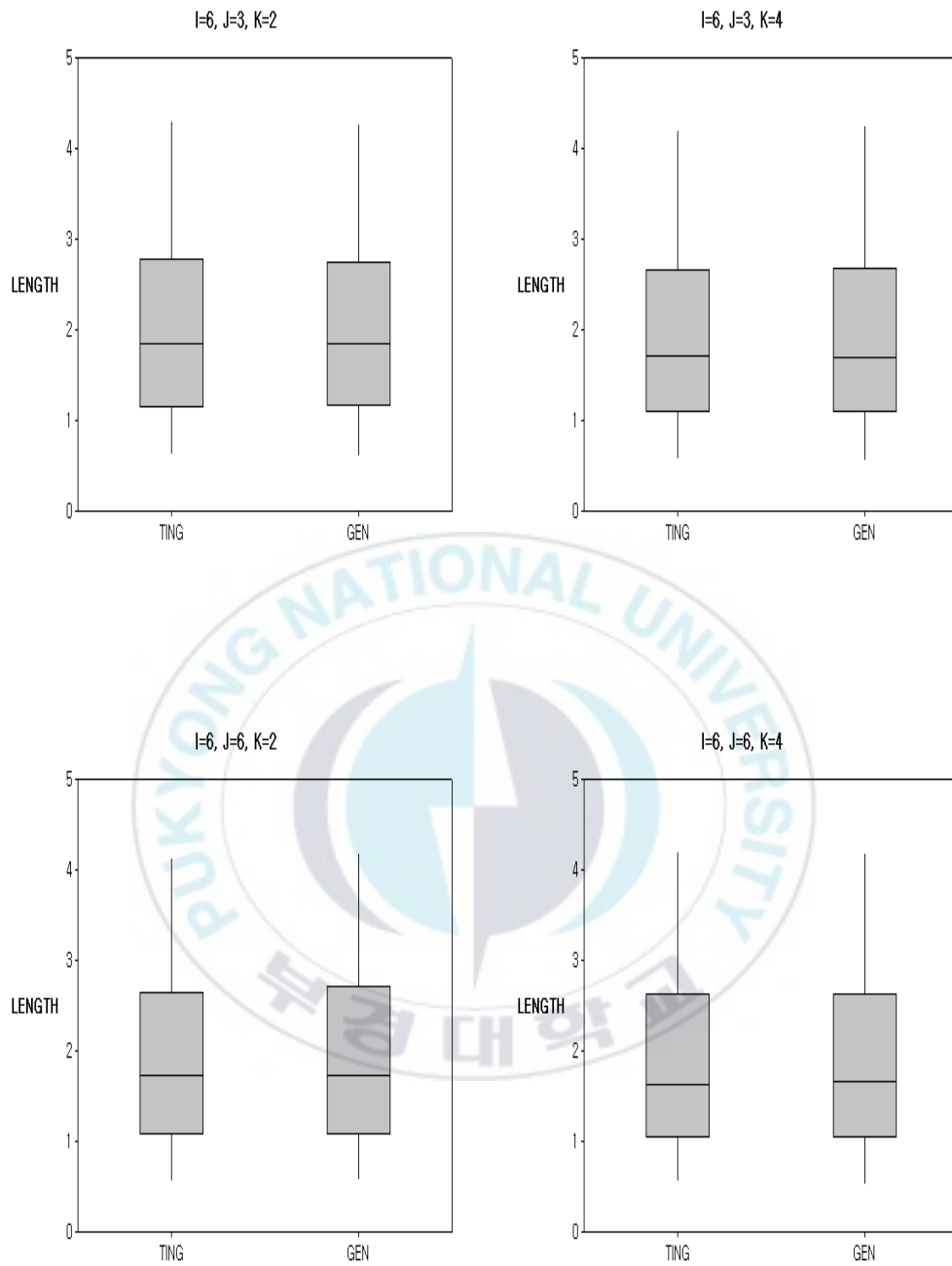
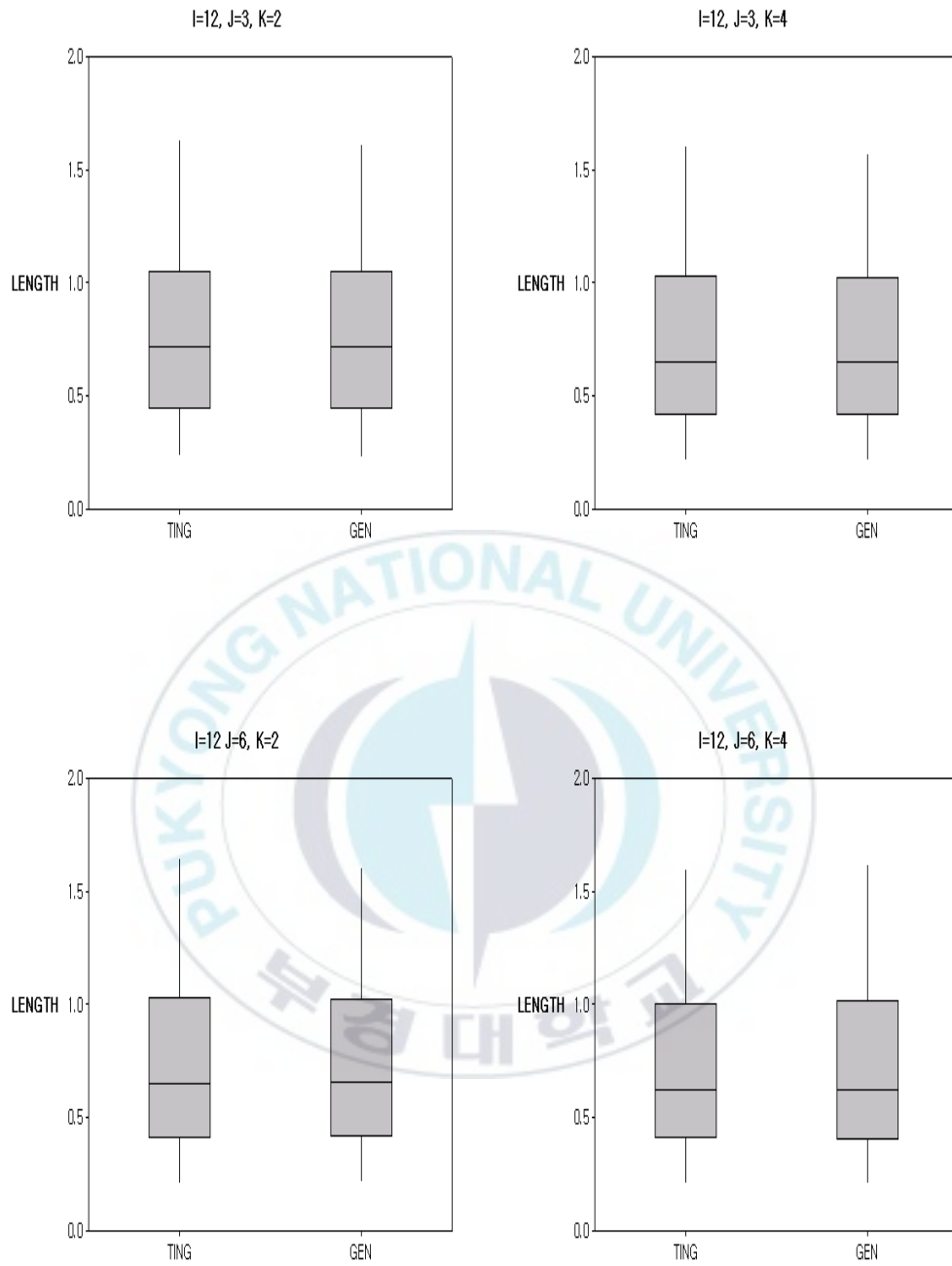


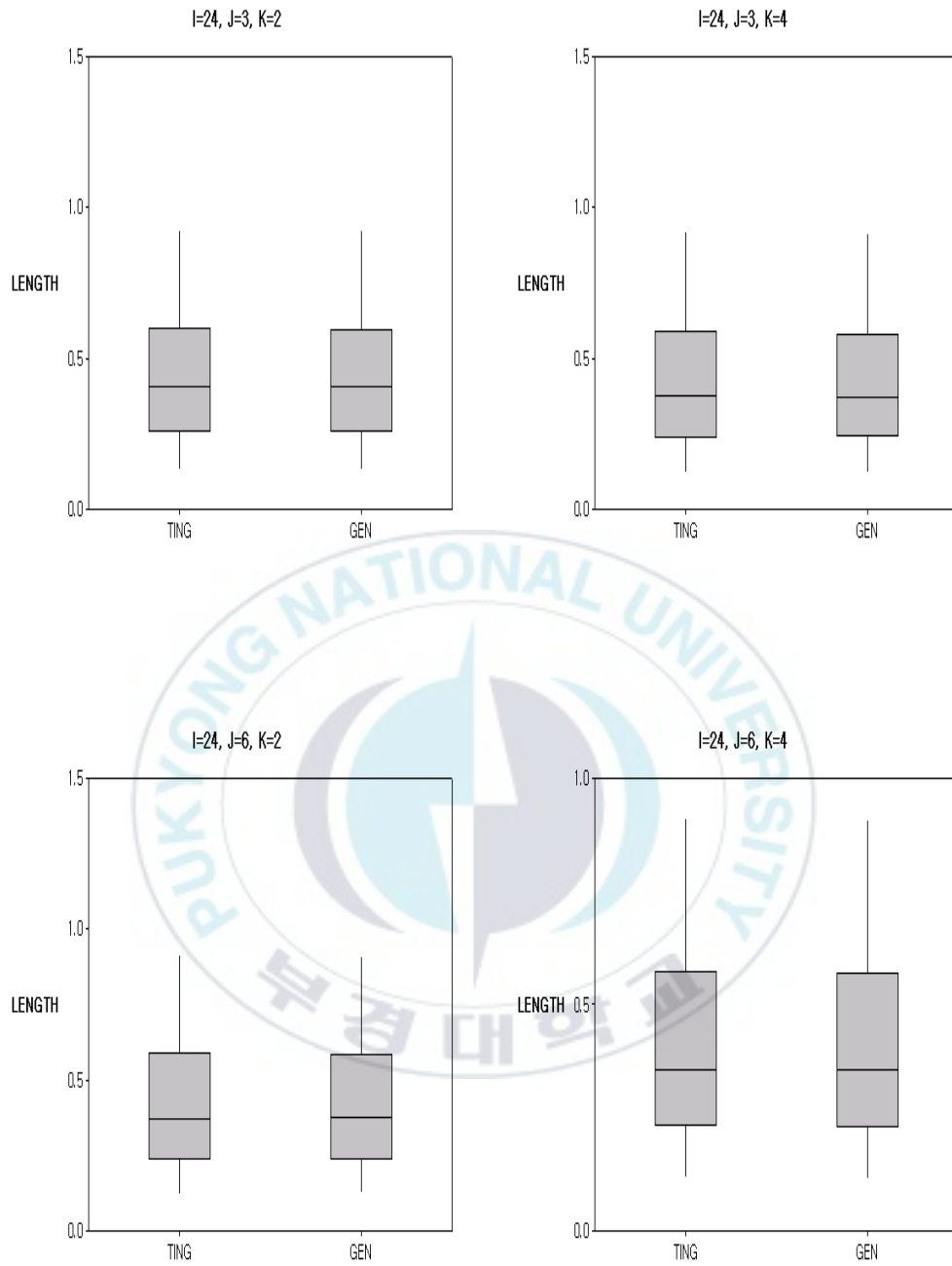
Figure 3.2.2.c Boxplots for Simulated Confidence Coefficients  
for 90% Two-sided Intervals on  $\sigma_O^2$



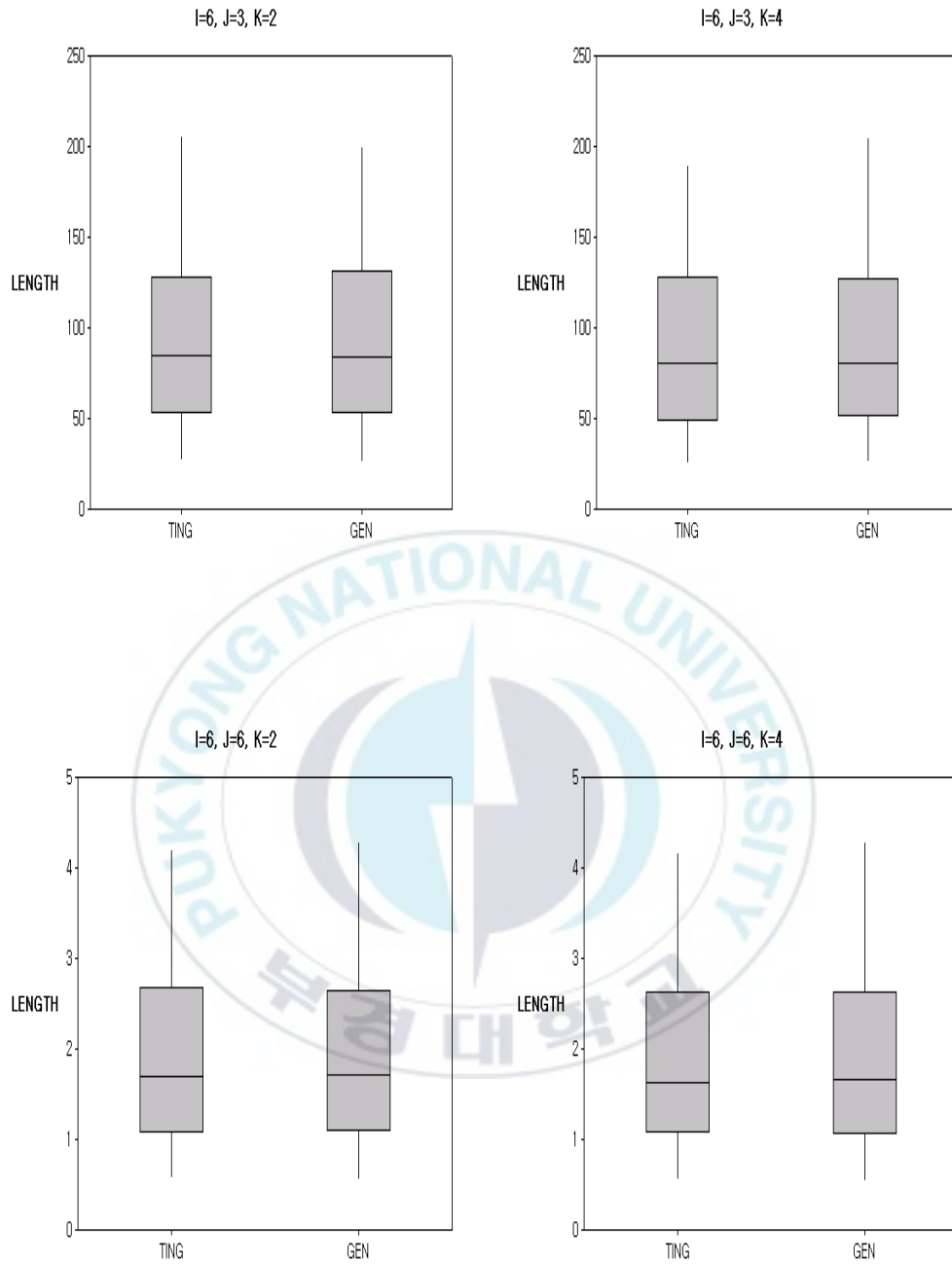
*Figure 3.2.3.a* Boxplots for Average Interval Lengths  
for 90% Two-sided Intervals on  $\sigma_P^2$



*Figure 3.2.3.b* Boxplots for Average Interval Lengths  
for 90% Two-sided Intervals on  $\sigma_P^2$

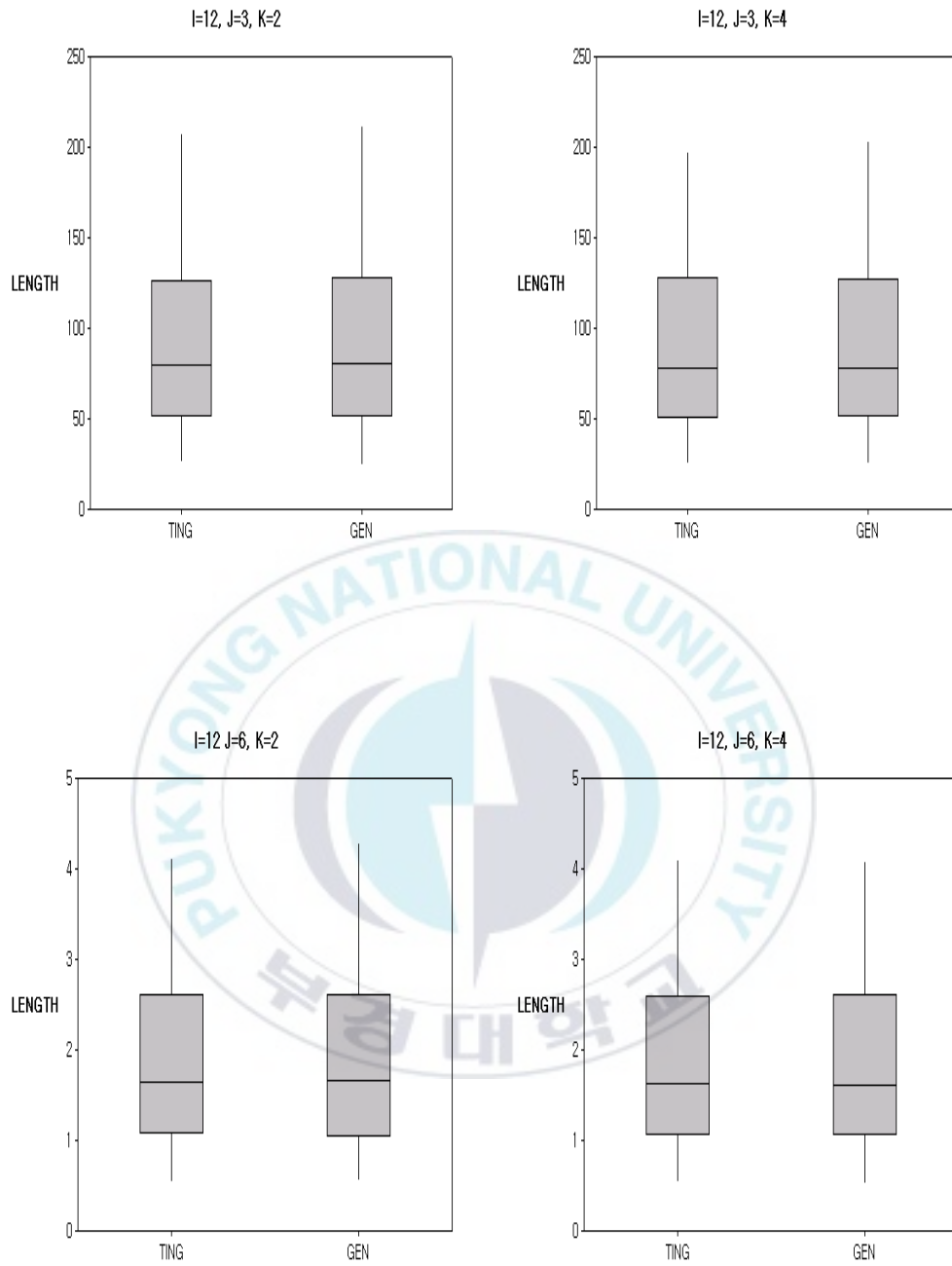


*Figure 3.2.3.c* Boxplots for Average Interval Lengths  
for 90% Two-sided Intervals on  $\sigma_P^2$

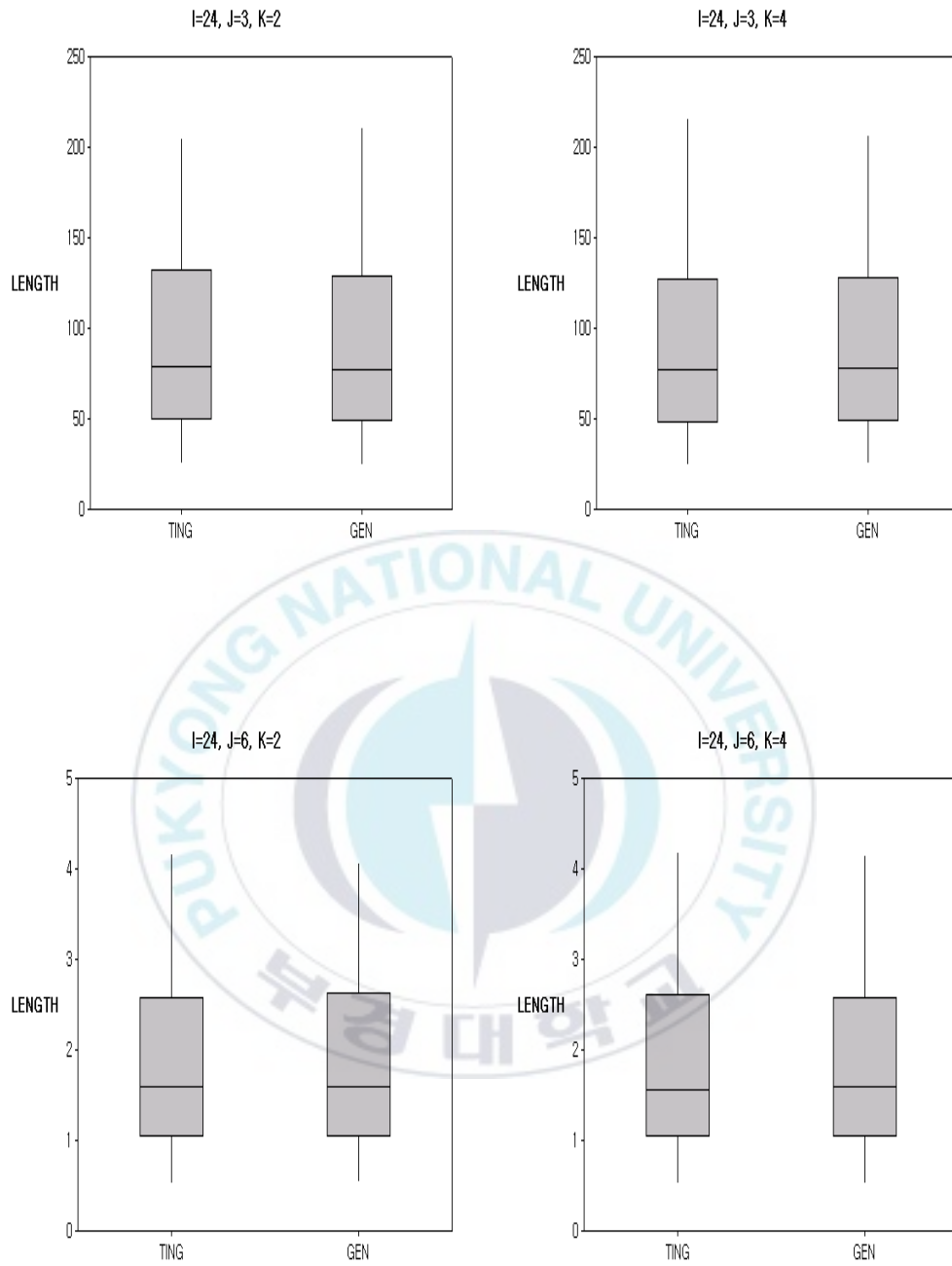


*Figure 3.2.4.a* Boxplots for Average Interval Lengths  
for 90% Two-sided Intervals on  $\sigma_O^2$





*Figure 3.2.4.b* Boxplots for Average Interval Lengths  
for 90% Two-sided Intervals on  $\sigma_O^2$



*Figure 3.2.4.c* Boxplots for Average Interval Lengths  
for 90% Two-sided Intervals on  $\sigma_O^2$

### 3.3 A Numerical Example

The confidence intervals on variance components are now applied to a data set. Milliken and Johnson(2002 p.370) published a data set from an experiment designed to evaluate the effect of the speed in rpm of a circular bar of steel and the feed rate into a cutting tool on the roughness of the surface finish of the final turned product, where the depth of cut was set to 0.02 in. The treatment structure is a two-way with four levels of speed(rpm) and four levels of feed rate. Eight replications were performed for each combination of speed and feed rate. There is variation in the hardness of the bar stock used in the experiment; thus the hardness of each piece of bar was measured to be used as a possible covariate. There is a linear relationship between roughness and hardness.

In order to apply to this data set, the speed and feed rate are assumed to be operator effects and part effects, respectively. The data set was constructed by selecting first three speed rates(operators) and four feed rate(parts) with first two observations of each combination of speed and feed rate to represent replicated measurements. Roughness( $Y$ ) is linearly related to hardness( $X$ ). The selected data set is listed in Table 3.3.1. The SAS code is written to calculate confidence intervals on the variance for parts, operators, and measurement error. The SAS code used is listed in the Appendix. The mean squares in Table 2.2.2,  $S_P^2/(JK)$ ,  $S_O^2/(IK)$ , and  $S_E^2$  can be obtained in MEAN SQUARE ERRORS of ANOVA Tables by executing following PROC GLM statements.

**TABLE 3.3.1 Data Set Used**

|   | Operators |    |     |    |     |    |
|---|-----------|----|-----|----|-----|----|
|   | 1         |    | 2   |    | 3   |    |
|   | Y         | X  | Y   | X  | Y   | X  |
| 1 | 50        | 61 | 65  | 59 | 84  | 64 |
|   | 53        | 65 | 55  | 44 | 104 | 70 |
| 2 | 64        | 54 | 81  | 65 | 108 | 41 |
|   | 61        | 58 | 81  | 53 | 118 | 67 |
| 3 | 97        | 62 | 103 | 61 | 123 | 41 |
|   | 79        | 48 | 105 | 53 | 137 | 41 |
| 4 | 141       | 66 | 158 | 56 | 192 | 69 |
|   | 142       | 61 | 154 | 49 | 195 | 57 |

**TABLE3.3.2 An Example Statement of  
PROC GLM for Calculating Mean Squares**

```

.
PROC GLM DATA = TWO;
MODEL YMEAN = XMEAN;
.
.
PROC GLM DATA = THREE;
MODEL YMEAN2 = XMEAN2;
.
PROC GLM DATE = ONE;
CLASS PART OPERATOR;
MODEL Y = X PART OPERATOR;
.

```

The results of PROC GLM are shown in Table 3.3.3.

**TABLE 3.3.3 Results of PROC GLM**

| SV         | DF | MS       | EMS                         |
|------------|----|----------|-----------------------------|
| Parts      | 2  | 15417.25 | $\sigma_E^2 + JK\sigma_P^2$ |
| Operators  | 1  | 6688.86  | $\sigma_E^2 + IK\sigma_O^2$ |
| Replicates | 17 | 28.89    | $\sigma_E^2$                |

The ANOVA estimators of  $\sigma_P^2$ ,  $\sigma_O^2$ , and  $\sigma_E^2$  are computed using the results of PROC GLM and (2.2.8). In particular,

$$\begin{aligned}
 \hat{\sigma}_P^2 &= \frac{S_P^2 - S_E^2}{JK} = \frac{15417.25 - 28.89}{3 \times 2} = 2564.7 \\
 \hat{\sigma}_O^2 &= \frac{S_O^2 - S_E^2}{IK} = \frac{6688.86 - 28.89}{4 \times 2} = 832.49 \\
 \hat{\sigma}_E^2 &= 28.89
 \end{aligned} \tag{3.3.1}$$

The calculated values of  $S_P^2$ ,  $S_O^2$ , and  $S_E^2$  are substituted in (2.3.3) and (2.3.5) for computing TING method. The values are used as observed values to construct the distribution in (2.4.2) and (2.4.4) for GEN method . PROC MIXED automatically generates confidence intervals based on MIXED method. The resulting confidence intervals are reported in Table 3.3.4.

Since

$$\begin{aligned}
 \frac{\hat{\sigma}_P^2}{\hat{\sigma}_P^2 + \hat{\sigma}_O^2 + \hat{\sigma}_E^2} &= \frac{2564.7}{3425.1} = 0.7, \\
 \frac{\hat{\sigma}_O^2}{\hat{\sigma}_P^2 + \hat{\sigma}_O^2 + \hat{\sigma}_E^2} &= \frac{832.49}{3425.1} = 0.2,
 \end{aligned} \tag{3.3.2}$$

the estimates are assumed to be  $\hat{\sigma}_P^2 = 0.7$ ,  $\hat{\sigma}_O^2 = 0.2$ , and  $\hat{\sigma}_E^2 = 0.1$  without loss of generality. By simulation study it is shown that the confidence interval based on PROC MIXED does not keep the stated confidence coefficients when  $\hat{\sigma}_P^2$  or  $\hat{\sigma}_O^2$  is approximately below 0.3. Thus the confidence interval based on  $\hat{\sigma}_O^2$  is not recommended in this example although it is shorter than ones based on TING and GEN methods.

**TABLE 3.3.4 90% Confidence Intervals on Variance Components**

| Effects     | Method | Lower Bound | Upper Bound | Interval Length |
|-------------|--------|-------------|-------------|-----------------|
| Part        | TING   | 852.8       | 50089.9     | 49237.1         |
|             | GEN    | 865.1       | 50362.0     | 49496.9         |
|             | MIXED  | 654.8       | 14705.0     | 14050.2         |
| Operator    | TING   | 214.0       | 212630.3    | 212416.3        |
|             | GEN    | 217.2       | 213030.4    | 212813.2        |
|             | MIXED  | 197.1       | 11923.0     | 11725.9         |
| Measurement | TING   | 17.8        | 56.6        | 38.8            |
| Error       | GEN    | 17.8        | 56.7        | 38.9            |
|             | MIXED  | 17.8        | 56.6        | 38.8            |

### 3.4 Concluding Remarks

In this thesis two-factor crossed mixed model with one covariate for gauge R & R study is considered. This model employs  $J$  operators randomly chosen to conduct measurements on  $I$  randomly selected parts from a manufacturing process. In this R&R study each operator measures each part  $k$  times. The measurement is assumed to be linearly related to one covariate in this R&R study. The variabilities of the parts, operators, and measurements can be measured in terms of confidence intervals. Confidence intervals of the variance of part effects, operator effects, and measurement errors are useful tools to determine whether the variability is appropriate in a manufacturing process.

Three confidence intervals proposed are based on Ting et al.(1990) method (TING), generalized p-values concept (GEN), and SAS PROC MIXED (MIXED). Eight different designs of  $I$ ,  $J$ , and  $K$  are considered for simulation study to see if the proposed intervals maintain the stated confidence coefficients and to compare the average interval lengths of three methods. Two-sided 90% confidence intervals are computed 2000 times for eight designs with 36 combinations of the values of  $\sigma_P^2$ ,  $\sigma_O^2$ , and  $\sigma_E^2$ . Based on the simulation study TING and GEN methods generally maintain the stated confidence coefficients for all combinations of  $I$ ,  $J$ , and  $K$ . Their average interval lengths are similar and comparable. However, MIXED method does not keep the stated confidence coefficient especially for small values of  $\sigma_P^2$  and  $\sigma_O^2$ . In particular, when the values of  $\sigma_P^2$  and  $\sigma_O^2$  are small, the simulated confidence coefficients dramatically fall below the stated confidence coefficient 0.9. Thus TING and GEN methods are recommended for calculating confidence intervals on the variance of part and operator effects for all combinations of  $I$ ,  $J$ , and  $K$ . MIXED method is an alternative for computing confidence intervals if the values of  $I$ ,  $J$ , and  $K$  are large enough.

## REFERENCES

- [1] Adamec, E. and Richard, R. K. (2003), “ Confidence Intervals for a Discrimination Ratio in a Gauge R & R Study with Three Random Factors, ” *Quality Engineering*, 15(3), 383-389.
- [2] Borror, C. M., Montgomery, D. C., and Runger, G. C. (1997), “ Confidence Intervals for Variance Components from Gauge Capability Studies, ” *Quality and Reliability Engineering International*, 13, 361-369.
- [3] Burdick, R. K. and Larsen, G. A. (1997), “ Confidence Intervals on Measures of Variability in R & R Studies, ” *Journal of Quality Technology*, 29(3), 261-273.
- [4] Burdick, R. K., Borror, C. M., and Montgomery, D. C. (2003), “ A Review of Methods for Measurement Systems Capability Analysis, ” *Journal of Quality Technology*, 35(4), 342-354.
- [5] Burdick, R. K., Borror, C. M., and Montgomery, D. C. (2005), “*Design and Analysis of Gauge R & R Studies-Making Decisions with Confidence Intervals in Random and Mixed ANOVA Models*, ” ASA-SIAM Series on Statistics and Applied Probability, SIAM, Philadelphia, ASA, Alexandria, VA.
- [6] Dolezal, K. K., Burdick, R. K., and Birch, N. J. (1998), “ Analysis of a Two-factor R & R Study with Fixed Operators, ” *Journal of Quality Technology*, 30(2), 163-170.
- [7] Gong, L., Burdick, R. K., and Quiroz, J. (2005), “ Confidence Intervals for Unbalanced Two-factor Gauge R & R Studies, ” *Quality and Reliability Engineering International*, 21(8), 727-741.



- [8] Milliken, G. A. and Johnson, D. E. (2002), “*Analysis of Messy Data Volume III: Analysis of Covariance*, ” CHAPMAN & HALL/CRC.
- [9] Montgomery, D. C. and Runger, G. C. (1993 a), “ Gauge Capability and Designed Experiments. Part I: Basic Methods, ” *Quality Engineering*, 6(1), 115-135.
- [10] Montgomery, D. C. and Runger, G. C. (1993 b), “ Gauge Capability and Designed Experiments. Part II: Experimental Design Models and Variance Component Estimation, ” *Quality Engineering*, 6(2), 289-305.
- [11] Searle, S. R. (1987), “*Linear Models for Unbalanced Data*”, John Wiley & Sons, Inc.
- [12] Statistical Analysis System (2005), “*SAS User’s Guide : Statistics, Cary, North Carolina*”, SAS Institute Inc.
- [13] Ting, N., Burdick, R. K., Graybill, F. A., Jeyaratnam, S., and Lu, T.-F. C.(1990), “Confidence Intervals on Linear Combinations of Variance Components,” *Journal of Statistical Computation and Simulation*, 35, 135-143.

## Appendix

SAS Code for constructing confidence intervals on variance components

```
OPTIONS LS=75 PS=55;
data one;
input y x part operator replicate @@;
datalines;
50 61 1 1 1 53 65 1 1 2 65 59 1 2 1 55 44 1 2 2
84 64 1 3 1 104 70 1 3 2 64 54 2 1 1 61 58 2 1 2
81 65 2 2 1 81 53 2 2 2 108 41 2 3 1 118 67 2 3 2
97 62 3 1 1 79 48 3 1 2 103 61 3 2 1 105 53 3 2 2
123 41 3 3 1 137 41 3 3 2 141 66 4 1 1 142 61 4 1 2
158 56 4 2 1 154 49 4 2 2 192 69 4 3 1 195 57 4 3 2
;
proc sort data=one;
  by part;
proc means;
  by part;
  var y x;
  output out=two mean= ymean xmean;
PROC GLM DATA = two;
  MODEL ymean = xmean /solution ;
proc sort data=one;
  by operator;
proc means;
  by operator;
  var y x;
  output out=three mean= ymean2 xmean2;
PROC GLM DATA = three;
  MODEL ymean2 = xmean2 /solution;
PROC GLM data=one ;
  class part operator ;
  MODEL y = x part operator /solution;
proc mixed data=one asycov cl alpha=0.1 method=reml;
  classes part operator;
  model y = x;
  random part operator;
*---F values to calculate confidence intervals
```

```

using TING method;
proc iml;
SP2 = 15417.25483;
S02 = 6688.860576;
SE2 = 28.89106;
ALPHA=.10;
print SP2 S02 SE2 alpha;
I = 4;
J = 3;
K= 2;
N1 = I - 2;
N2 = J - 2;
N3 = I*J*K - I - J;
print I J K N1 N2 N3;
F1 = FINV( 1 - alpha/2, N1, N3);
F2 = FINV( alpha/2, N1, N3);
G1 = 1 - 1/(CINV(1 - ALPHA/2, N1)/N1);
H2 = 1/(CINV(ALPHA/2, N3)/N3) - 1;
H1 = 1/(CINV(ALPHA/2, N1)/N1) - 1;
G2 = 1 - 1/(CINV(1 - ALPHA/2, N3)/N3);
G12 = ((F1 - 1)**2 - (G1 * F1)**2 - H2**2)/F1;
H12 = ((1 - F2)**2 - (H1 * F2)**2 - G2**2)/F2;
PRINT ALPHA F1 F2;
PRINT G1 H2 H1 G2 G12 H12;
*---Calculation of Confidence Intervals on SigPsq
using TING method;
SigPlb = ( SP2 - SE2 - SQRT(G1**2 * SP2**2
      + H2**2 * SE2**2 + G12*SP2*SE2))/(J*K);
SigPub = ( SP2 - SE2 + SQRT(H1**2 * SP2**2
      + G2**2 * SE2**2 + H12*SP2*SE2))/(J*K);
SigPint = max(0, SigPub) - max(0, SigPlb);
PRINT SigPlb SigPub SigPint;
F3 = FINV( 1 - alpha/2, N2, N3);
F4 = FINV( alpha/2, N2, N3);
G3 = 1 - 1/(CINV(1 - ALPHA/2, N2)/N2);
H4 = 1/(CINV(ALPHA/2, N3)/N3) - 1;
H3 = 1/(CINV(ALPHA/2, N2)/N2) - 1;
G4 = 1 - 1/(CINV(1 - ALPHA/2, N3) /N3);
G34 = ((F3 - 1)**2 - (G3 * F3)**2 - H4**2)/F3;

```

```

H34 = ((1 - F4)**2 - (H3 * F4)**2 - G4**2)/F4;
PRINT ALPHA F3 F4;
PRINT G3 H4 H3 G4 G34 H34;
*---Calculation of Confidence Intervals on Sig0sq
using TING method;
Sig0lb = ( S02 - SE2 - SQRT(G3**2 * S02**2
      + H4**2 * SE2**2 + G34*S02*SE2))/(I*K);
Sig0ub = ( S02 - SE2 + SQRT(H3**2 * S02**2
      + G4**2 * SE2**2 + H34*S02*SE2))/(I*K);
Sig0int = max(0, Sig0ub) - max(0, Sig0lb);
PRINT Sig0lb Sig0ub Sig0int;
*---Calculation of Confidence Intervals on SigEsq
using TING method;
SigElb = SE2/(CINV(1 - ALPHA/2, N3)/N3);
SigEub = SE2/(CINV(ALPHA/2, N3)/N3);
SigEint = max(0, SigEub) - max(0, SigElb);
PRINT SigElb SigEub SigEint;
proc iml;
y = {50, 53, 65, 55, 84, 104, 64, 61, 81, 81,
      108, 118, 97, 79, 103, 105, 123, 137, 141,
      142, 158, 154, 192, 195};
x = {61, 65, 59, 44, 64, 70, 54, 58, 65, 53,
      41, 67, 62, 48, 61, 53, 41, 41, 66, 61, 56,
      49, 69, 57};
one = j(24, 1, 1);
x = one||x;
print y x;
z1 = {1 0 0 0, 1 0 0 0, 1 0 0 0, 1 0 0 0, 1 0 0 0, 1 0 0 0,
      0 1 0 0, 0 1 0 0, 0 1 0 0, 0 1 0 0, 0 1 0 0, 0 1 0 0,
      0 0 1 0, 0 0 1 0, 0 0 1 0, 0 0 1 0, 0 0 1 0, 0 0 1 0,
      0 0 0 1, 0 0 0 1, 0 0 0 1, 0 0 0 1, 0 0 0 1, 0 0 0 1};
z2 = {1 0 0, 1 0 0, 0 1 0, 0 1 0, 0 0 1, 0 0 1,
      1 0 0, 1 0 0, 0 1 0, 0 1 0, 0 0 1, 0 0 1,
      1 0 0, 1 0 0, 0 1 0, 0 1 0, 0 0 1, 0 0 1,
      1 0 0, 1 0 0, 0 1 0, 0 1 0, 0 0 1, 0 0 1};
I = ncol(z1);
J = ncol(z2);
K = 2;
print I J K;

```

```

z3 = I(I*J*K);
w1 = (1/(J*K))*z1';
w2 = (1/(I*K))*z2';
w3 = z3';
x1 = w1* x;
x2 = w2* x;
x3 = x||z1||z2;
print x1 x2;
h1 = x1*inv(x1'*x1)*x1';
h2 = x2*inv(x2'*x2)*x2';
h3 = x3*ginv(x3'*x3)*x3';
i4 = i(I);
i3 = i(J);
i24 = i(I*J*K);
r1 = J*K * y'*w1'*(i4 - h1)*w1*y;
r2 = I*K * y'*w2'*(i3 - h2)*w2*y;
r3 = y'*w3'*(i24 - h3)*w3*y;
print r1 r2 r3;
*--- Observed values-----;
sp2 = r1 / (I - 2);
so2 = r2 / (J - 2);
se2 = r3 / (I*J*K - I - J);
print sp2 so2 se2;
DF3 = I*J*K - I - J;
DF1 = I - 2;
DF2 = J - 2;
ALPHA = 0.10;
SEED1 = 239480;
SEED2 = 189790;
SEED3 = 3344393;
SEED4 = 9007889;
IT2 = 10000;
IT1 = 1;
KKK = IT1;
GPQ=J(IT2, IT1);
DO LL = 1 TO IT2 ;
    USS = 2 * RANGAM(SEED3, DF3/2);
    UTS = 2 * RANGAM(SEED4, DF1/2);
    ESTIMATEP = (1/(J*K)) *

```

```

      ( (DF1 / UTS) * SP2 - (DF3 / USS) * SE2);
      GPQ(|LL, KKK|) = ESTIMATEP ;
END;
*-----Sort  GPQ and find PERCENTILES;
FINAL=J(IT2, IT1, 0); DO MM = 1 TO IT1;
      X = GPQ(|, MM|);
      B = X;
      X[RANK(X),] = B;
      FINAL(|,MM|) = X;
END;
LOWERBDP = FINAL(|IT2 * ALPHA/2,|);
UPPERBDP = FINAL(|IT2*(1-ALPHA/2),|);
PRINT LOWERBDP UPPERBDP;
DO LL = 1 TO IT2 ;
      USS = 2 * RANGAM(SEED3, DF3/2);
      UTS = 2 * RANGAM(SEED4, DF2/2);
      ESTIMATEO = (1/(I*K)) *
      ( (DF2 / UTS) * S02 - (DF3 / USS) * SE2);
      GPQ(|LL, KKK|) = ESTIMATEO ;
END;
*-----Sort  GPQ and find PERCENTILES;
FINAL=J(IT2, IT1, 0);
DO MM = 1 TO IT1;
      X = GPQ(|, MM|);
      B = X;
      X[RANK(X),] = B;
      FINAL(|,MM|) = X;
END;
LOWERBDO = FINAL(|IT2 * ALPHA/2,|);
UPPERBDO = FINAL(|IT2*(1-ALPHA/2),|);
PRINT LOWERBDO UPPERBDO;
DO LL = 1 TO IT2 ;
      USS = 2 * RANGAM(SEED3, DF3/2);
      ESTIMATEE = (DF3 / USS) * SE2 ;
      GPQ(|LL, KKK|) = ESTIMATEE ;
END;
*-----Sort  GPQ and find PERCENTILES;
FINAL=J(IT2, IT1, 0);
DO MM = 1 TO IT1;

```

```

X = GPQ(|, MM|);
B = X;
X[RANK(X),] = B;
FINAL(|,MM|) = X;
END;
LOWERBDE = FINAL(|IT2 * ALPHA/2,|);
UPPERBDE = FINAL(|IT2*(1-ALPHA/2),|);
PRINT LOWERBDE UPPERBDE;
RUN;

```

